



**JACCO**

# Airflow Measurement Systems

Greg Drensky

# Who is Jacco

- Established 1968
  - Hudson, Ohio
  - Columbus, Ohio
  - Toledo, Ohio
- Focused on the Engineered Environment
  - Systems Knowledgeable
    - HVAC Systems
    - Service & Maintenance
    - Parts
- Full Circle Support
- 30 Minute Design



# Who is Jacco

## •Operations Group

- Brenda Homjak
- Mike Spangler
- Chad Russell



## Purpose Statement

The purpose of our Company is to solve our customers problems, in the most economical way, at all times optimizing the owning experience.





## Who is Jacco

- 30 Minute Design

- Unit Performance
- Drawing
- Weights
- Electrical
- Specifications?
- Sequence of Operation?
- Cartoon?
- Narrative?



# Who is Jacco

## 2015 Seminars

Seminars	Instructor	Date
Psychrometrics	JKC	14-Jan
The Refrigeration Cycle	JKC	11-Feb
Energy Recovery	GAD	11-Mar
Applied Rooftop Systems	JKC	8-Apr
VRF Design & Installation	GAD	13-May
Geothermal Systems	GAD	10-Jun
Chilled Beam, Radiant Cooling & DOAS	JKC	12-Aug
Vertical Market Systems	GAD	9-Sep
Building Pressure & Air Flow Measurement	GAD	14-Oct
Controlling HVAC Systems - Sequence of Operations	JKC	11-Nov



*Accurate*

*Stable*

*Reliable*

## *Airflow Measurement Solutions*

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# Agenda

- Why Measure & Control Outdoor Air Delivery?
  - Industry Updates
- Analyze Alternatives:
  - Fixed Outdoor Air Damper Position = No Control
  - Static Pressure Control Strategies
  - AFMS Pressurization Airflow Control Strategies
- Demand Control Ventilation
  - Outdoor Airflow Control Improves CO<sub>2</sub>-based Ventilation Control Systems
- Air Flow Measurement Technology
- Why Ebtron?
- Innovative ways Consulting Engineers are using Air Flow Monitoring to Enhance Building Designs

# Indoor Environmental Quality



## Occupant Well-being

- Health
- Productivity

## Risk Management

- Liability

## Facility Operations

- Energy
- Operations/Maintenance Expense

# Airflow Measurement and IEQ



# Maintain Contaminants below Threshold Levels

## Reduce Contaminant Sources

- Select low VOC emission building materials, carpets, furniture, etc.
- Provide proper filtration (filter bank integrity, replace filters).
- Reduce conditions that favor mold and fungal growth in or near the building envelope (leaks, improper **building pressure**).
- Avoid negative **building pressure** that transports unfiltered outside air into the building prior to HVAC filtration.
- Reduce conditions that favor mold and fungal growth in the HVAC system (maintain drain pans, maintain proper **outside and supply airflow rates**).

## Replace Contaminants with Outdoor Air

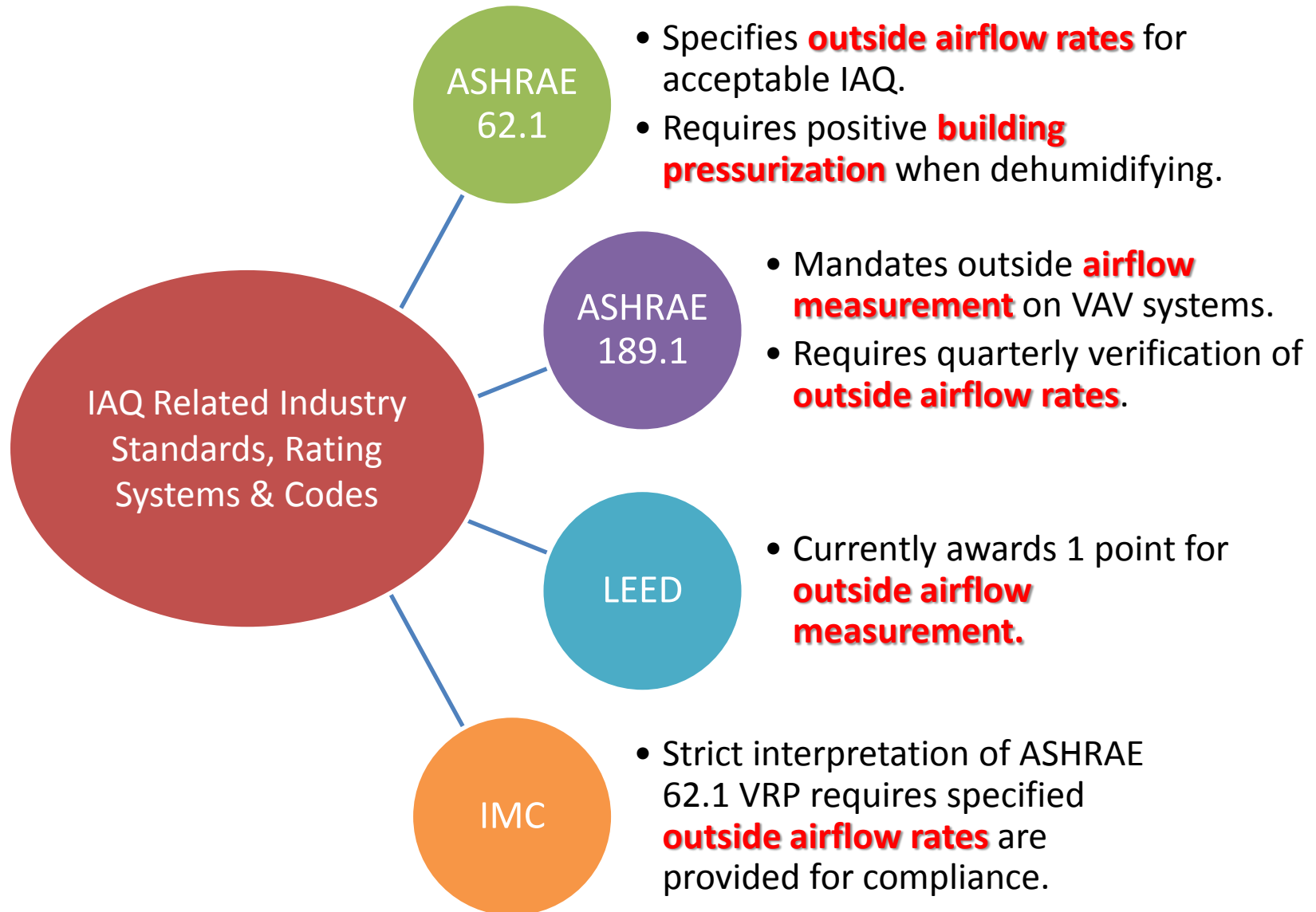
- Provide proper **outside airflow rates** to maintain contaminant levels within the building below threshold levels.

## Provide High Level Filtration when Necessary

- Filter specific contaminants of concern when outside air dilution ventilation is not enough to maintain threshold levels.



# Follow Industry Standards, Rating Systems & Codes



# ASHRAE 62.1-2010

(Includes Addenda a, c, d, and e to 62.1-2010 published in the 2011 Supplement to 62.1-2010)

## 1. PURPOSE

**1.1** The purpose of this standard is to specify minimum ventilation rates and other means to provide conditions suitable to human occupancy. **specify minimum ventilation rates**

**1.2** This standard is intended for regulatory application to new buildings, additions to existing buildings, and existing buildings that are identified in the standard. **regulatory application**  
[new construction/additions]

**1.3** This standard is intended to be used to guide the improvement of indoor air quality in existing buildings. **guide**  
[improve existing buildings]

# ASHRAE 189.1-2011

(Proposed addendum s)

BSR/ASHRAE/IES/USGBC Addendums to ANSI/ASHRAE/USGBC/IES Standard 189.1-2011

## Public Review Draft

Proposed Addendum s to Standard 189.1-2011 Standard for the Design of High-Performance Green Buildings Except Low-Rise Residential Buildings

Second Public Review (Independent Substantive Change - September 2012) (Draft Shows Proposed Changes to Current Standard)

This draft has been recommended for public review by the responsible project committee. To submit a comment on this proposed addendum, go to the ASHRAE website at <http://www.ashrae.org/standards/iesar-draft-technology/public-review-draft> and access the online comment database. The draft is subject to modification until it is approved for publication by the Board of Directors and ANSI. Until this time, the current edition of the standard (as modified by any published addenda on the ASHRAE website) remains in effect.




The current edition of any standard may be purchased from the ASHRAE Bookstore @ <http://www.ashrae.org> or by calling 404-639-8400 or 1-800-527-4722 (for orders in the U.S. or Canada).

This standard is under continuous maintenance. To propose a change to the current standard, use the change submitted form available on the ASHRAE website @ <http://www.ashrae.org>.

The appearance of any technical data or editorial material in this public review document does not constitute endorsement, warranty, or guarantee by ASHRAE of any product, service, process, procedure, or design, and ASHRAE expressly disclaims such.

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AMERICAN SOCIETY OF HEATING, REFRIGERATING AND AIR-CONDITIONING ENGINEERS, INC. 1791 Tullie Circle, NE Atlanta GA 30329-2505



**Important Note:** *Addendum s* is in its second and final public review stage. Content variation with respect to airflow measurement is not substantially different from the parent document except where noted on the following slides.

# ASHRAE 189.1-2011

(Proposed addendum s)

## 8.3.1.2 Outdoor Air Delivery Monitoring.

**8.3.1.2.2 Monitoring Requirements.** Each mechanical ventilation system shall have a permanently installed device to measure the *minimum outdoor airflow*, which meets the following requirements:

1. The device shall employ methods described in ASHRAE Standard 111.
2. The device shall have an accuracy **±10%** of the *minimum outdoor airflow*. Where the *minimum outdoor airflow* varies, as in *demand control ventilation* systems, the device shall maintain this accuracy over the entire range of occupancy and system operation.
3. The device shall be capable of notifying the building operator, either by activating a local indicator or by sending a signal to a building monitoring system, whenever an *outdoor air fault condition* exists. This notification shall require manual reset.

**Exception:** Constant volume air supply systems that do not employ *demand control ventilation* and that use an indicator to confirm that the intake damper is open to the position, determined during system startup and balancing, needed to maintain the design *minimum outdoor airflow*.

WHY EXEMPT?

# Pressurization Control Helps Meet the Intent of LEED 2009: Better Performing Buildings

Prerequisite or Credit	Description	NC	SCHOOLS	CS
EA Prerequisite 1	Fundamental Commissioning	Required	Required	Required
EA Prerequisite 2	Minimum Energy Performance	Required	Required	Required
EA Credit 1	Optimize Energy Performance	1-19 points	1-19 points	3-21 points
EA Credit 3	Enhanced Commissioning	2 points	2 points	2 points
EA Credit 5	Measurement and Verification	3 points	2 points	NA
IEQ Prerequisite 1	Minimum IAQ Performance	Required	Required	Required
IEQ Prerequisite 2	ETS (tobacco smoke) Control	Required	Required	Required
IEQ Prerequisite 3	Minimum Acoustical Performance	NA	Required	NA
<b>IEQ Credit 1</b>	<b>Outdoor Air Delivery Monitoring</b>	<b>1 Point</b>	<b>1 Point</b>	<b>1 Point</b>
IEQ Credit 2	Increased Ventilation	1 Point	1 Point	1 Point
IEQ Credit 3/3.1	Construction Management Plan (constr.)	1 Point	1 Point	1 Point
IEQ Credit 3.2	Construction Management Plan (occup.)	1 Point	1 Point	NA
IEQ Credit 6.2	Controllability of Systems - Thermal	1 Point	1 Point	1 Point
IEQ Credit 7/7.1	Thermal Comfort - Design	1 Point	1 Point	1 Point
IEQ Credit 7.2	Thermal Comfort - Verification	1 Point	1 Point	NA
IEQ Credit 9	Enhanced Acoustical Performance	NA	1 Point	NA
IEQ Credit 10	Mold Prevention	NA	1 Point	NA
ID Credit 1	Innovation in Design	1-5 points	1-4 points	1-5 points



## INDOOR ENVIRONMENTAL QUALITY (IEQ) Credit 1: Outdoor Air Delivery Monitoring

Install permanent monitoring systems to ensure that the ventilation systems maintain design minimum requirements. Configure all monitoring equipment to generate an alarm when the airflow values or carbon dioxide levels vary by 10% or more from the design values via either a building automation system alarm to the building operator or a visual or audible alert to the building occupants.

Monitor CO<sub>2</sub> concentrations within all densely occupied spaces (those with a design occupant density of 25 people or more per 1,000 square feet).

Provide a direct outdoor airflow measurement device capable of measuring the minimum outdoor air intake flow with an accuracy of plus or minus 15% of the design minimum outdoor air rate, as defined by ASHRAE 62.1-2007 for mechanical ventilation systems where 20% or more of the design supply airflow serves nondensely occupied spaces.





## Public Review Version of LEED (2012)



### INDOOR ENVIRONMENTAL QUALITY

*Includes:*  
Building Design & Construction  
Interior Design & Construction  
Existing Buildings: Operations and Maintenance  
Neighborhood Development

Credits shown in gray do not have substantive changes and are not open for public comment.

## INDOOR ENVIRONMENTAL QUALITY (EQ) EQ PREREQUISITE: MINIMUM INDOOR AIR QUALITY PERFORMANCE

### Required Monitoring

For variable air volume systems, provide a direct outdoor airflow measurement device capable of measuring the minimum outdoor air intake flow. This device must measure the minimum outdoor air intake flow with an accuracy of  $\pm 10\%$  of the design minimum outdoor airflow rate, as defined by the ventilation requirements above. An alarm must indicate when the outdoor airflow value varies by 15% or more from the outdoor airflow setpoint.

For constant-volume systems, balance outdoor airflow to the design minimum outdoor airflow rate defined by ASHRAE Standard 62.1–2010 (with errata but without addenda2), or higher. Install a current transducer on the supply fan, an airflow switch, or similar monitoring device.





# The IMC is a STRICT interpretation of the ASHRAE Standard 62 *Ventilation Rate Procedure*

Updated: October, 2012

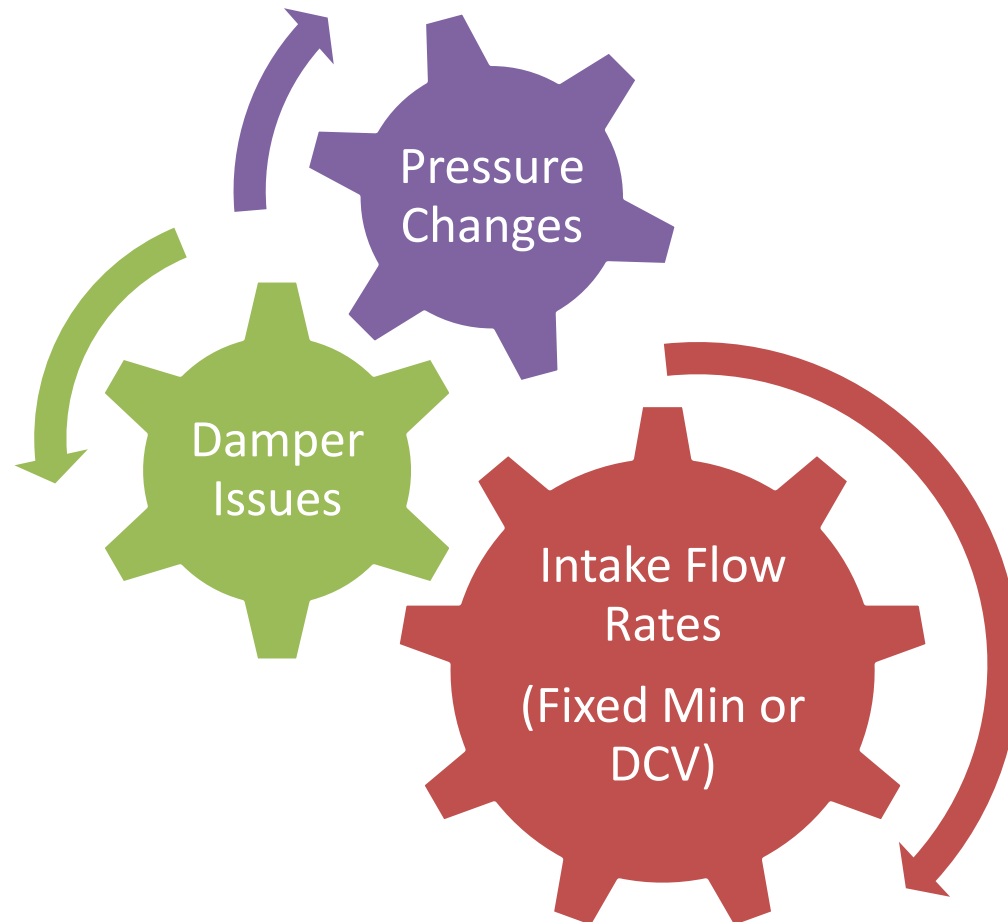


## SECTION 405 SYSTEMS CONTROL

405.1 General. Mechanical ventilation systems shall be provided with manual or automatic controls that will operate such systems whenever the spaces are occupied. Air-conditioning systems that supply required *ventilation air* shall be provided with controls designed to **automatically maintain the required outdoor air supply rate** during occupancy.

# ALL OA Intake Systems

## Require Measurement with Control



# Intake Flow Rate Variations

Damper Issues

Pressure Variations

Hysteresis

Binding

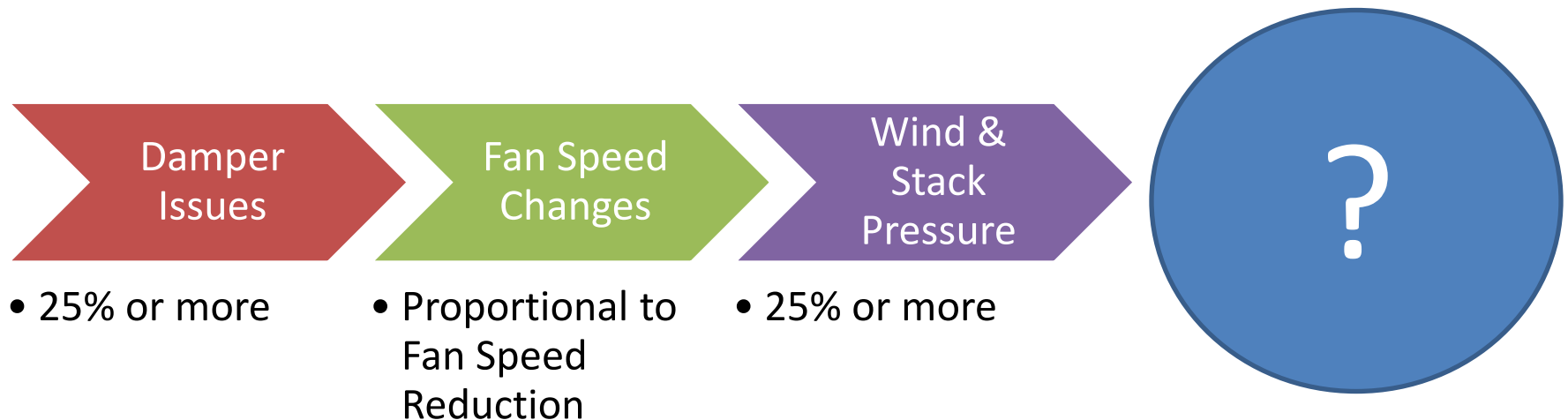
Deterioration

Supply Fan  
Speed

Wind

Stack Effect

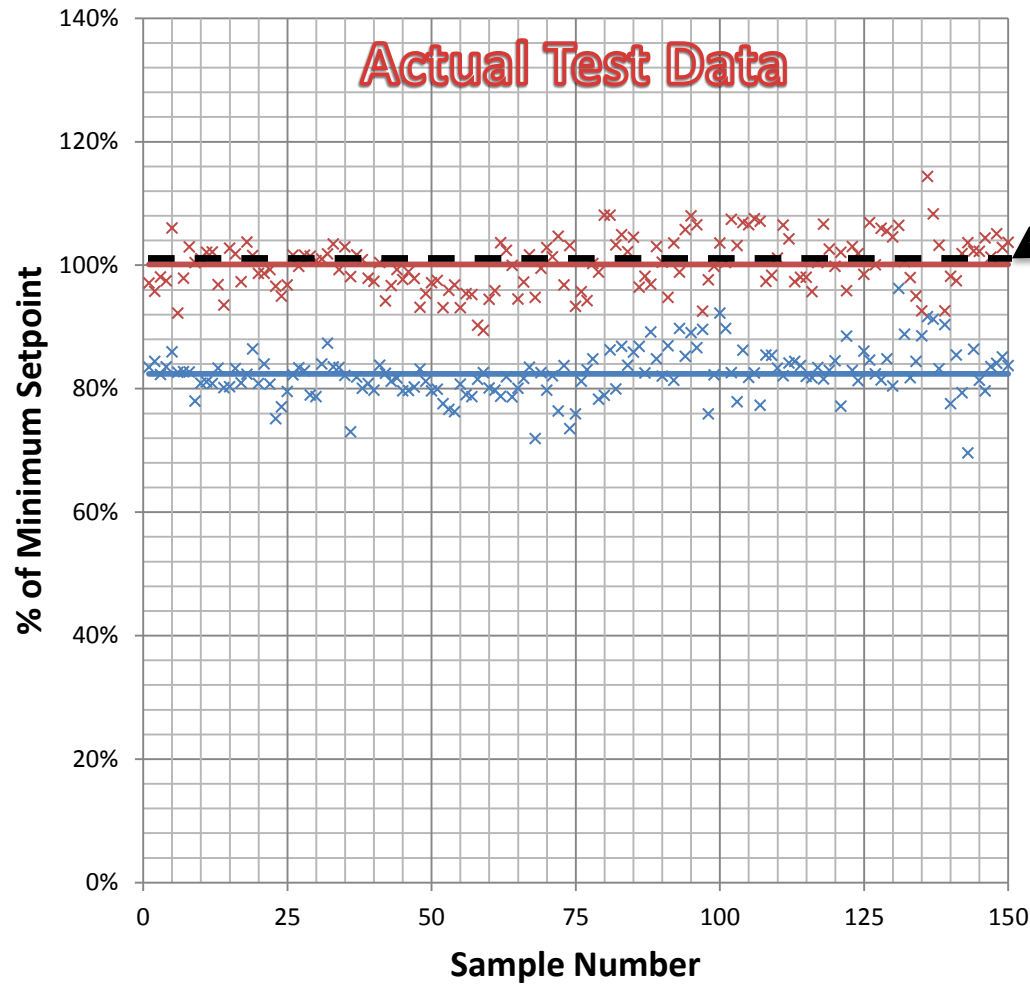
# Cumulative Uncertainty on Non-controlled Intake Flow Rates During Minimum or DCV\* Operation



\* DCV Uncertainty is most critical at minimum and maximum expected populations.

## Hysteresis - No Wind

15% Damper Open

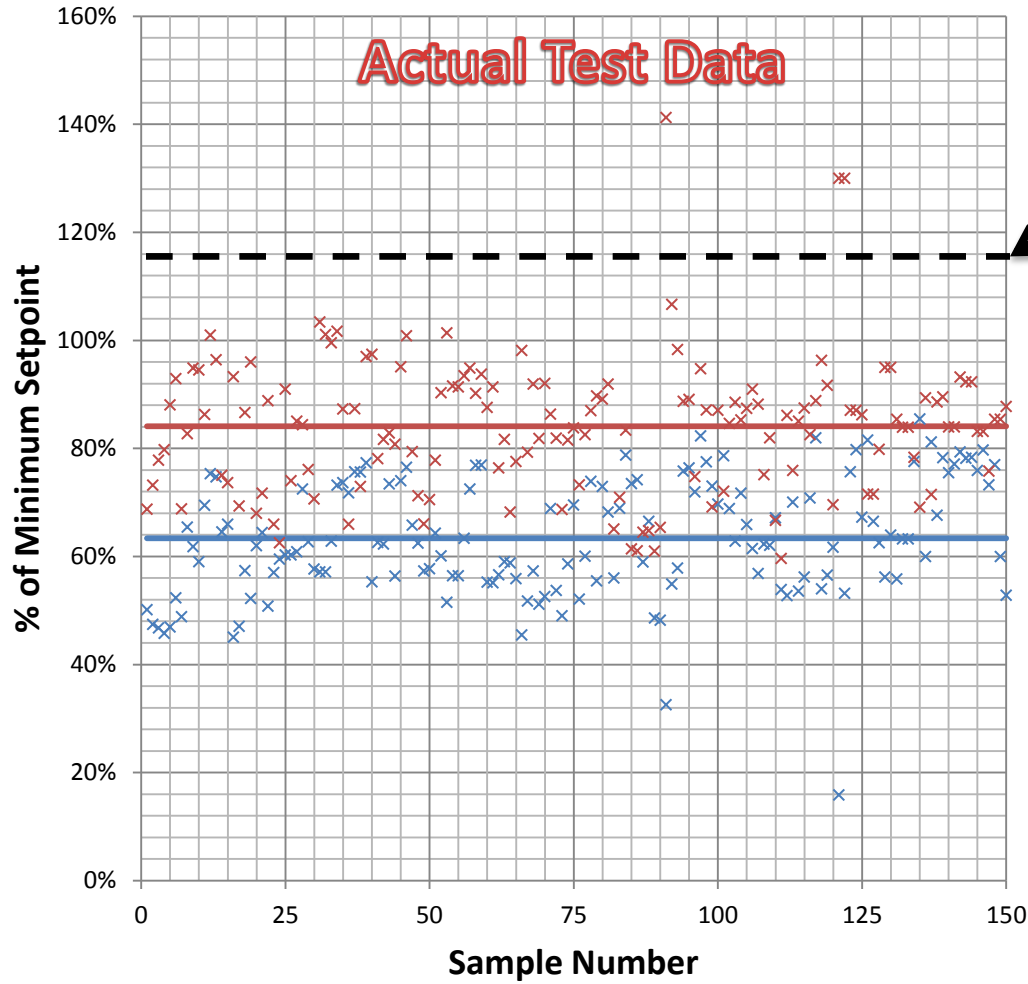


$V_{ot}$  Setpoint



# Hysteresis + 15 mph Cross Wind

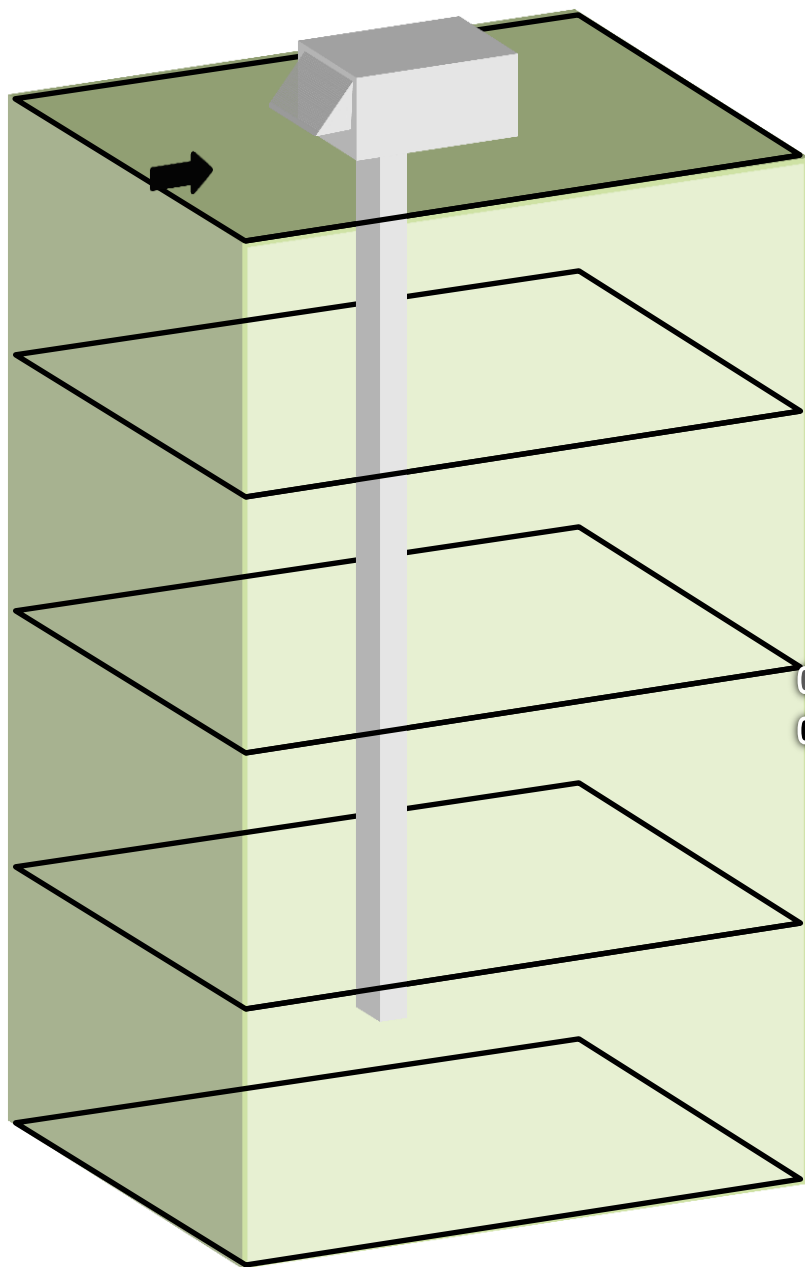
15% Damper Open



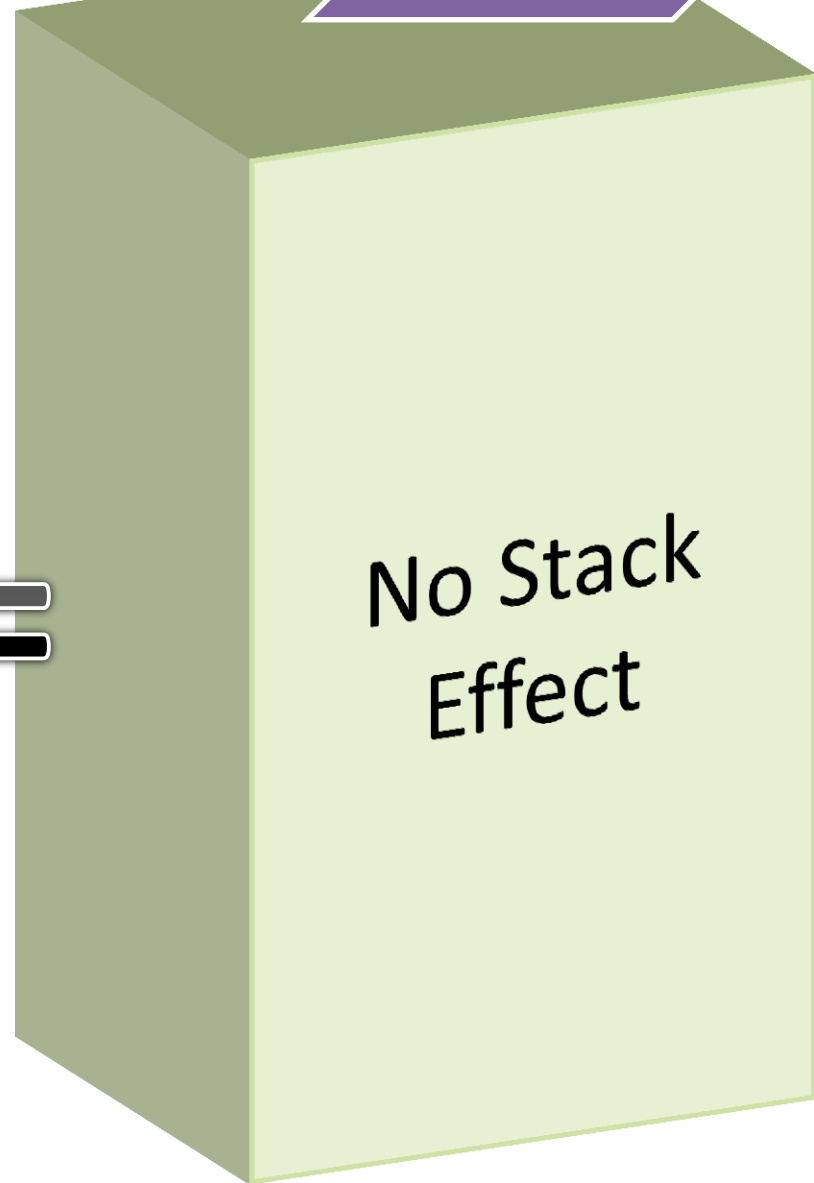
V<sub>ot</sub> Setpoint

- × From Closed
- × From Open
- Average
- Average



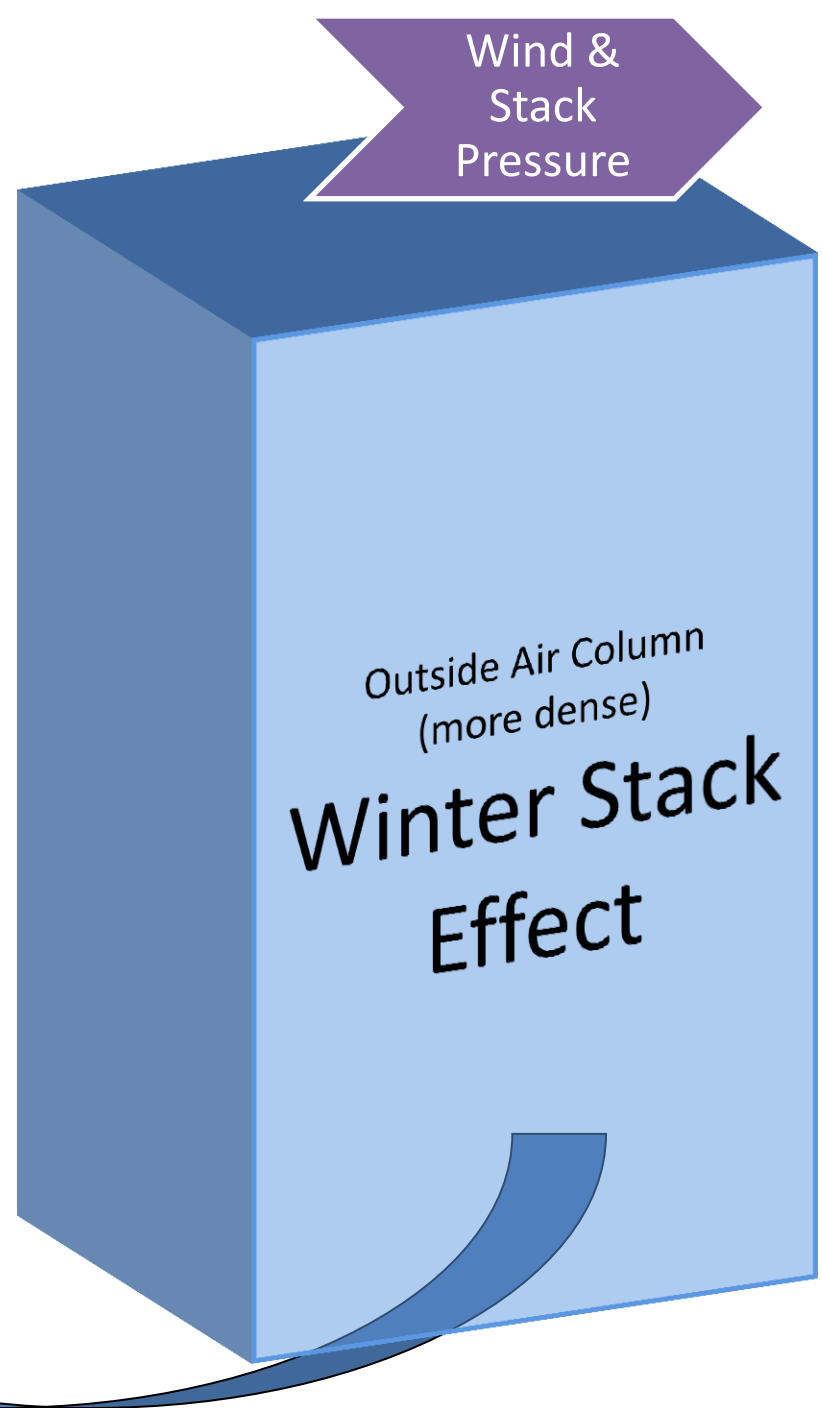
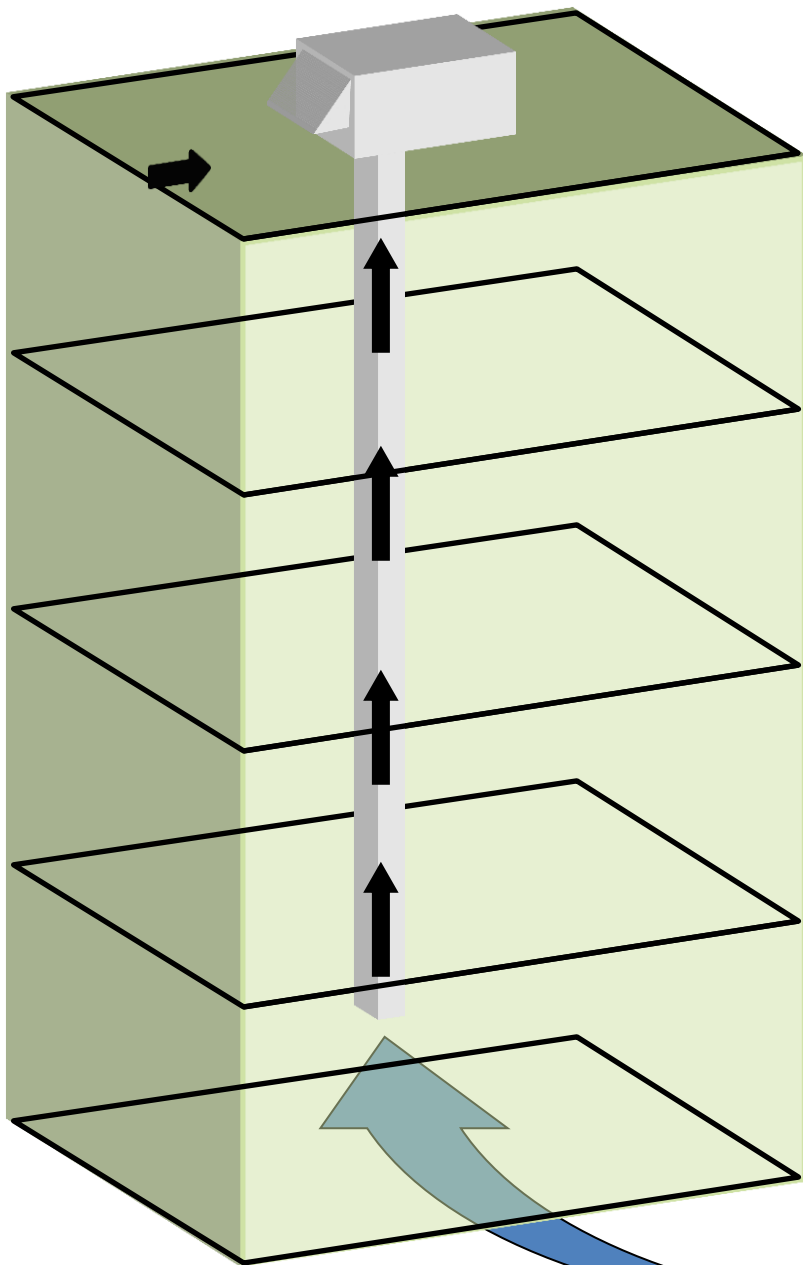


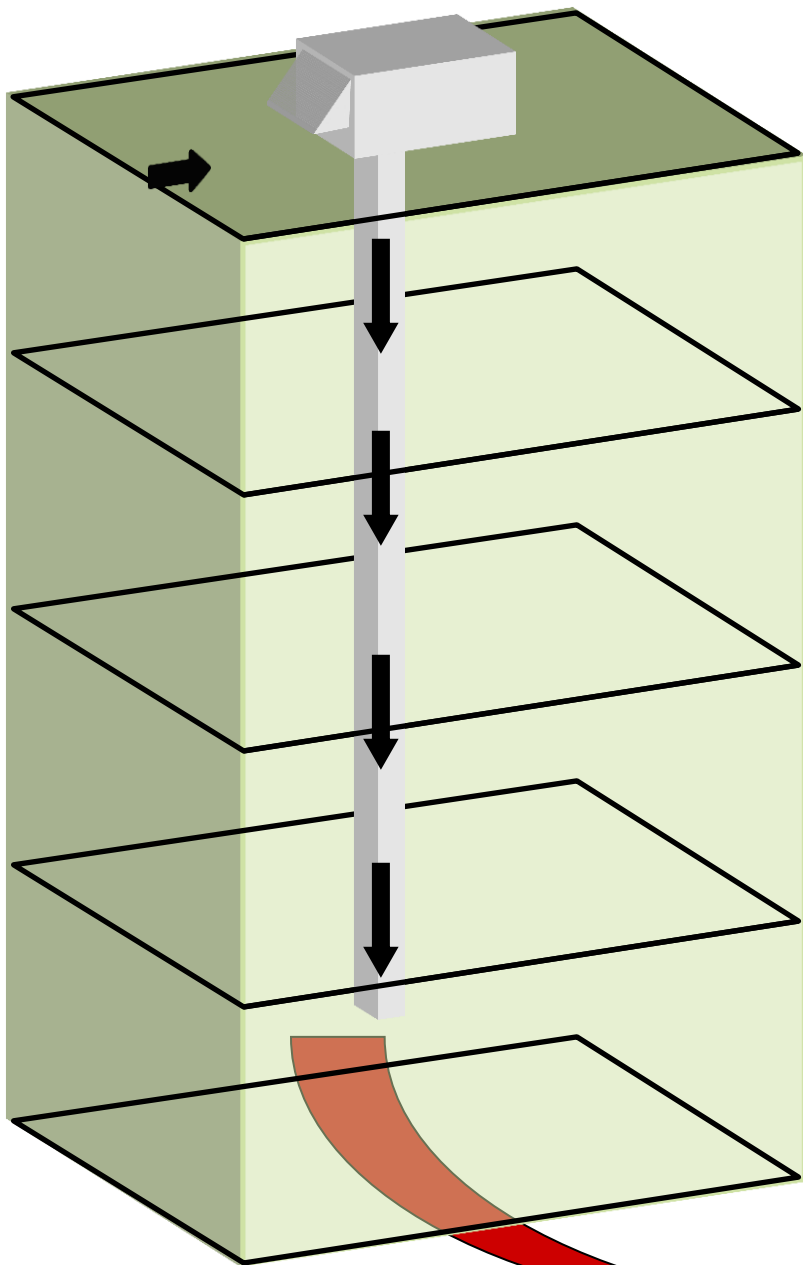
Wind &  
Stack  
Pressure



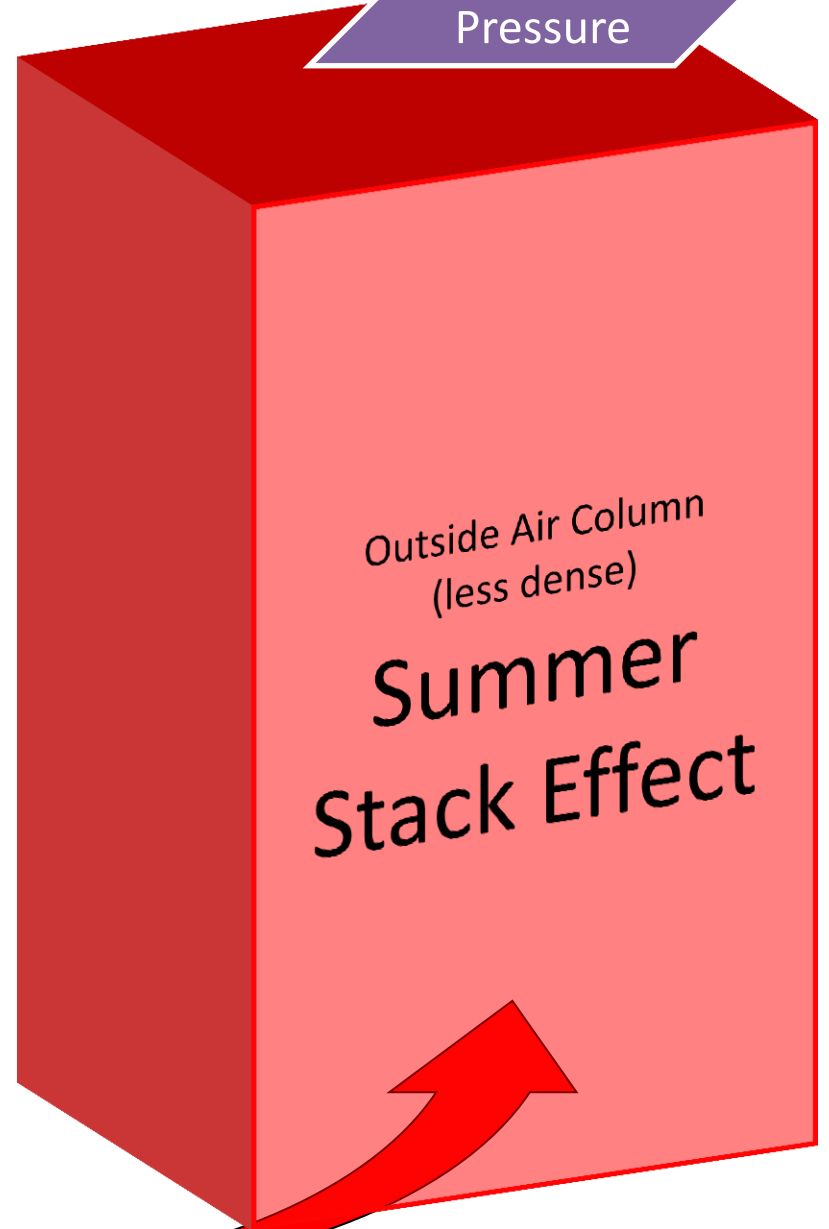
No Stack  
Effect







Wind &  
Stack  
Pressure



Outside Air Column  
(less dense)  
**Summer  
Stack Effect**

# The Logical Conclusion ...



**On ALL OA Intakes**

# Building Pressurization



# ASHRAE 62.1-2010

(Includes Addenda a, c, d, and e to 62.1-2010 published in the 2011 Supplement to 62.1-2010)

**5.9.2 Exfiltration.** For a building, the ventilation system(s) shall be designed to ensure that the minimum outdoor air intake equals or exceeds the maximum exhaust airflow.

**Note:** Although individual zones within a building may be neutral or negative with respect to outdoors or to other zones, net positive mechanical intake airflow for the building as a whole reduces infiltration of untreated outdoor air.

The OA intake airflow shall exceed the exhaust airflow to maintain a net positive mechanical intake airflow to limit dirt/moisture migration.

Negative pressure is an IEQ nightmare!



# Mechanical Cooling

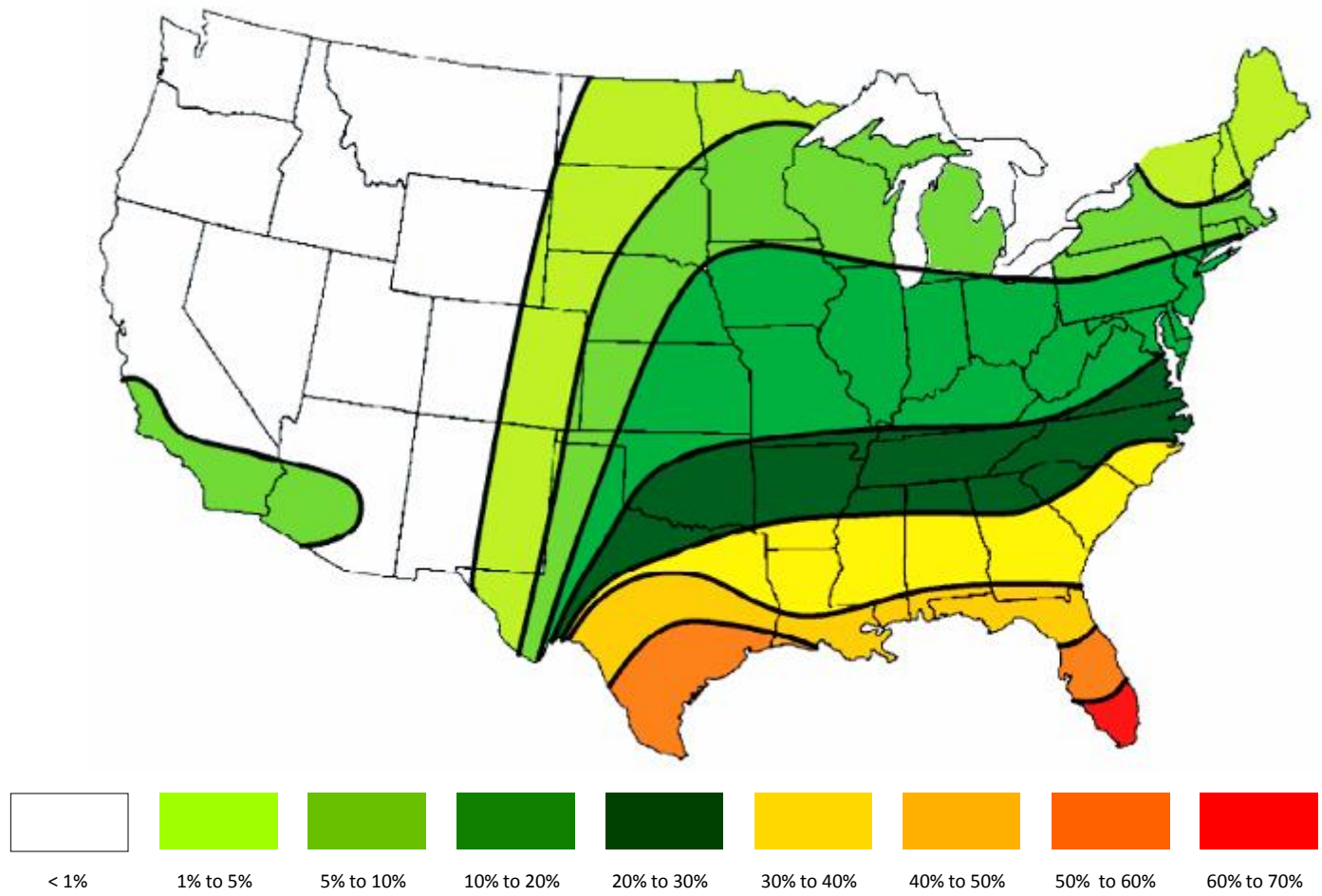




# High Dew Point Regions

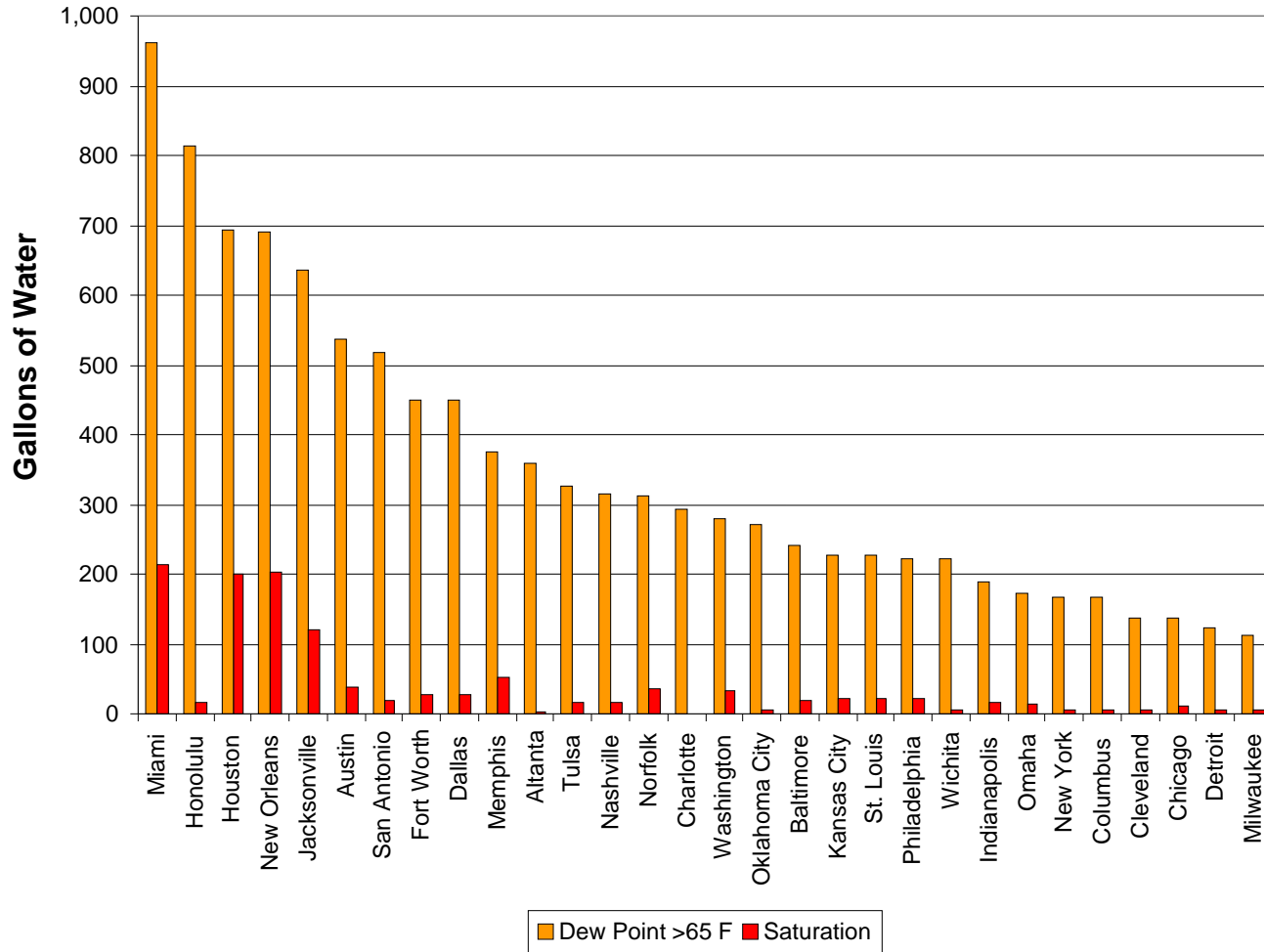
Percentage of year that the dew point exceeds 65 F

5 year hourly dry bulb and dew point analysis



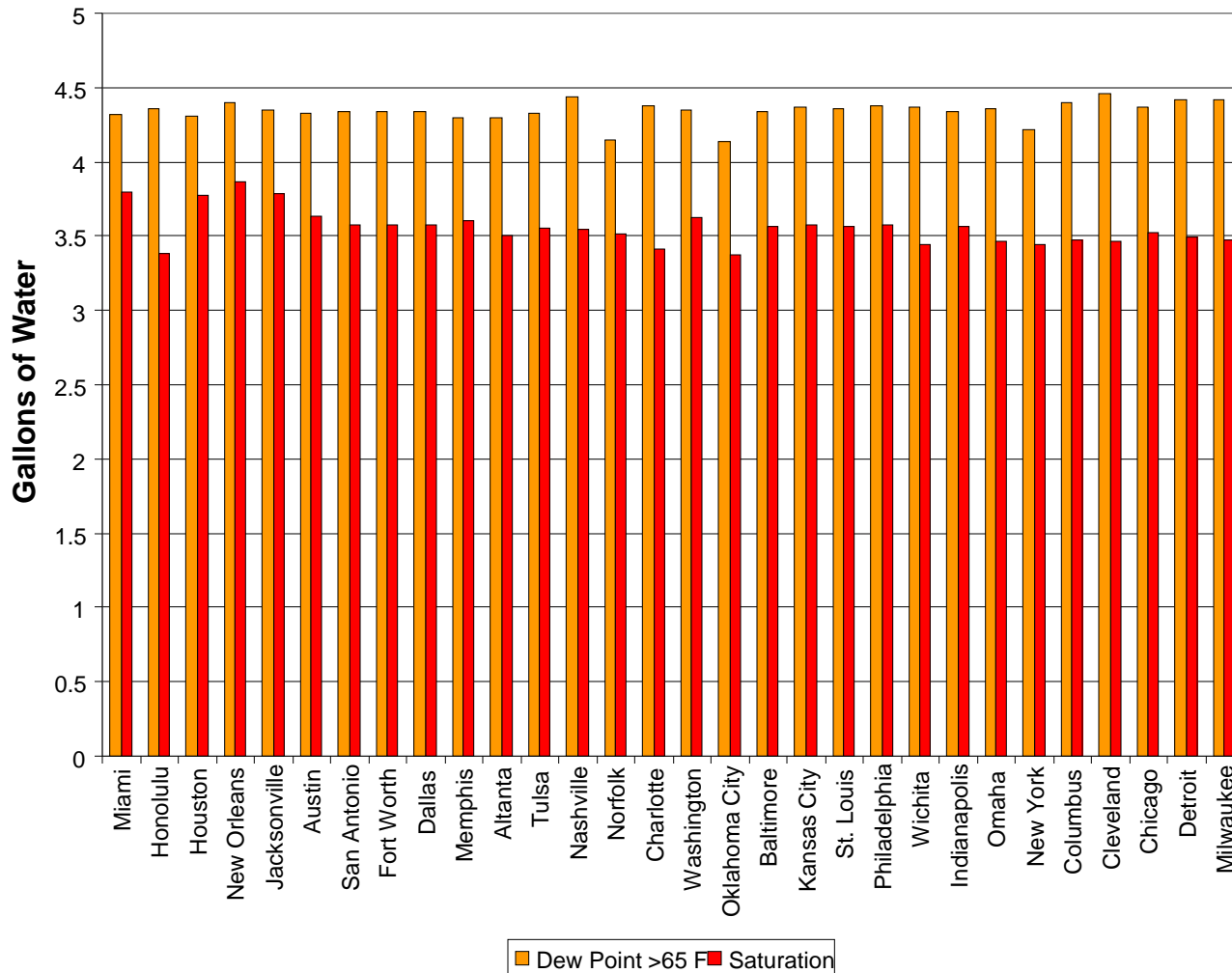
Data provided to EBTRON courtesy of the Forecast Institute, Inc.

**Annual Gallons of Water Transported Across the Building Envelope for every 1,000 CFM of Negative Airflow First 30 of top 50 US Cities by Population (2000 Census)**

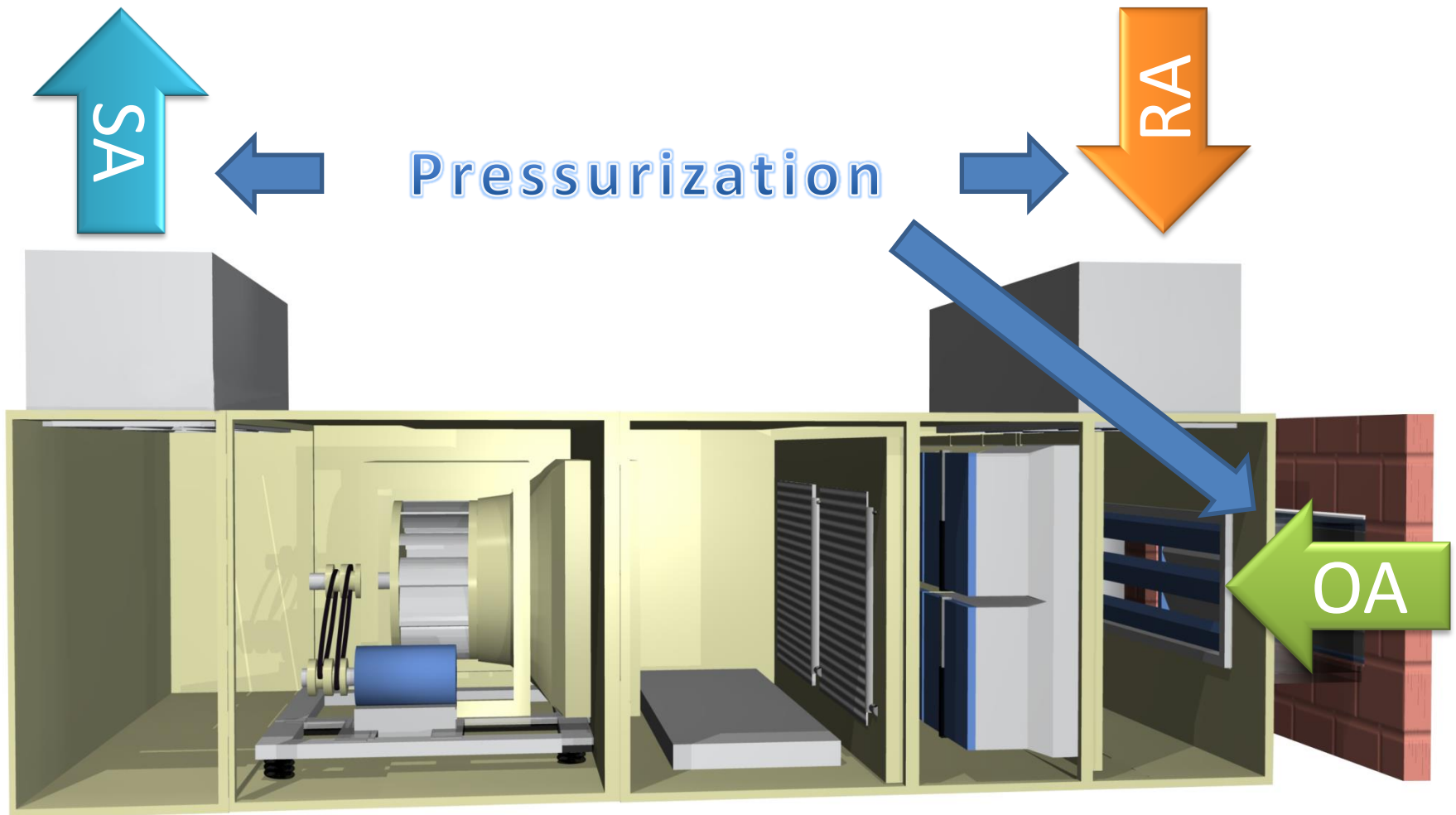




## Avg. Daily Gallons of Water Transported Across the Building Envelope for every 1,000 CFM of Negative Airflow (when outdoor conditions specified exist)



# Airflow Measurement and IEQ



**ACCURACY COUNTS!!!**

# Typical $\Delta P$ Transducer Error

## Performance Data

Standard

Optional

→ Accuracy* RSS(at constant temp)	±1.0% FS	±0.4% FS	±0.25% FS
Non-Linearity, BFSL	±0.96% FS	±0.38% FS	±0.22% FS
Hysteresis	0.10% FS	0.10% FS	0.10% FS
Non-Repeatability	0.05% FS	0.05% FS	0.05% FS
<u>Thermal Effects**</u>			
→ Compensated Range °F(°C)	0 to +150 (-18 to +65)		
→ Zero/Span Shift %FS/°F(°C)	0.033 (0.06)		
Maximum Line Pressure	10 psi		
Overpressure	Up to 10 psi (Range Dependent)		
→ Long Term Stability	0.5% FS/1 YR		

**setra**

**Model 264**

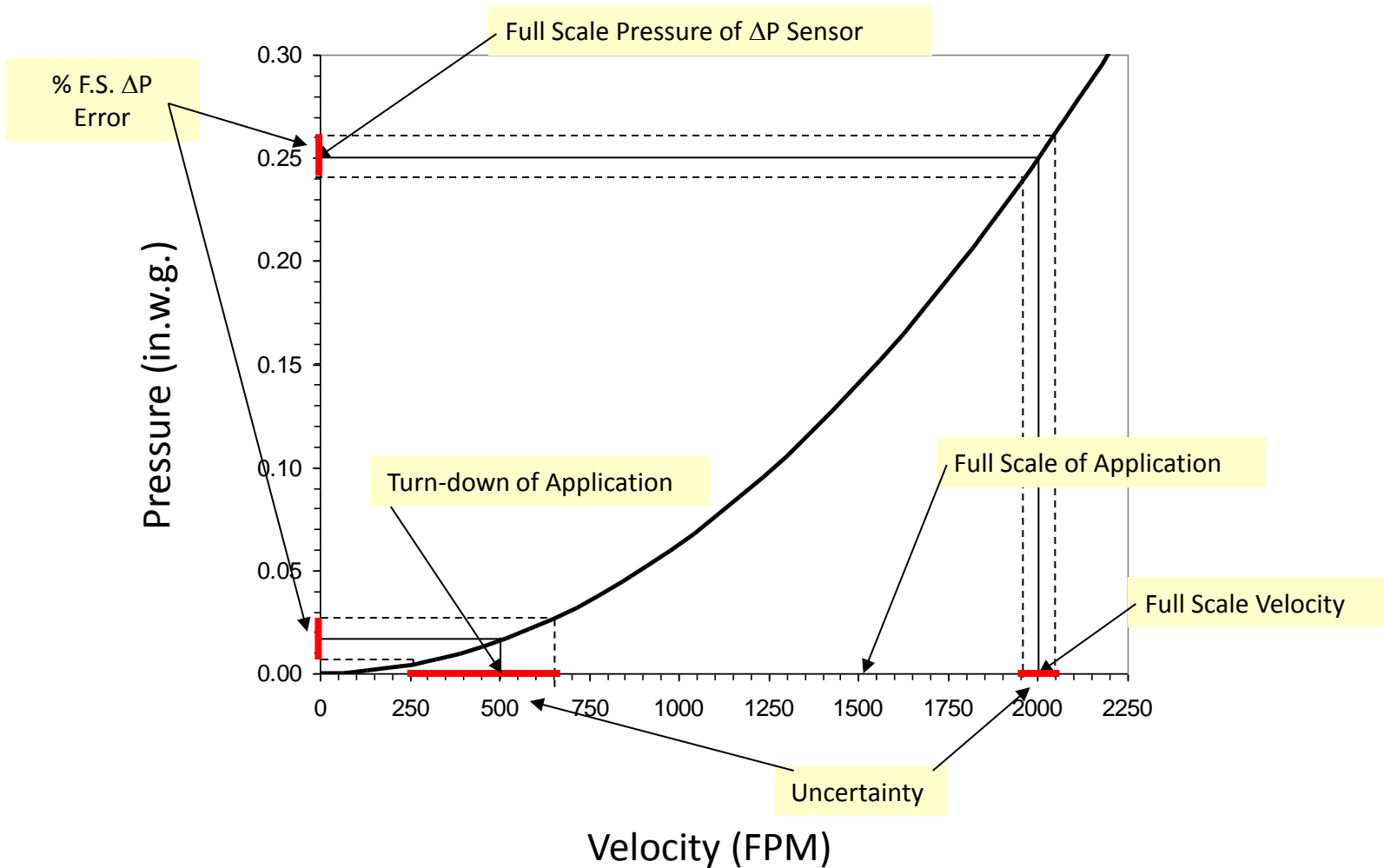
**Very Low Differential Pressure Transducer**

Unidirectional Ranges: 0 - 0.1 to 0 - 100 in. W.C.

Bidirectional Ranges: 0 - ±0.5 to 0 - ±50 in. W.C.

Air or Non-Conducting Gas

# % F.S. Dilemma with $\Delta P$ Devices



# VAV Tracking Example

## System:

Total SA flow: 100,000 CFM  
 $\Delta$ CFM Setpoint: 10,000 CFM  
Building Pressure Desired: 0.02 in.w.g.  
Pressurization Flow: 5,000 CFM  
Local Exhaust: 5,000 CFM  
Max Turndown: 40%  
SA Duct Area: 55.5 ft<sup>2</sup>  
RA Duct Area: 56.7 ft<sup>2</sup>

## Calculated Velocities:

Max velocity SA duct: 1,800 FPM  
Min velocity SA duct: 720 FPM  
Max velocity RA duct: 1,500 FPM  
Min velocity RA duct: 500 FPM

## Sensors:

DP sensor: 0 to 0.25 in.w.g., 1 % F.S.  
Flow probe: Averaging pitot array

## Test Conditions:

DP sensor located in mechanical room  
Setup temperature: 70 °F  
Operating temperature: 100 °F, 1 year after startup

## Component Accuracies:

### DP Sensor:

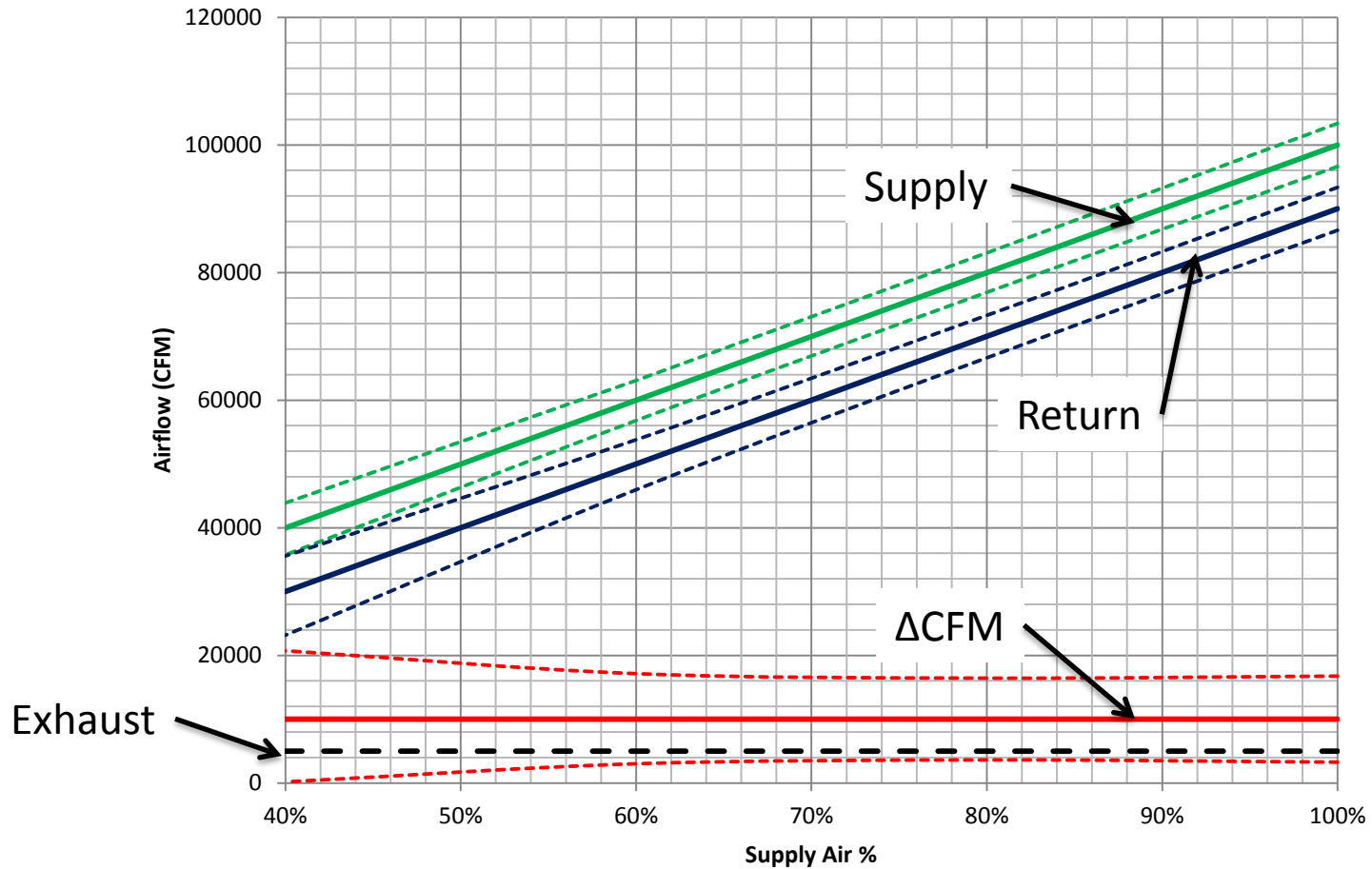
Total Accuracy = Accuracy + Temp Effect + Drift  
1% F.S. + 1% F.S. + ½ % F.S. = 2 ½ % F.S.

### Airflow Measuring Device:

3% of reading

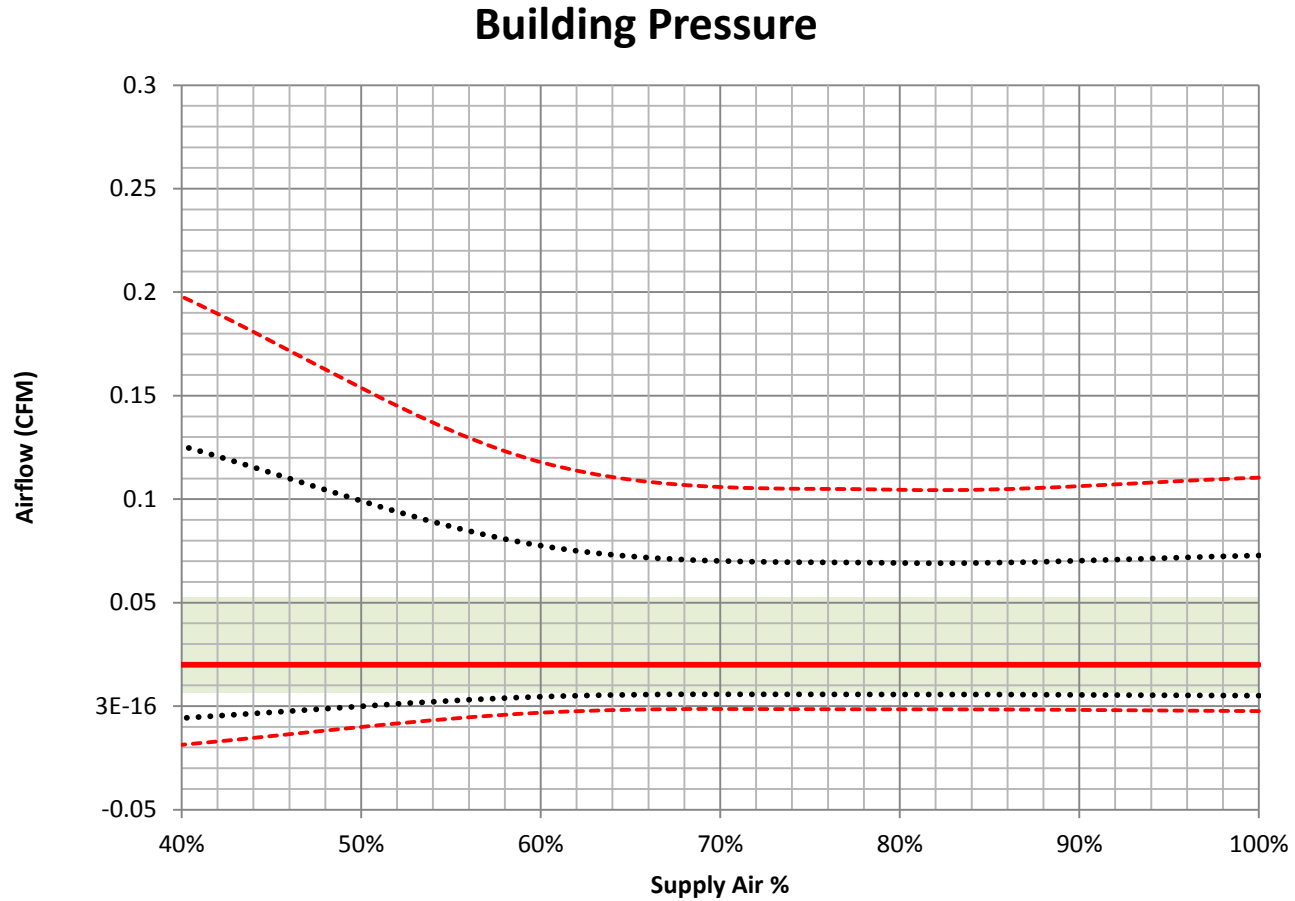
# Pitot Array and Transducer

## Tracking Uncertainty





# Pitot Array and Transducer



# How did we come up with this?



Determine the uncertainty of a 1%, 0 to 0.25 in.w.g. pressure transducer and pitot array at 500 FPM and 100 °F after 1 year?

1. Calculate the velocity pressure for 500 fpm:

$$p_{vel} = \frac{V=4005}{(500/4005)^2} \sqrt{p_{vel}} \longrightarrow \left(\frac{V}{4005}\right)^2 = p_{vel}$$

2. Determine the transducer uncertainty % F.S.:

$$1\% \text{ F.S. (out of box)} + 0.033\% \text{ F.S./}^\circ\text{F} \cdot 30^\circ\text{F} + 0.5\% \text{ (1 year drift)} = 2.5\% \text{ F.S.}$$

3. Determine the transducer uncertainty in in.w.g.

$$2.5\% \cdot 0.25 = 0.00625 \text{ in.w.g.}$$

4. Calculate the velocity after biasing the nominal pressure by the pressure uncertainty and reapplying the equation above (in this case the negative uncertainty)

$$V = 4005 \cdot \sqrt{0.0156 - 0.00625} = 387 \text{ FPM or } -22.6\%$$

5. Add the array uncertainty (in this case we used 3% of reading)

$$\text{Total Uncertainty} = \sqrt{22.6\%^2 + 3\%^2} = 22.8\%$$

# VAV Tracking Example

## System:

Total SA flow: 100,000 CFM  
ΔCFM Setpoint: 10,000 CFM  
Building Pressure Desired: 0.02 in.w.g.  
Pressurization Flow: 5,000 CFM  
Local Exhaust: 5,000 CFM  
Max Turndown: 40%

Fan Throat Velocities:  
Max velocity: 10,000 FPM  
Min velocity: 4,000 FPM

## Sensors:

DP sensor: 0 to 25 in.w.g., 1 % F.S.  
Flow probe: Piezo-ring

## Test Conditions:

DP sensor located in mechanical room  
Setup temperature: 70 °F  
Operating temperature: 100 °F, 1 year after startup

## Component Accuracies:

### DP Sensor:

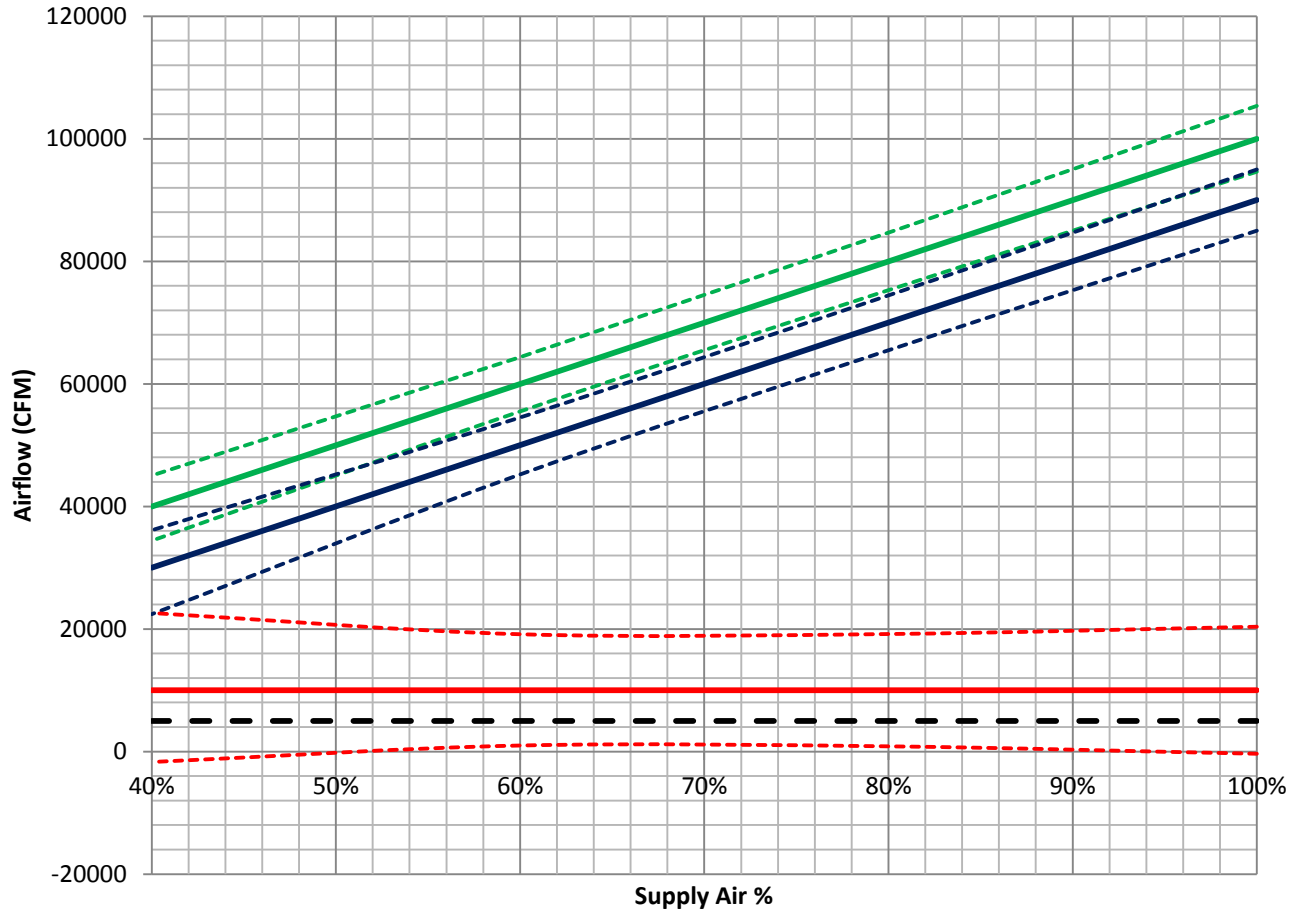
Total Accuracy = Accuracy + Temp Effect + Drift  
1% F.S. + 1% F.S. + ½ % F.S. = 2 ½ % F.S.

### Airflow Measuring Device:

5% of reading

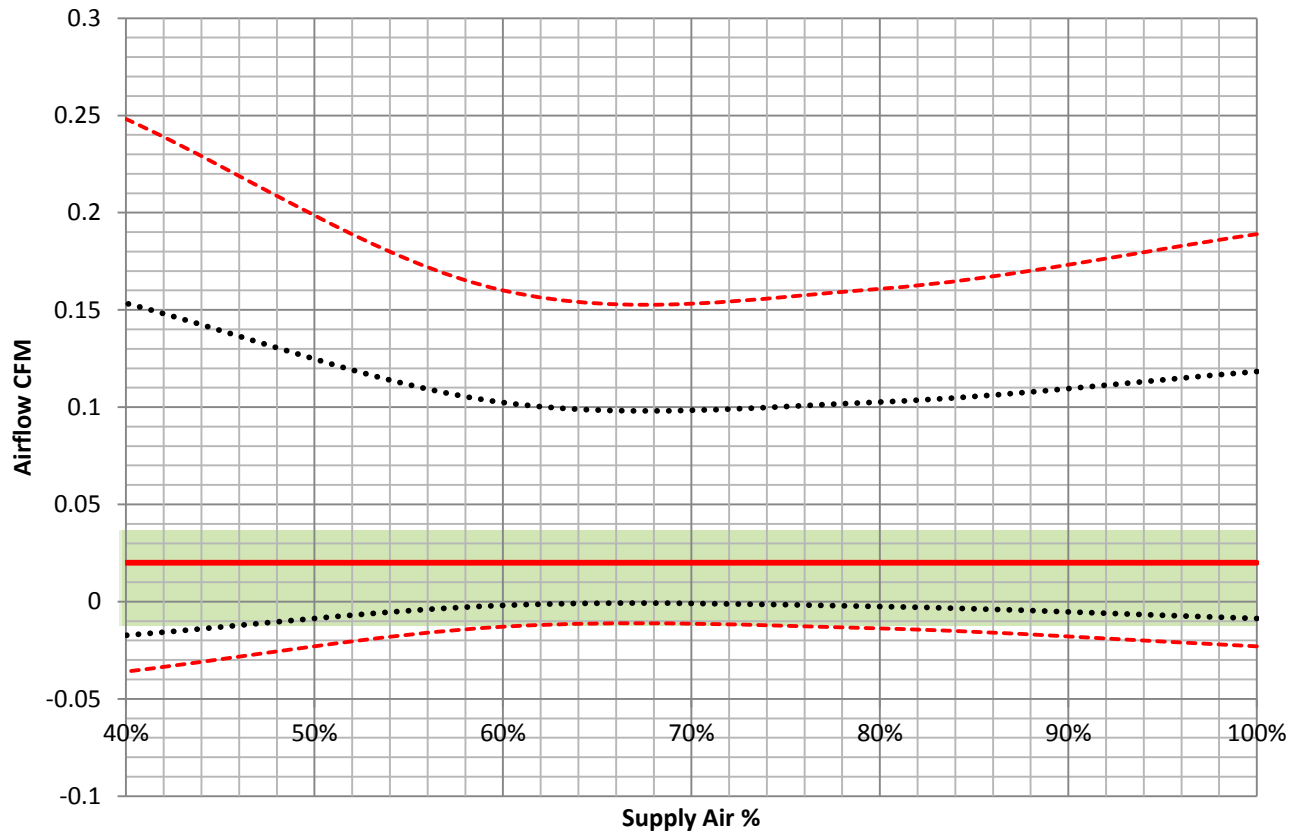
# Piezo-ring and Transducer

## Tracking Uncertainty



# Piezo-ring and Transducer

## Building Pressure



# VAV Tracking Example

## System:

Total SA flow: 100,000 CFM  
 $\Delta$ CFM Setpoint: 10,000 CFM  
Building Pressure Desired: 0.02 in.w.g.  
Pressurization Flow: 5,000 CFM  
Local Exhaust: 5,000 CFM  
Max Turndown: 40%  
SA Duct Area: 55.5 ft<sup>2</sup>  
RA Duct Area: 56.7 ft<sup>2</sup>

## Calculated Velocities:

Max velocity SA duct: 1,800 FPM  
Min velocity SA duct: 720 FPM  
Max velocity RA duct: 1,500 FPM  
Min velocity RA duct: 500 FPM

## Sensors:

EBTRON Thermal Dispersion System ( $\pm 2\%$  of reading sensor accuracy)

## Test Conditions:

Transmitter located in mechanical room  
Setup temperature: 70 °F  
Operating temperature: 100 °F, 1 year after startup

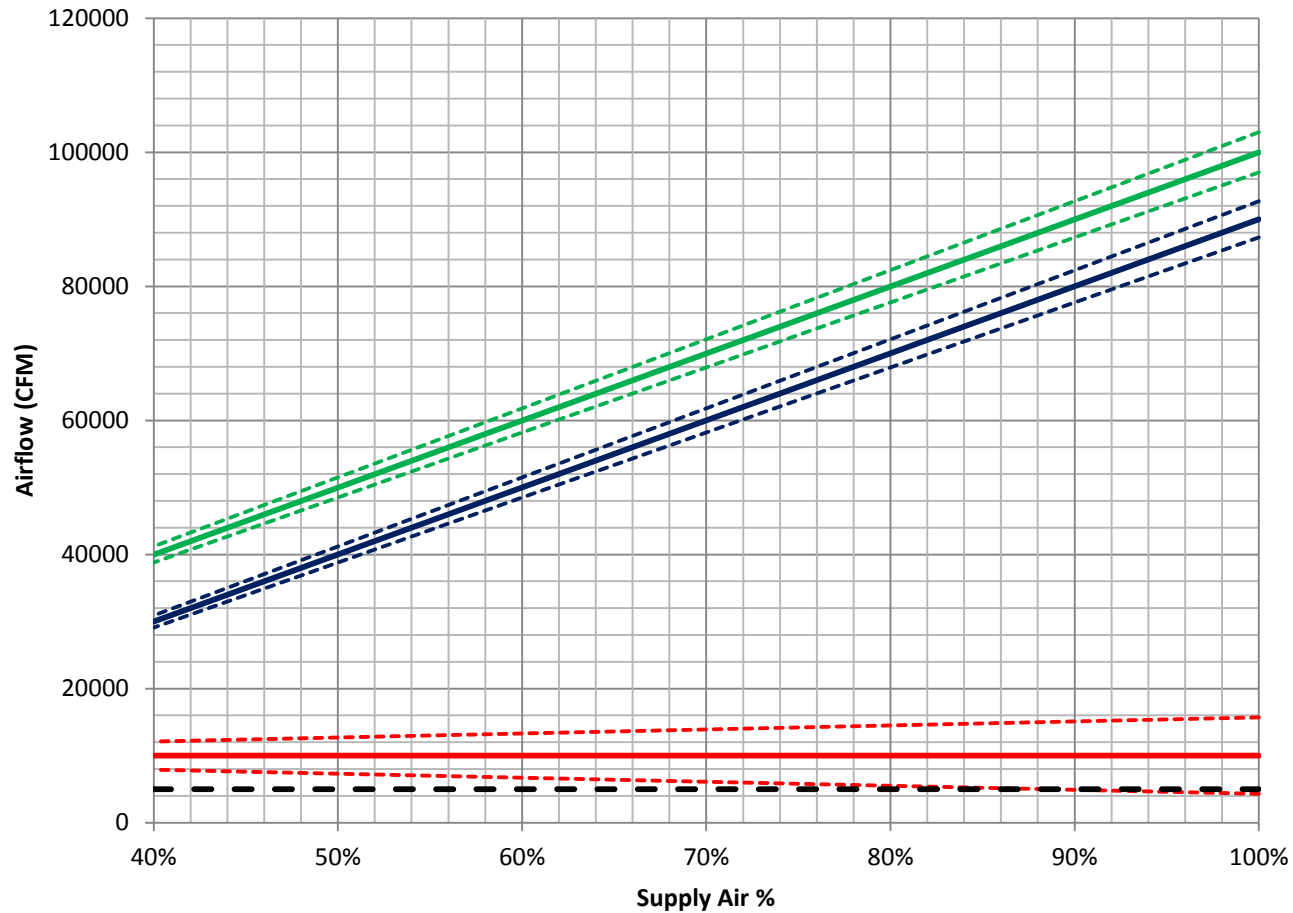
## Component Accuracies:

### System:

Installed accuracy:  $\pm 3\%$  of reading

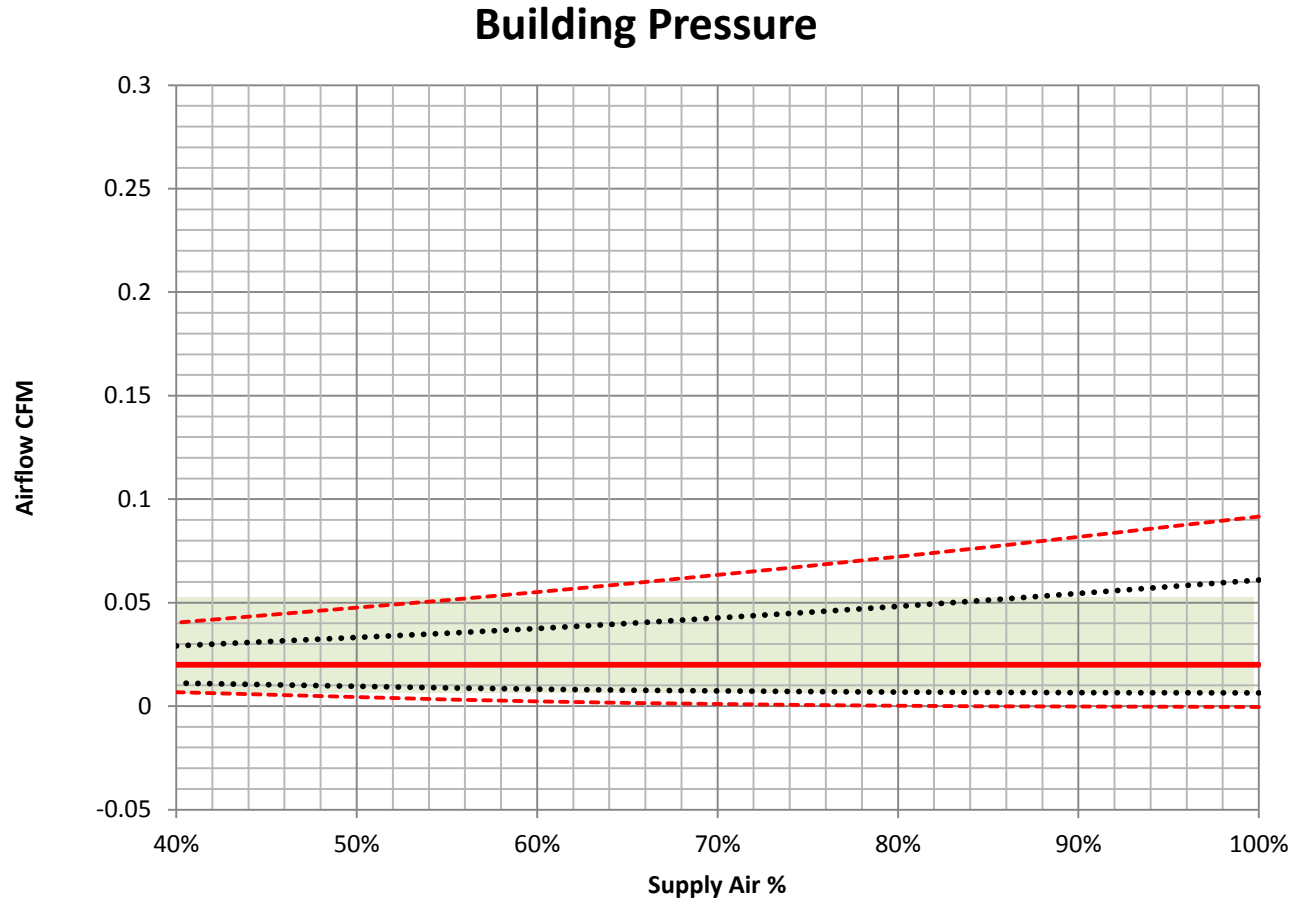
# **EBTRON** a measureable difference!

## Tracking Uncertainty



## GTx116-P Duct & Plenum Probes

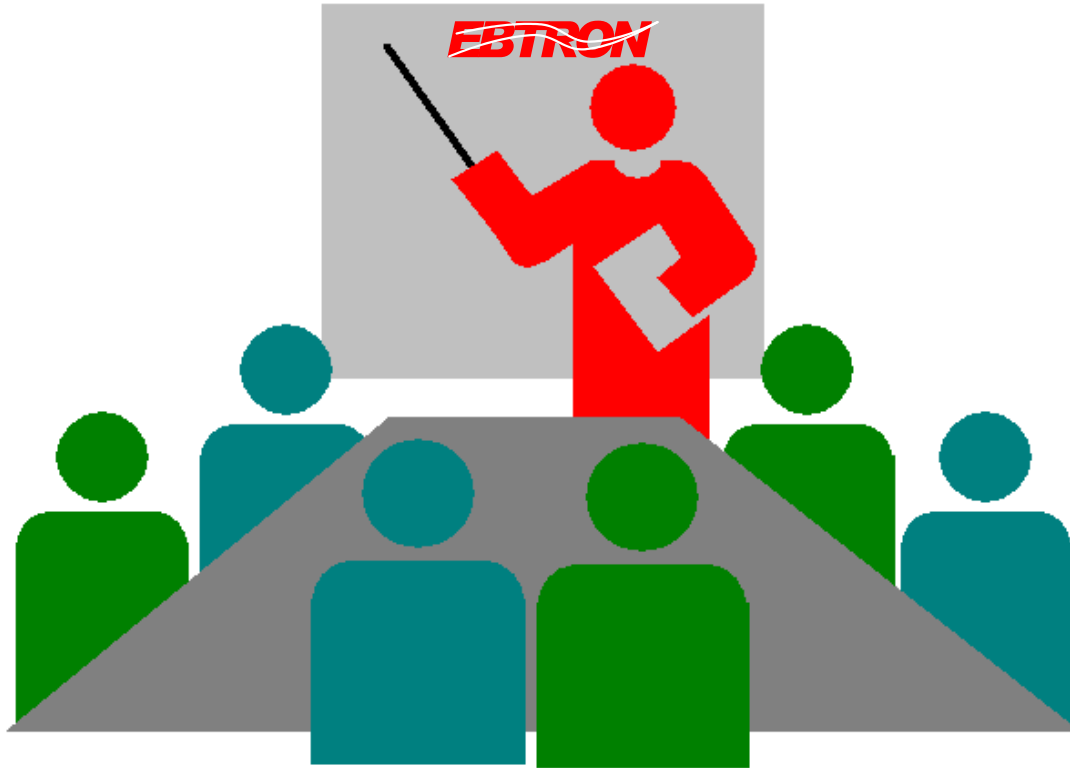
# **EBTRON** a measureable difference!



## GTx116-P Duct & Plenum Probes



# Indoor Environmental Quality



**Demand Control Ventilation**

# ASHRAE 62

## CO<sub>2</sub>, ASHRAE 62 and DCV

### ASHRAE 62-1989 VRP

“Comfort (odor) criteria are likely to be satisfied if the ventilation rate is set so that 1000 ppm CO<sub>2</sub> is not exceeded.”

Misleading!  
Out of Context!  
Would NOT result in  
Compliance!

### ASHRAE 62-1999 and 2001 VRP

“Comfort (odor) criteria with respect to human health and well-being are likely to be satisfied if the ventilation results in indoor CO<sub>2</sub> concentrations not to exceed 700 ppm above the outdoor air concentration.”

Misleading!  
Out of Context!  
Would NOT result in  
Compliance!

### ASHRAE 62-2004 to present

All references to specific CO<sub>2</sub> levels removed

Damage Done!

# CO<sub>2</sub> DCV ...

- Outside air dampers or fans are modulated to maintain the space CO<sub>2</sub> level.
- CO<sub>2</sub> levels are often associated as a direct indication of indoor air quality – the lower the better.
  - Not true. Space CO<sub>2</sub> levels rarely exceed 2,000 ppm. CO<sub>2</sub> does not become a contaminant until levels exceed 5,000 ppm.
  - CO<sub>2</sub> is simply an indirect method to estimate the outside air CFM/person entering the space.
  - There are NUMEROUS assumptions made that affect how CO<sub>2</sub> DCV impacts IAQ.

# ASHRAE 62.1-2010

(Includes Addenda a, c, d, and e to 62.1-2010 published in the  
2011 Supplement to 62.1-2010)

## DCV - Single Zone Systems

### What's needed?

1. Real-time population estimate of the zone ( $P_z$ )
2. Heating/cooling mode to determine  $E_z$
3. Outside airflow measuring device to measure  $V_{ot}$
4. Controller to calculate  $V_{ot}$  and maintain setpoint:

$$V_{ot} = \{R_p \cdot P_z + R_a \cdot A_z\} / E_z$$

# ASHRAE 62.1-2010

(Includes Addenda a, c, d, and e to 62.1-2010 published in the 2011 Supplement to 62.1-2010)

## 100% OA Systems

*Single zone and multi-zone with single zone recirculating systems, radiant panels or chilled beams (not valid on multi-zone recirculating systems).*

**6.2.4 100% Outdoor Air Systems.** For ventilation systems wherein one or more air handlers supply only *outdoor air* to one or more *ventilation zones*, the outdoor air intake flow ( $V_{ot}$ ) shall be determined in accordance with Equation 6-4.

$$V_{ot} = \sum_{all\ zones} V_{oz} \quad (6-4)$$

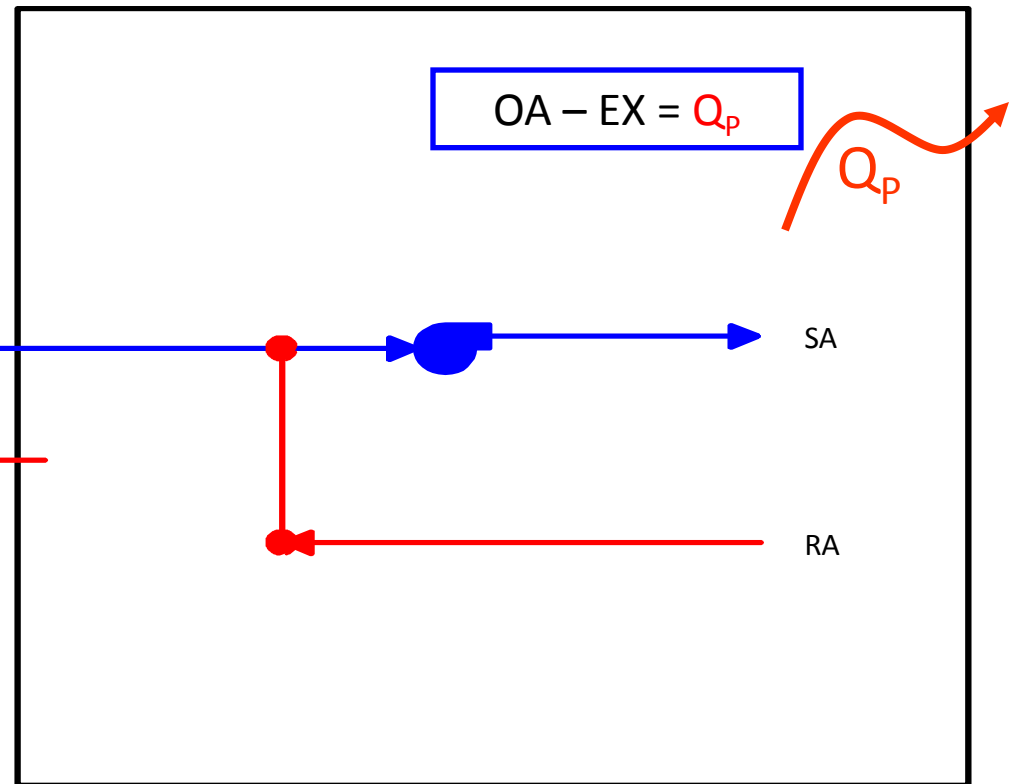
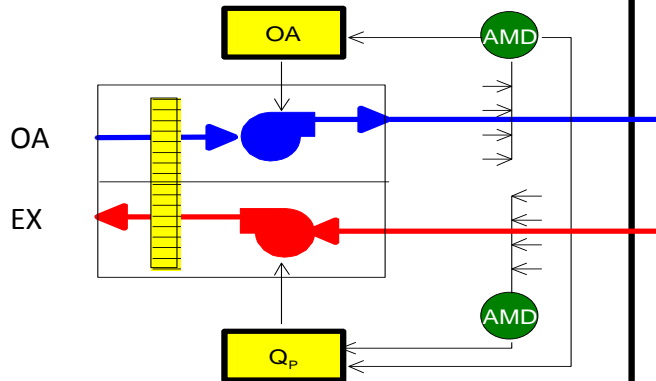
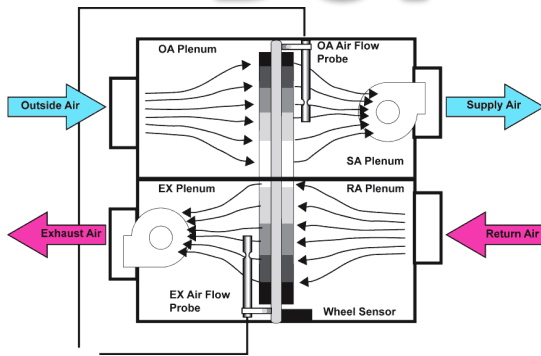
5.  $V_{ot}$  (outdoor air intake flow) is equal to the sum of all  $V_{oz}$ .

# ASHRAE 62.1-2010

(Includes Addenda a, c, d, and e to 62.1-2010 published in the 2011 Supplement to 62.1-2010)

## DCV - 100% OA Systems

*Single zone 100% outside air systems*



Note: In most DOAS systems  $E_z = 1$  (tempered air)

# ASHRAE 62.1-2010

(Includes Addenda a, c, d, and e to 62.1-2010 published in the 2011 Supplement to 62.1-2010)

## DCV - 100% OA Systems

*Single zone 100% outside air systems*

### What's needed?

1. Real-time population estimate of the zone ( $P_z$ )
2. Outside airflow measuring device to measure  $V_{ot}$
3. Controller to calculate  $V_{ot}$  and maintain setpoint:

$$V_{ot} = \{R_p \cdot P_z + R_a \cdot A_z\} / E_z$$

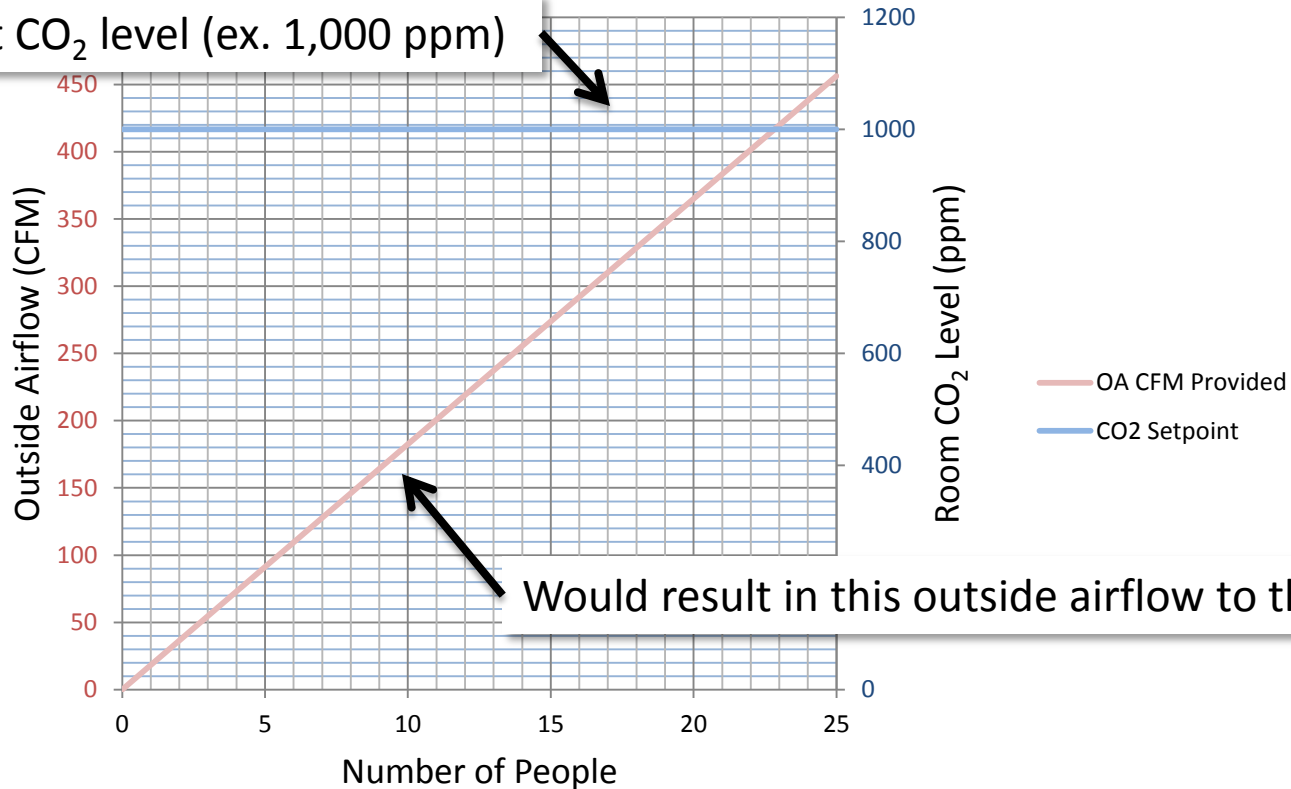
Note: In most DOAS systems  $E_z = 1$  (tempered air)

# Single Setpoint CO<sub>2</sub> DCV

## CO<sub>2</sub> DCV (1,000 sq.ft. classroom)

\*Assumptions: Steady-state, N=10,951, OA CO<sub>2</sub>=400ppm, no sensor error or bias

A constant CO<sub>2</sub> level (ex. 1,000 ppm)



Would result in this outside airflow to the space\*

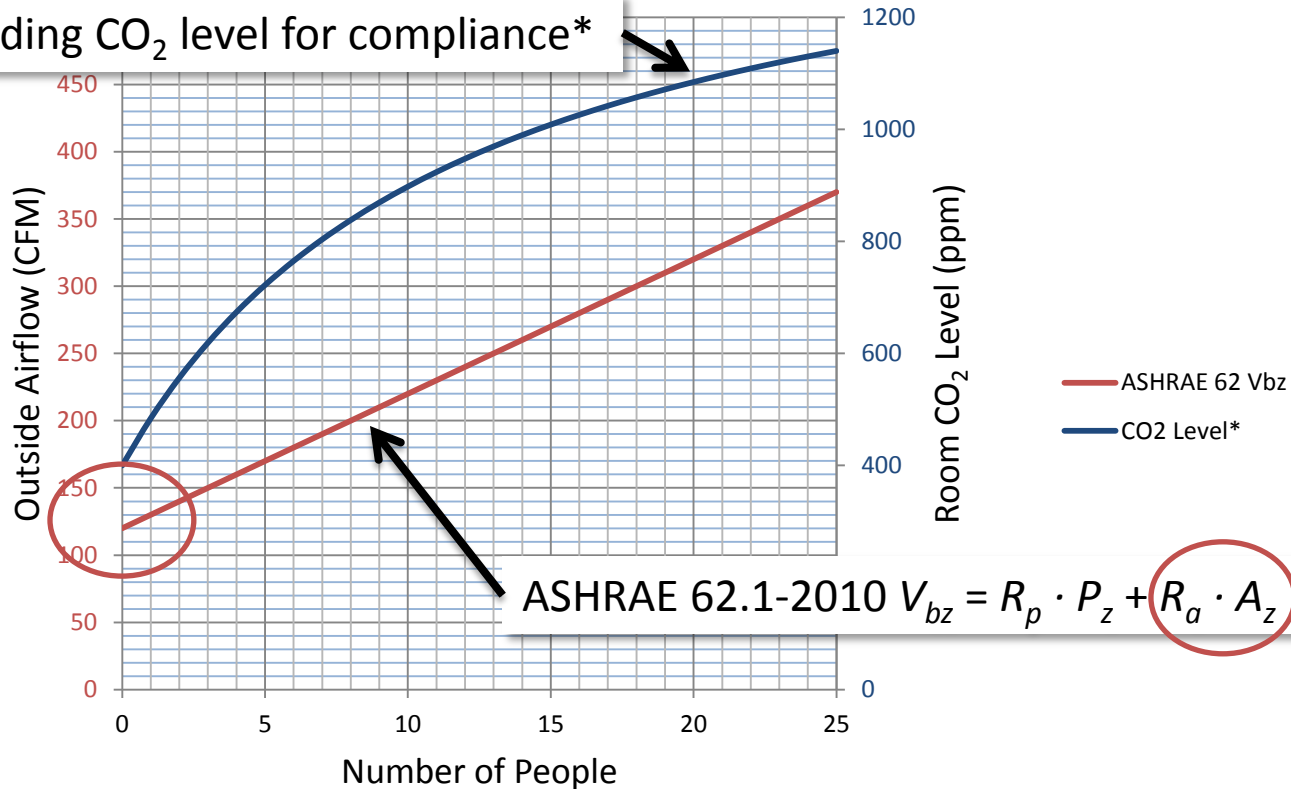


# ASHRAE 62.1 Requirements

## CO<sub>2</sub> DCV (1,000 sq.ft. classroom)

\*Assumptions: Steady-state, N=10,951, OA CO<sub>2</sub>=400ppm, no sensor error or bias

Corresponding CO<sub>2</sub> level for compliance\*

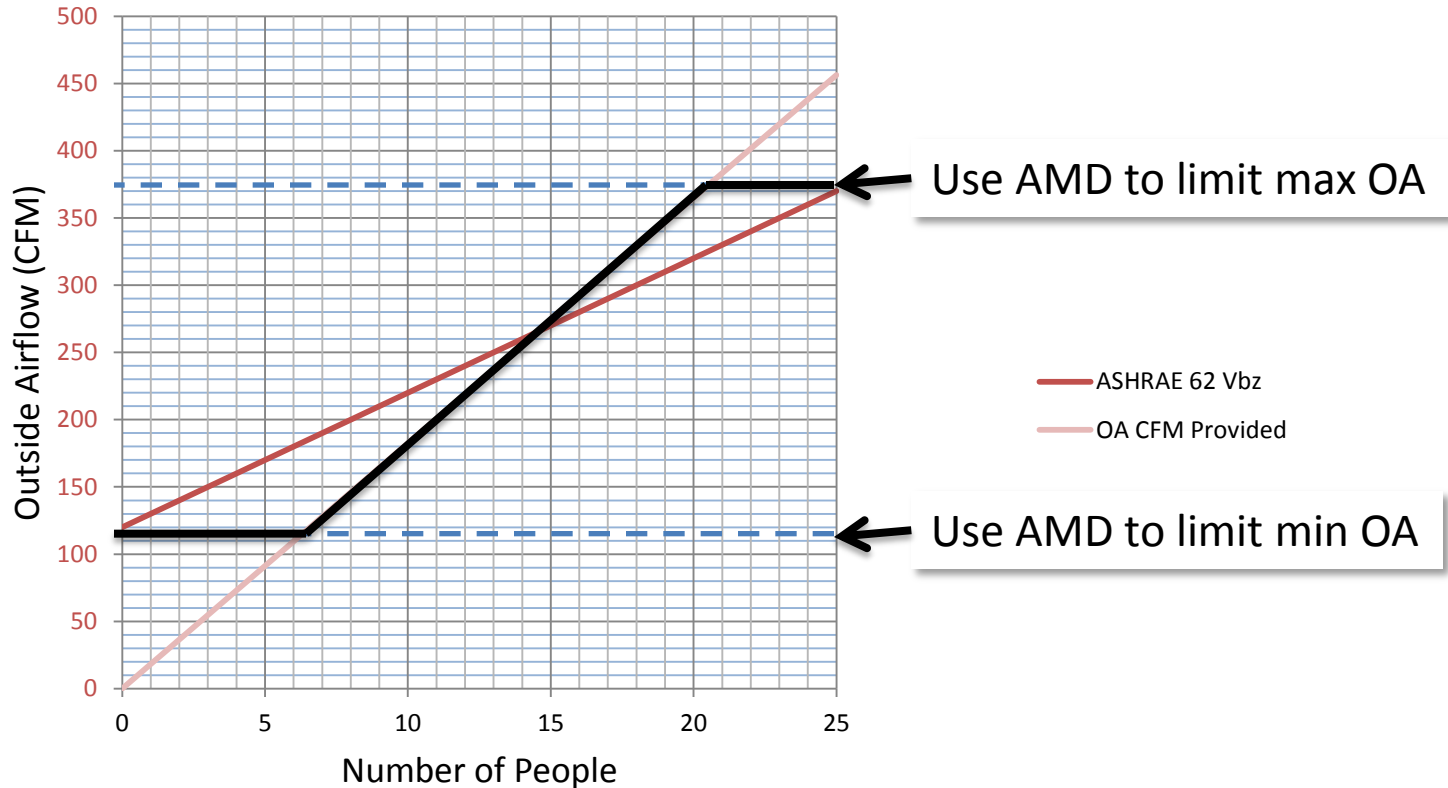


# OA AMD/CO<sub>2</sub> DCV

Reset OA airflow setpoint to maintain space CO<sub>2</sub> level

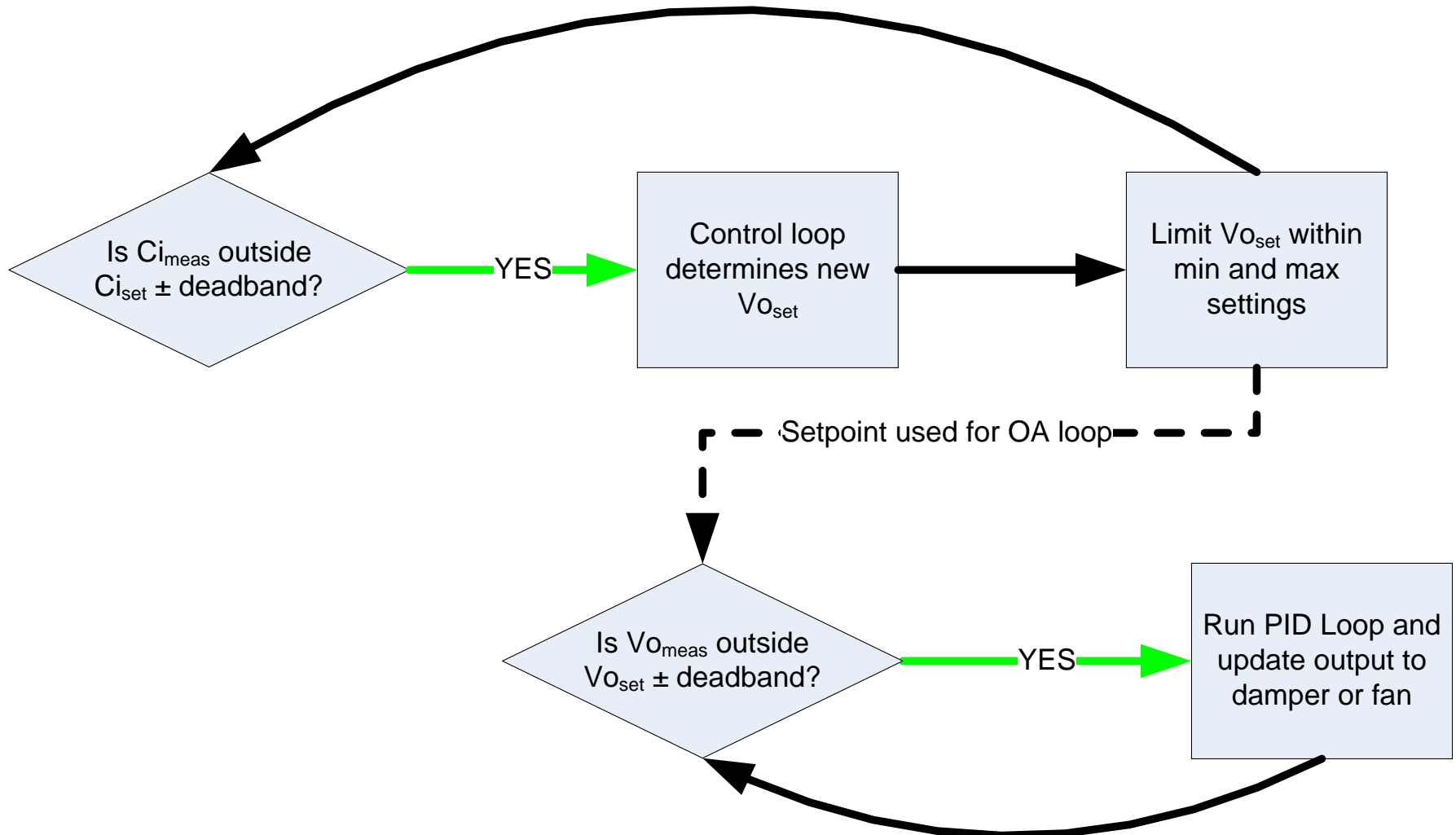
CO<sub>2</sub> DCV (1,000 sq.ft. classroom)

\*Assumptions: Steady-state, N=10,951, OA CO<sub>2</sub>=400ppm, no sensor error or bias



# OA AMD/CO<sub>2</sub> DCV

Reset OA airflow setpoint to maintain space CO<sub>2</sub> level



# ASHRAE 62.1-2010

(Includes Addenda a, c, d, and e to 62.1-2010 published in the 2011 Supplement to 62.1-2010)

## DCV - 100% OA Systems

*Multi-zone with single zone recirculating systems, radiant panels or chilled beams (not valid on multi-zone recirculating systems).*

### What's needed?

1. Real-time population estimate of **each** zone ( $P_z$ )
2. Damper (or terminal box) and an airflow measuring device to measure  $V_{oz}$  at each zone.
3. Controller to calculate  $V_{oz}$  and maintain setpoint at each zone:

$$V_{oz} = \{R_p \cdot P_z + R_a \cdot A_z\} / E_z$$

Note: In most DOAS systems  $E_z = 1$  (tempered air)

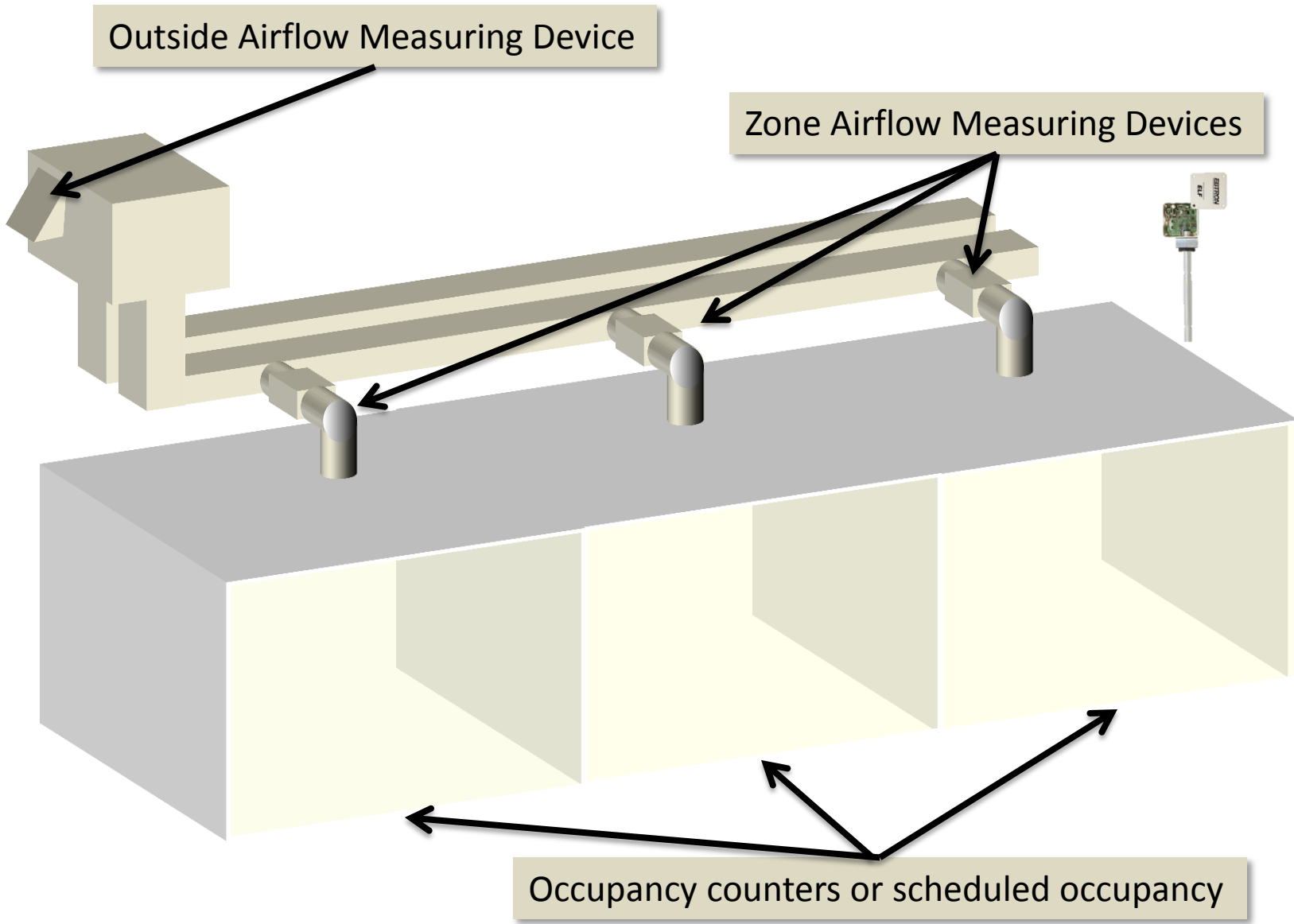
# ASHRAE 62.1-2010

(Includes Addenda a, c, d, and e to 62.1-2010 published in the  
2011 Supplement to 62.1-2010)

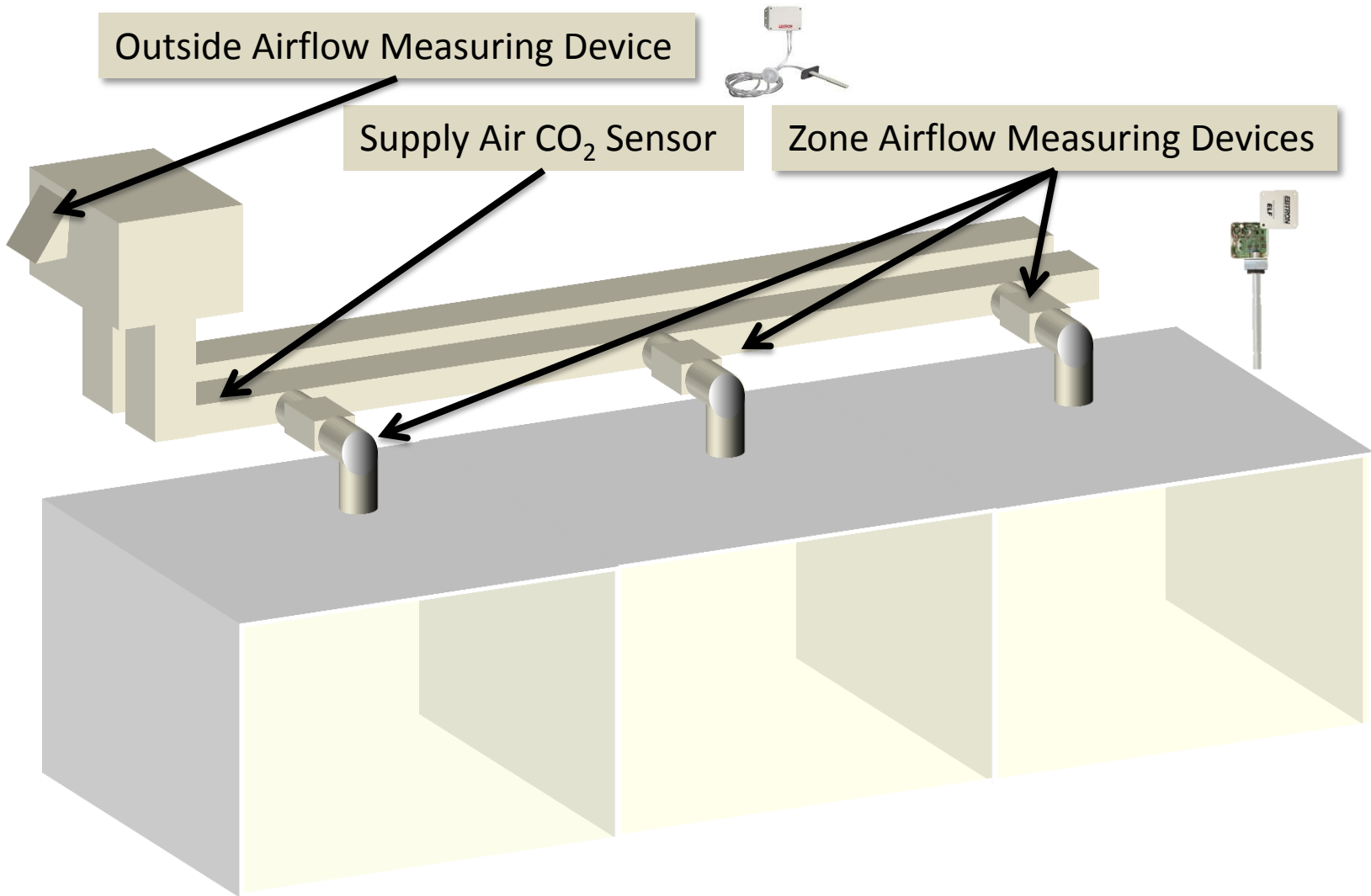
## Multi-zone Recirculating Systems

**More complicated!**

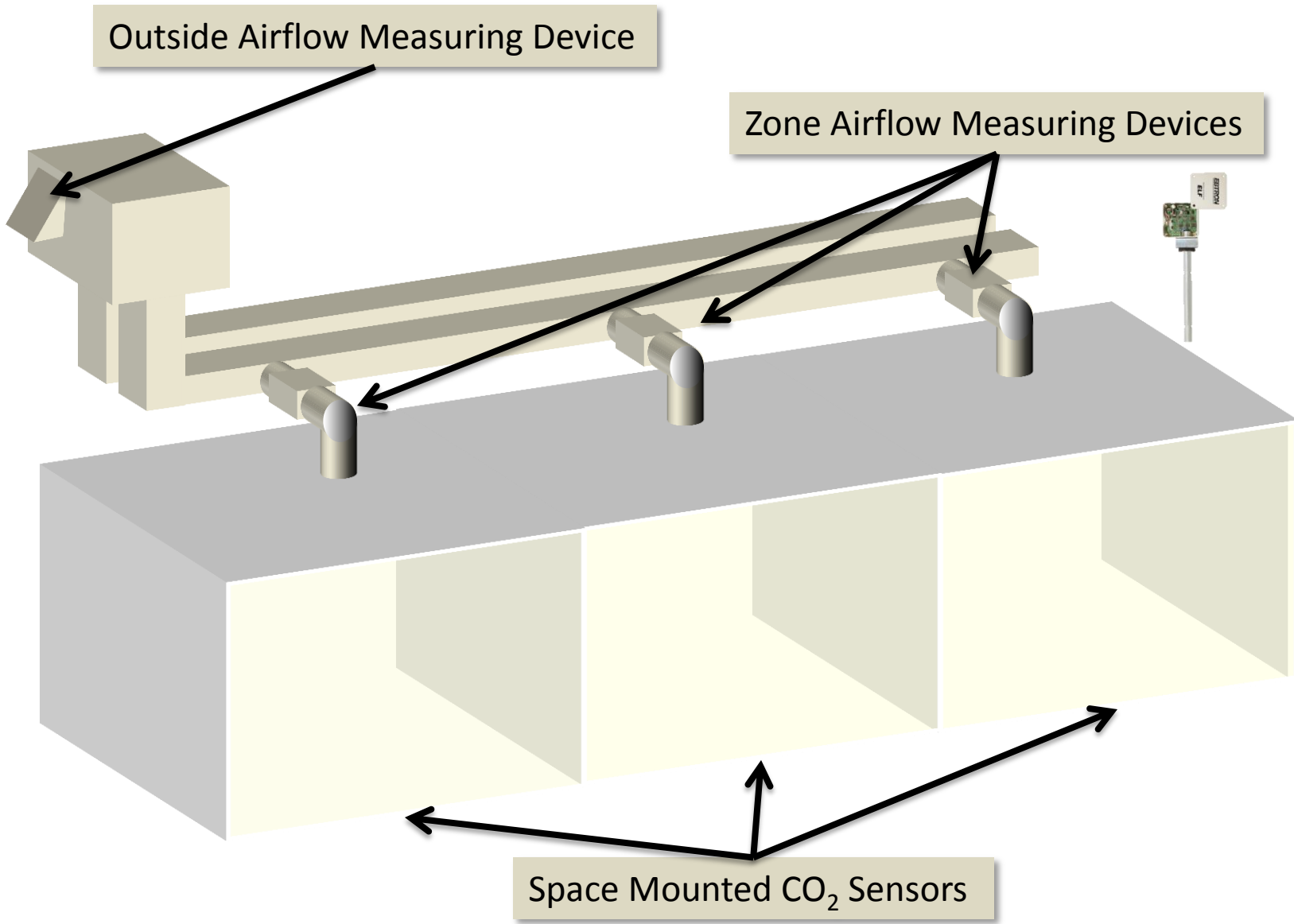
# Method #1: Counters or schedules



## Method #2: Total supply CO<sub>2</sub> / Zone Airflow

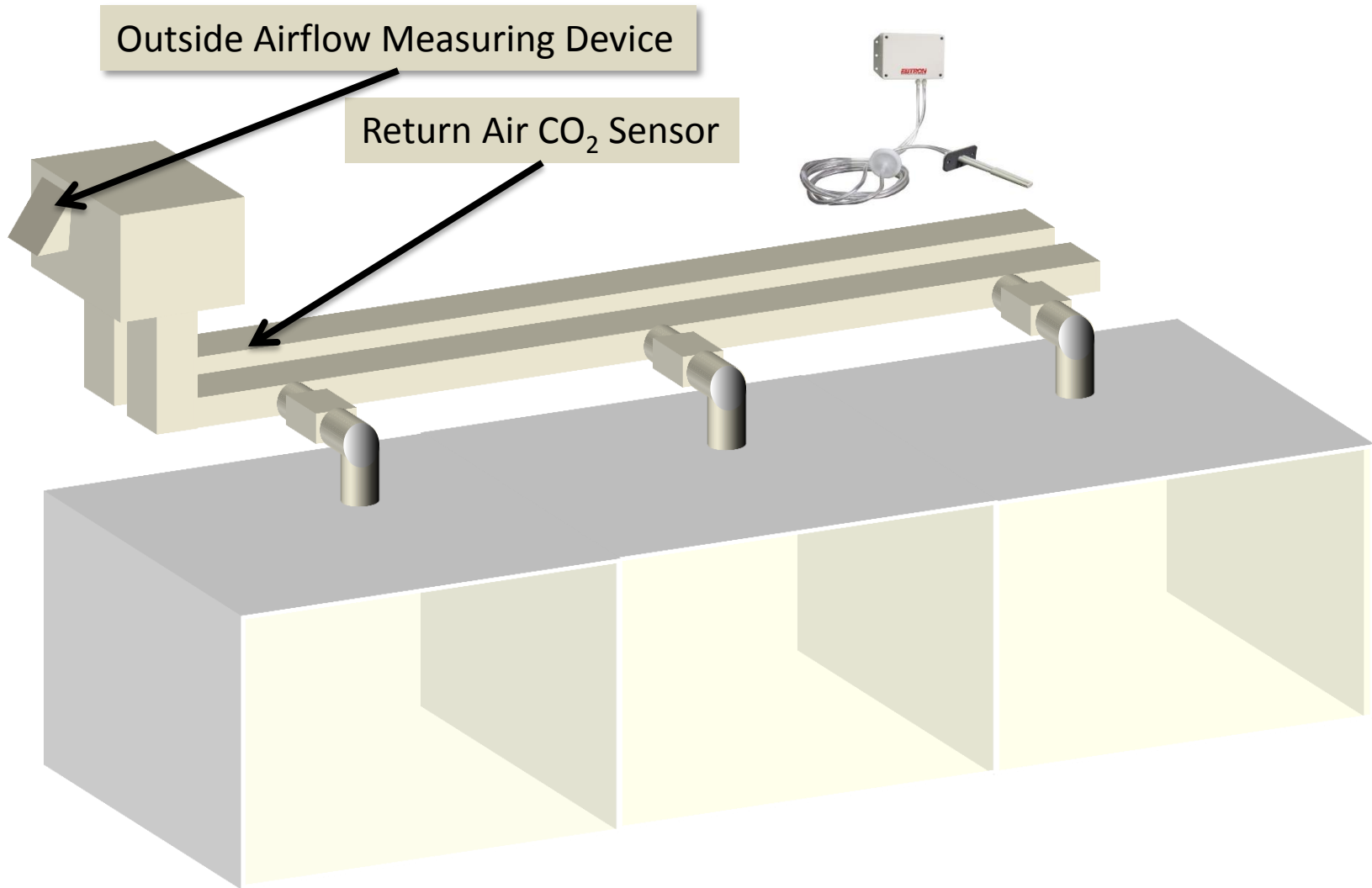


# Method #3: Space CO<sub>2</sub> / Zone Airflow

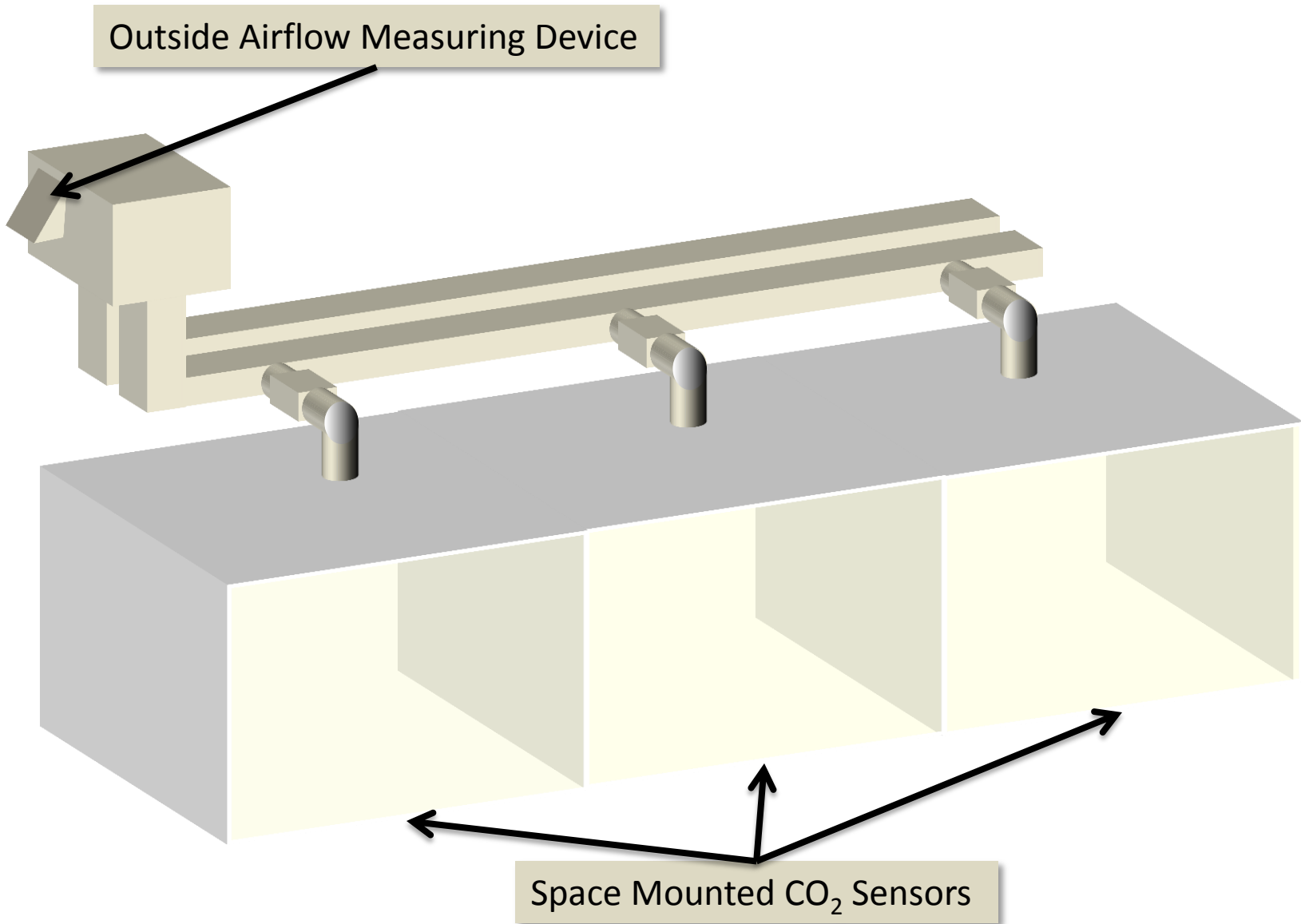




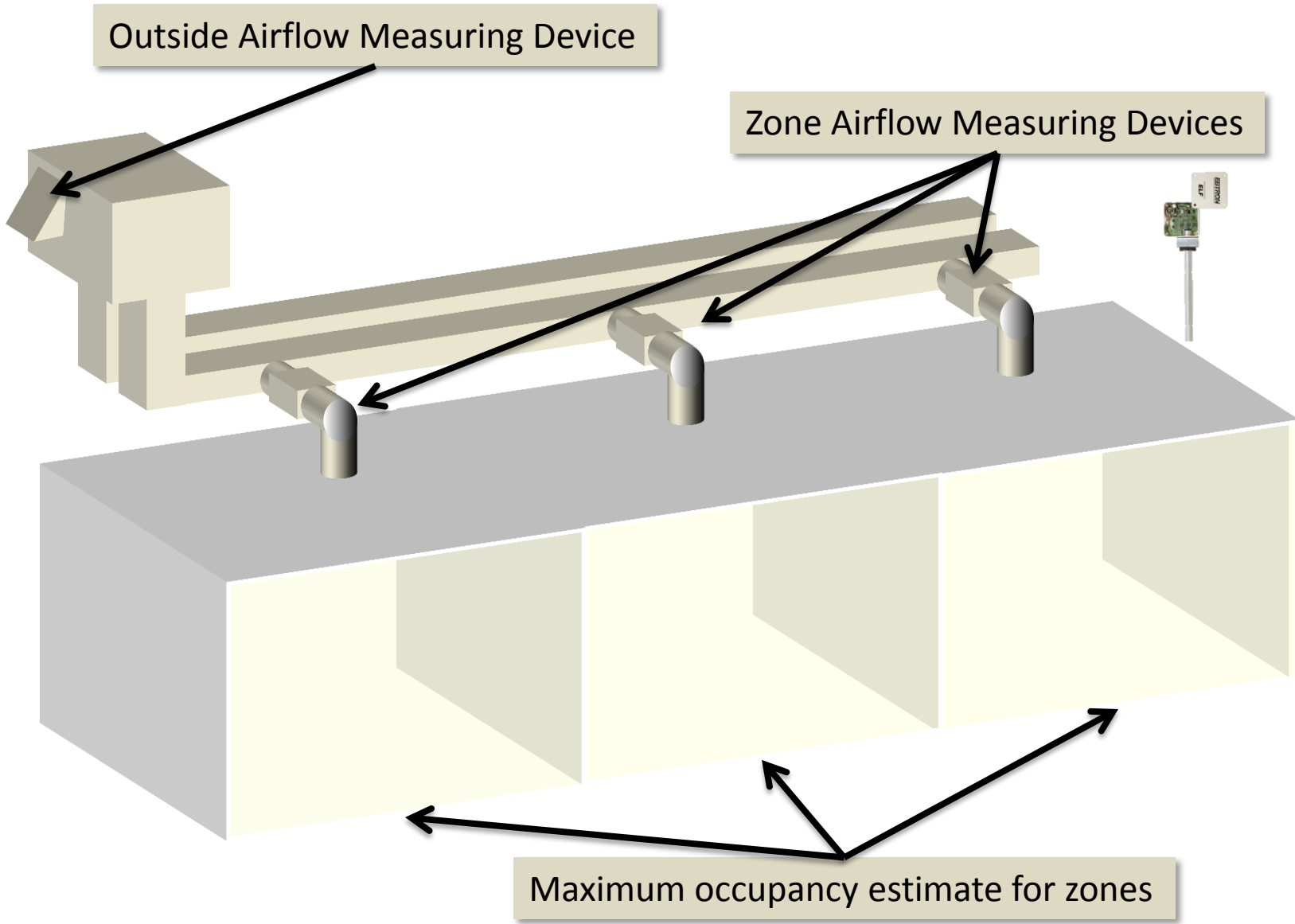
## Method #4: Maintain total return air CO<sub>2</sub> level



## Method #5: No zone to exceed specified CO<sub>2</sub> level

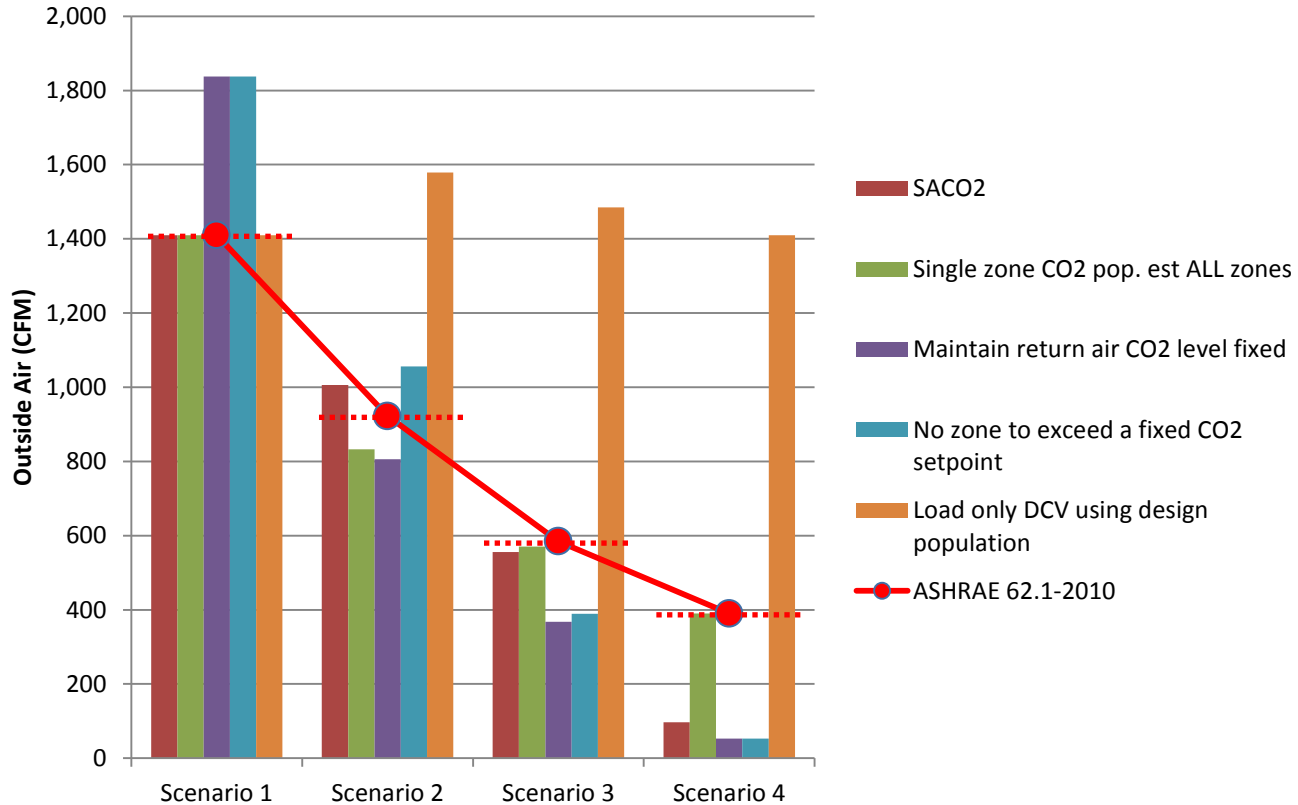


# Method #6: Zone airflow only (thermal load only DCV)



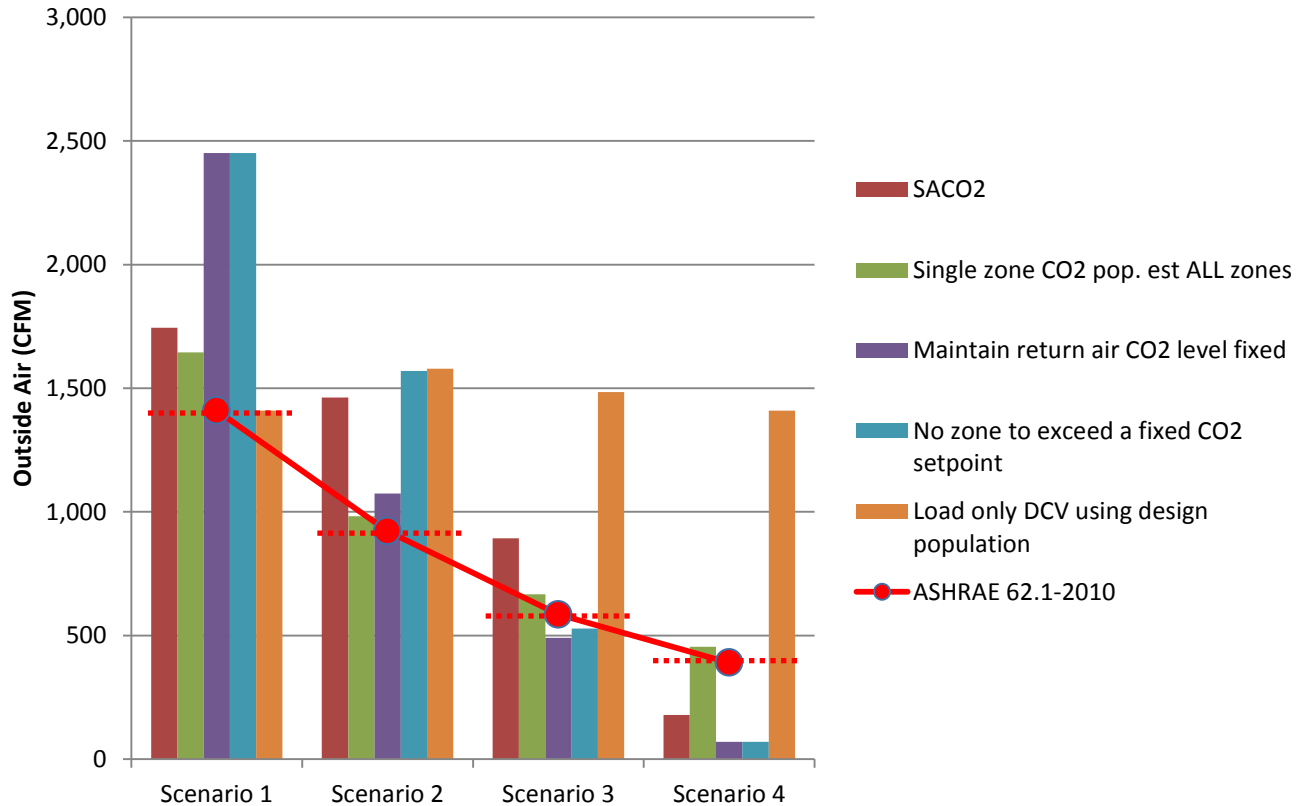
# Classroom Example

1.2 Mets, 400 ppm outside CO2, 0 ppm space CO2 sensor uncertainty



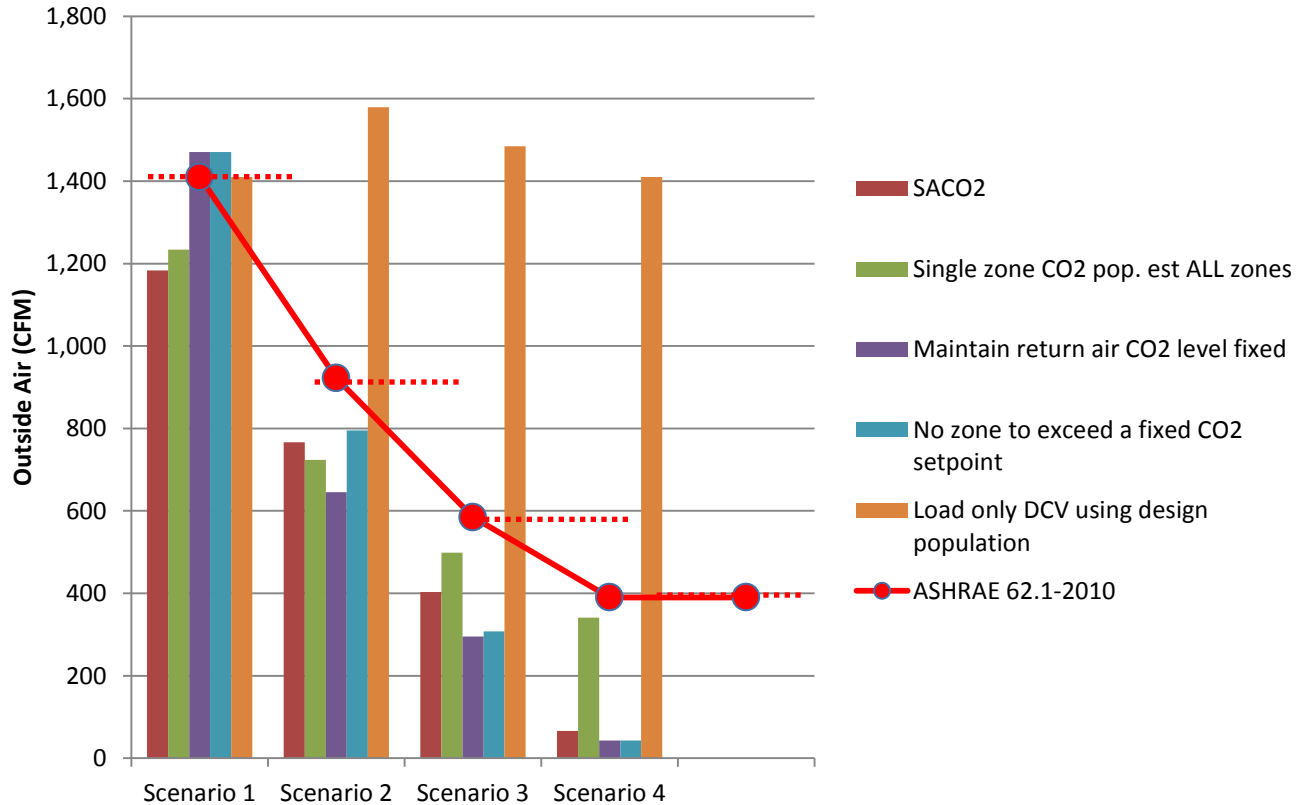
# Classroom Example

1.2 Mets, 450 ppm outside CO2, +100 ppm space CO2 sensor uncertainty



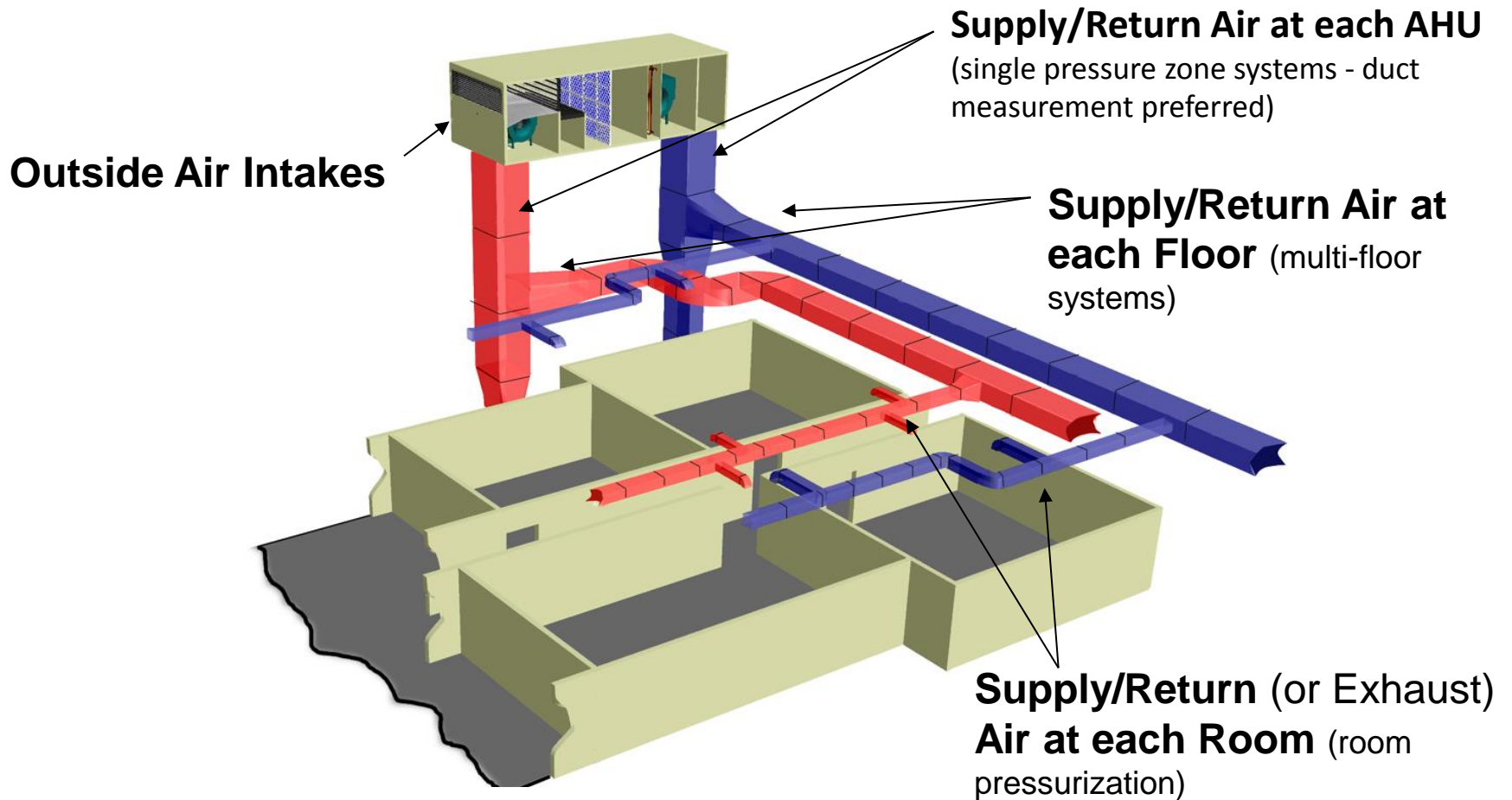
# Classroom Example

1.2 Mets, 350 ppm outside CO2, -100 ppm space CO2 sensor uncertainty



# Anatomy of a Healthy Building

## Key Airflow Measurement Locations





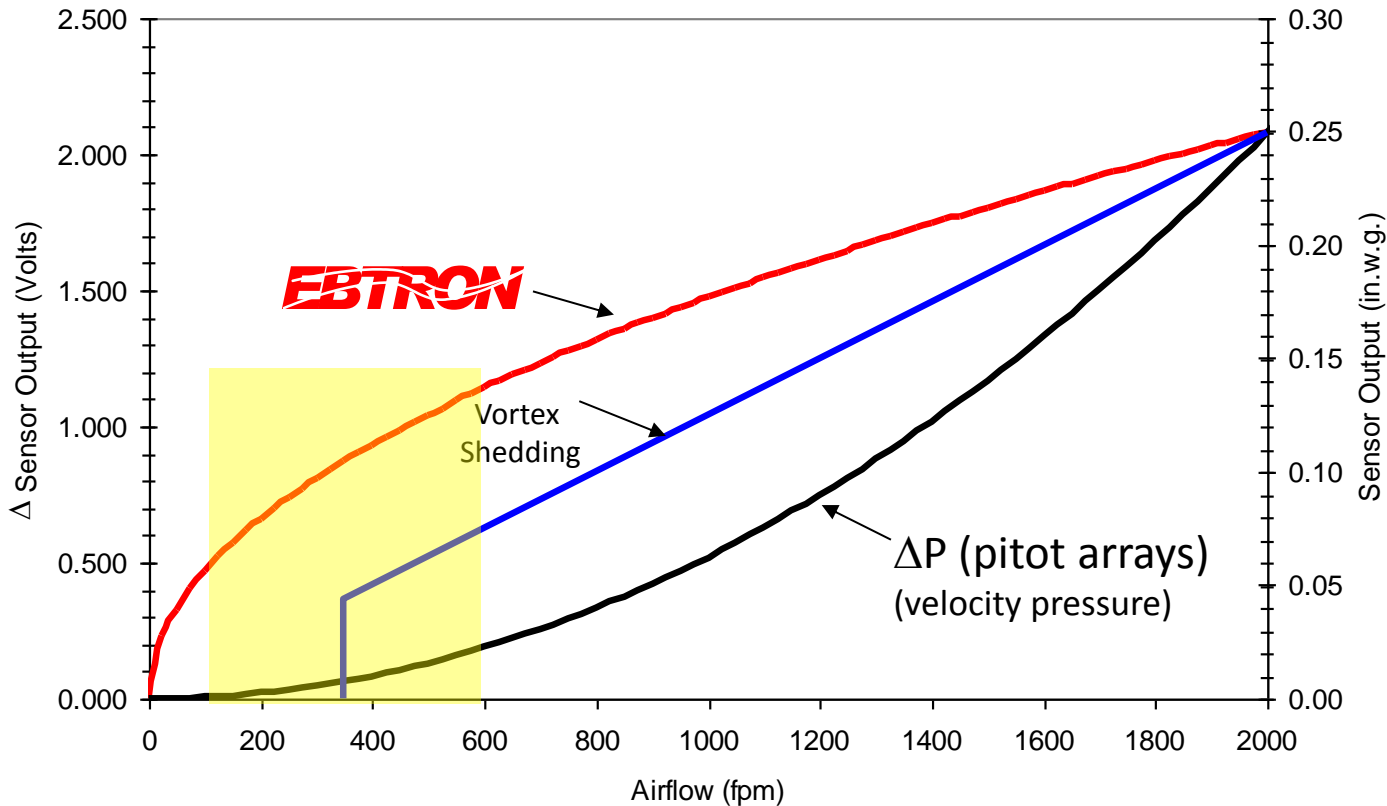
Thermal Dispersion Airflow Measurement

# Technology Comparison



# Technology Comparison

## Ebtron Signal vs. $\Delta P$ and Vortex Shedding

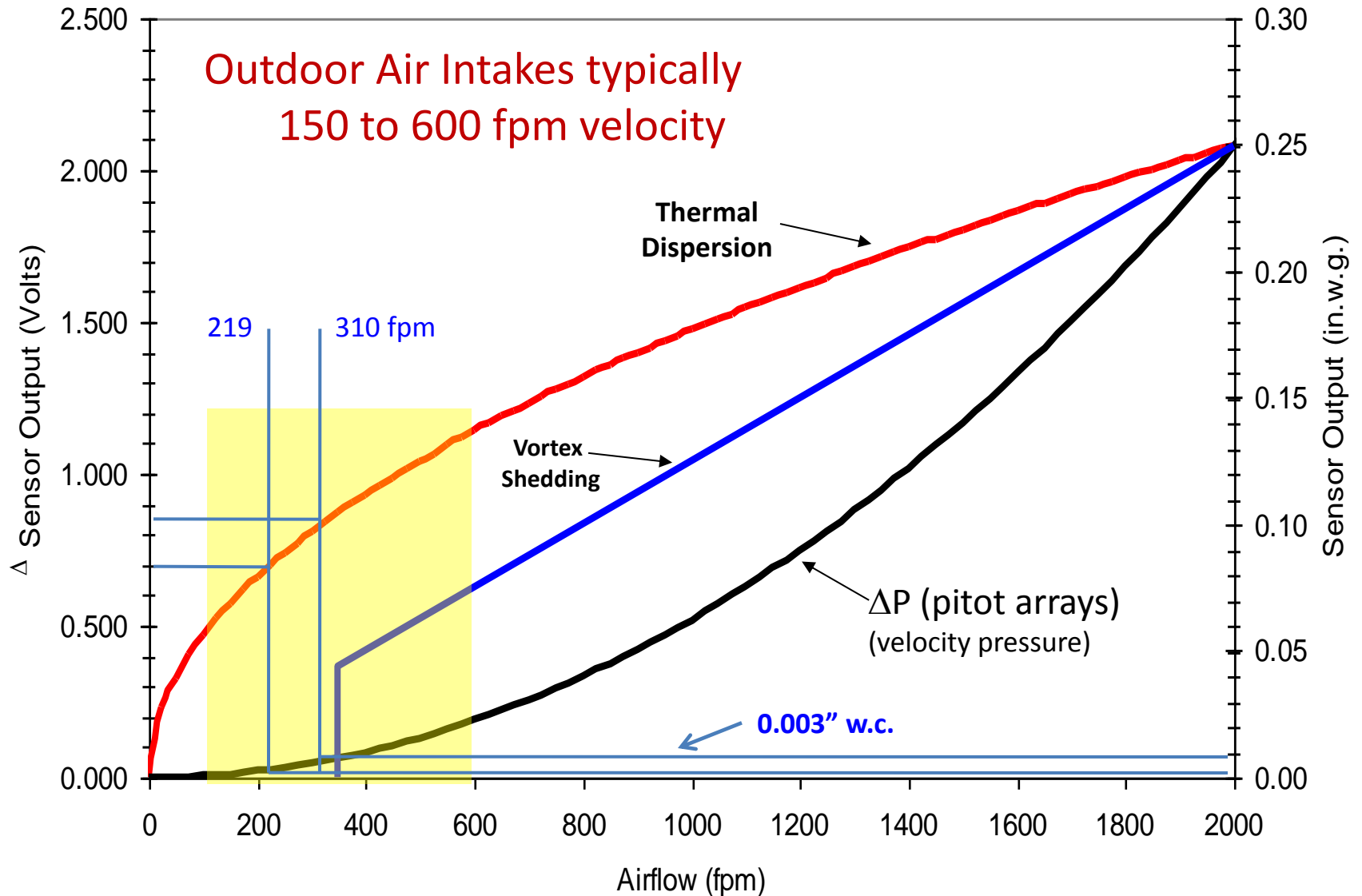


Ebtron's technology has the best sensitivity at low airflows

Outdoor Air Intakes typically 150 to 600 fpm velocity

# Technology Comparison

Thermal Dispersion has the Best Sensitivity at Low Airflows



# Pitot Tubes and Arrays



Air Monitor Corporation, FAN-E  
Averaging Pitot Array  
Stations with Honeycomb



Pitot-static Tube



Averaging Pitot Array  
Probes



Trane, Traq Damper  
Combination Pitot Array &  
Dampers



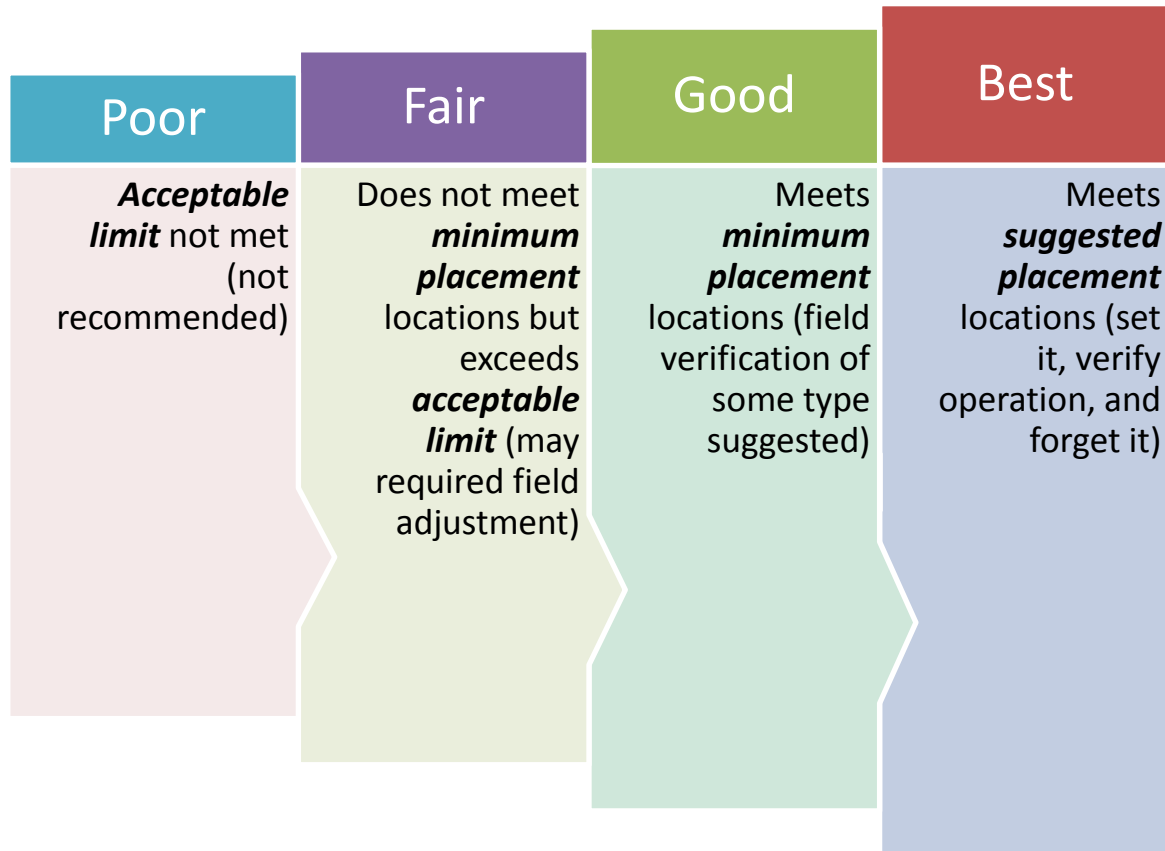
Terminal Box Flow  
Ring/Cross



Ruskin, IAQ-50  
Combination Pitot  
Array/Damper with  
Honeycomb

**EBTRON** a measurable difference!

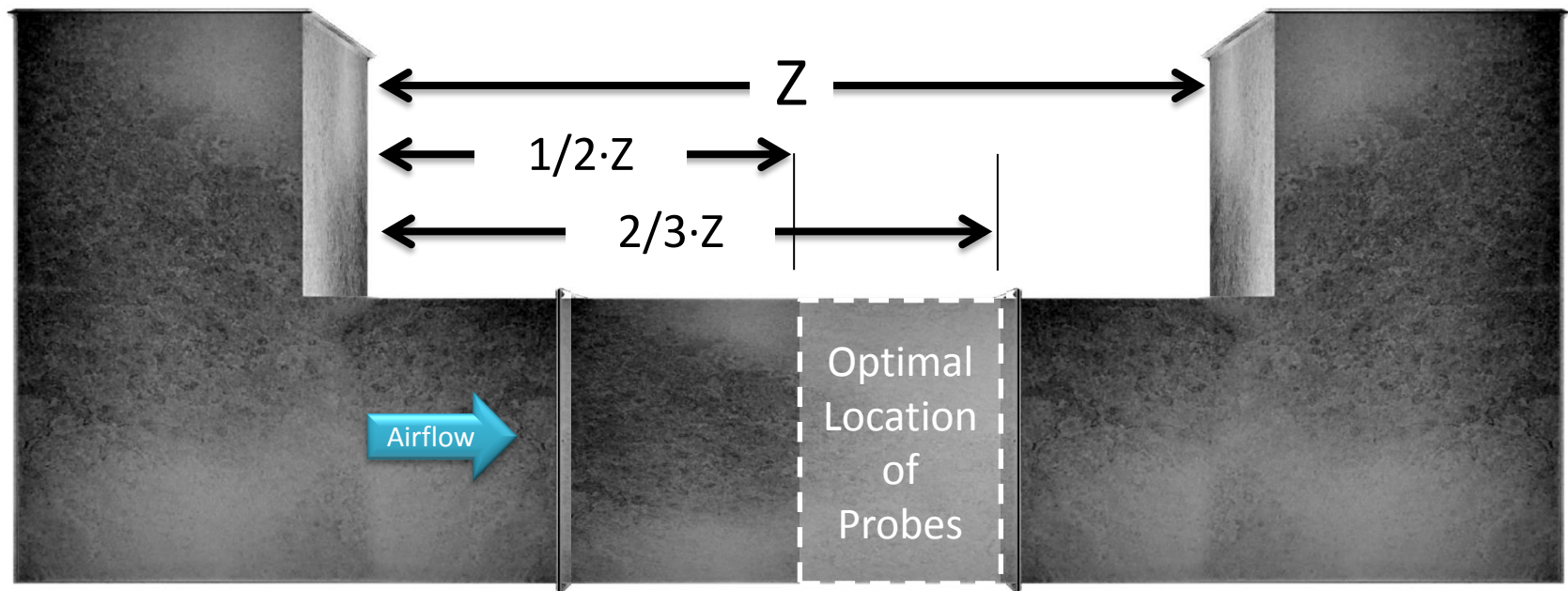
# Application Assessment



**EBTRON** a measurable difference!

# Go: Where to place probes

## Between Duct Fittings

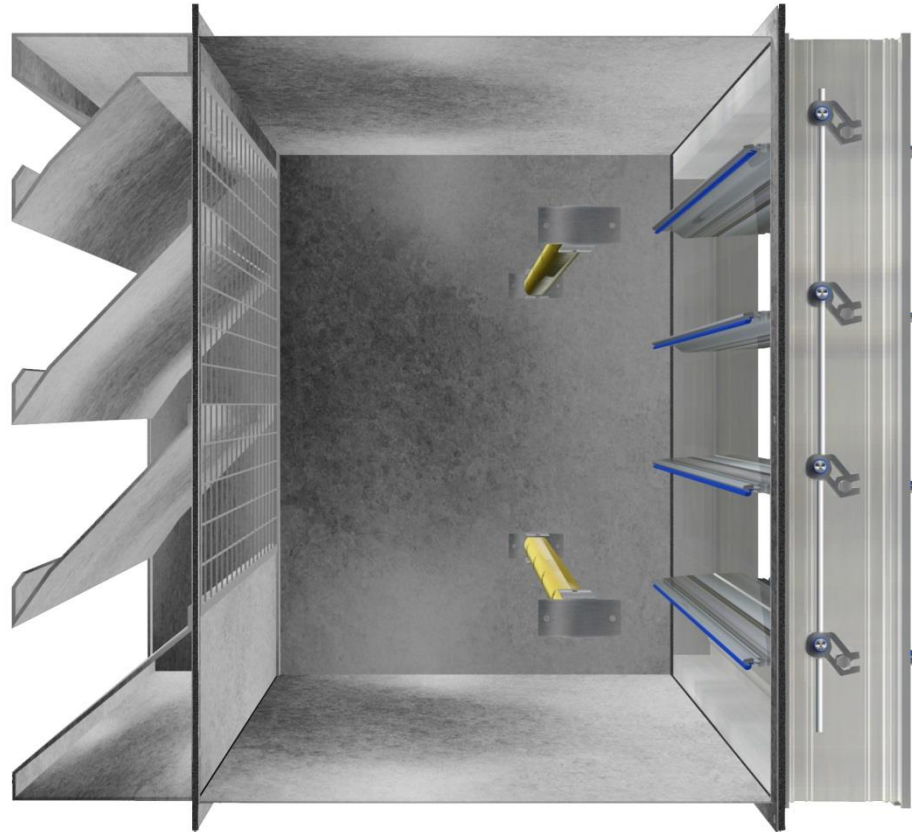


$Z$  is in multiples of equivalent diameters  $(L + W)/2$  based on up and downstream disturbances in ducted systems

**EBTRON** a measurable difference!

# Go: Where to place probes

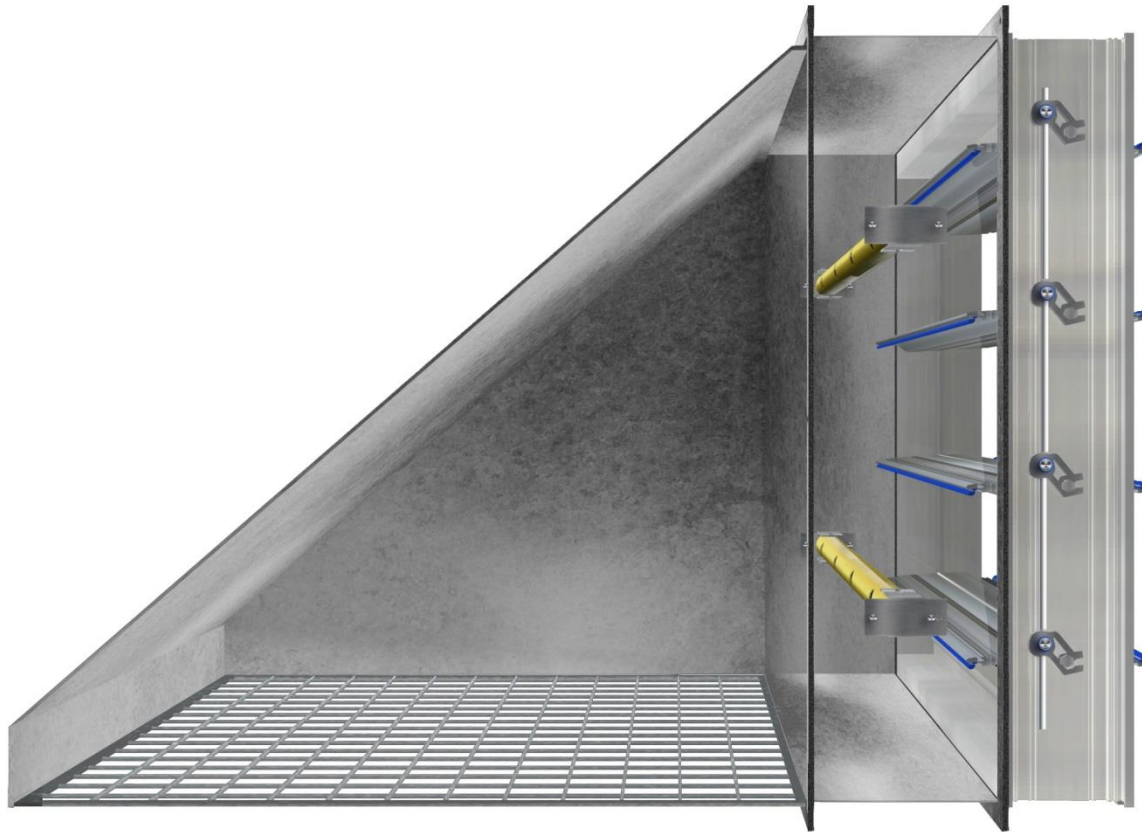
Outside Air Intake Applications



**EBTRON** a measurable difference!

# Go: Where to place probes

Outside Air Intake Applications



**EBTRON** a measureable difference!

The Real-world: Locating Probes

# What to expect for “Best”

Best

Meets  
**suggested  
placement**  
locations (set  
it, verify  
operation, and  
forget it)

- Field adjustment is NOT recommended
- Look for system/verification issues if verification techniques indicate inaccuracy
- “Out-of-the-box” installed accuracy should be equal to or better than  $\pm 3\%$  of reading



**EBTRON** a measureable difference!

The Real-world: Locating Probes

# What to expect for “Good”

Good

Meets  
**minimum  
placement**  
locations (field  
verification of  
some type  
suggested)

- Field adjustment should not be required in most cases
- “Out-of-the-box” installed accuracy should approach or equal  $\pm 3\%$  of reading (3 to 5% for outside air intakes close coupled to louvers or hoods)

**EBTRON** a measureable difference!

The Real-world: Locating Probes

# What to expect for “Fair”

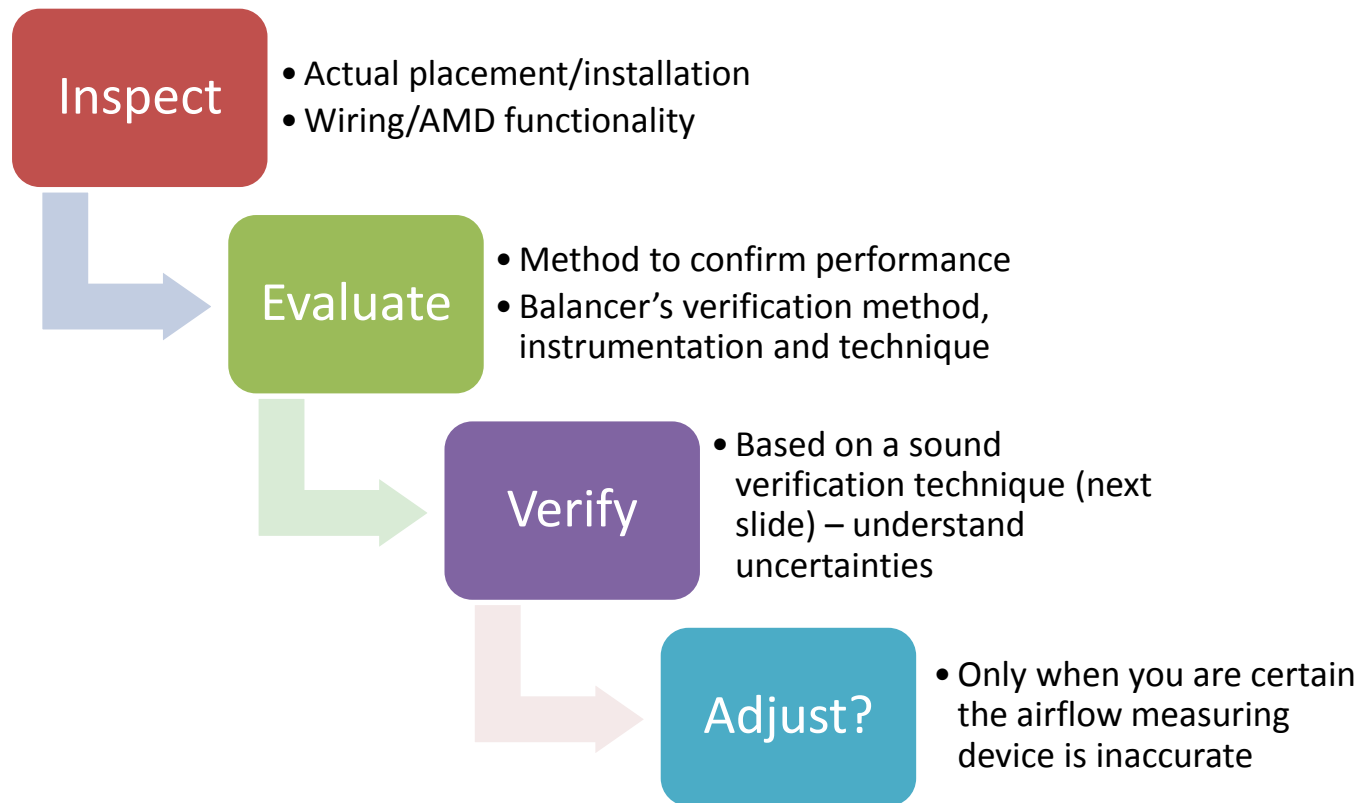
## Fair

Does not meet **minimum placement** locations but exceeds **acceptable limit** (may required field adjustment)

- AMD can be field adjusted, if airflow rate verification warrants, to fulfill the requirements of most applications
- Verification should be done at two airflow rates for variable air speed applications or one point for single air speed applications
- Reading may fluctuate more than in Good or Best locations but the average should be reliable.
- No statement of “out-of-the-box” installed accuracy can be made

**EBTRON** a measurable difference!

# Startup



**EBTRON** a measureable difference!

# Verification Methods

## Best

- Compare to EBTRON in closed loop (requires low leakage dampers)

## Good

- Compare to EBTRON in same path (requires low leakage dampers)
- Compare to calibrated handheld equipment at airflow rates and locations suitable for the device

## Fair

- Compare to sum of calibrated handheld equipment or hoods at multiple locations at airflow rates and locations suitable for the device

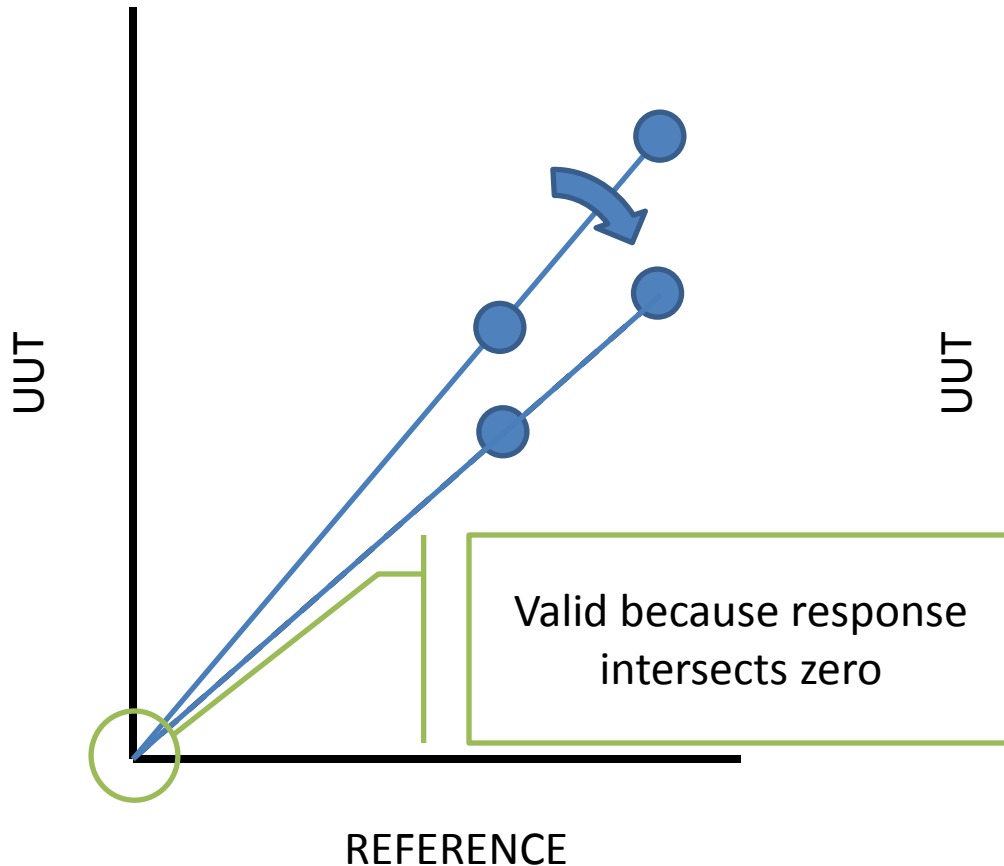
## Poor

- Compare to improperly applied or calibrated handheld instruments
- Compare to fan curves based on fan speed and pressure drop
- Compare to temperature mixing methods (OA)

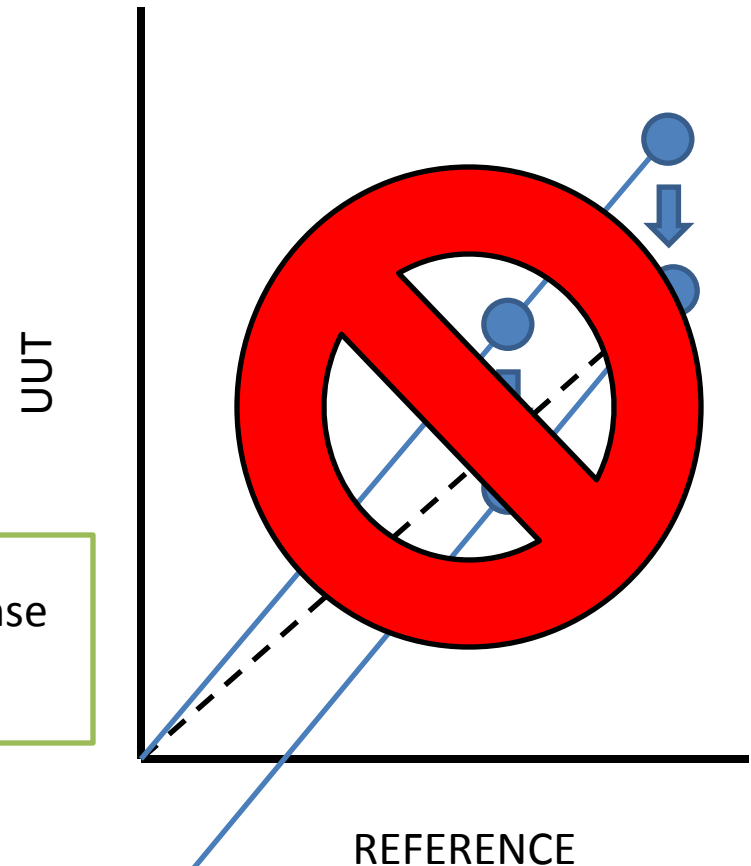
**EBTRON** a measurable difference!

# When you must adjust

One-point Gain Adjustment



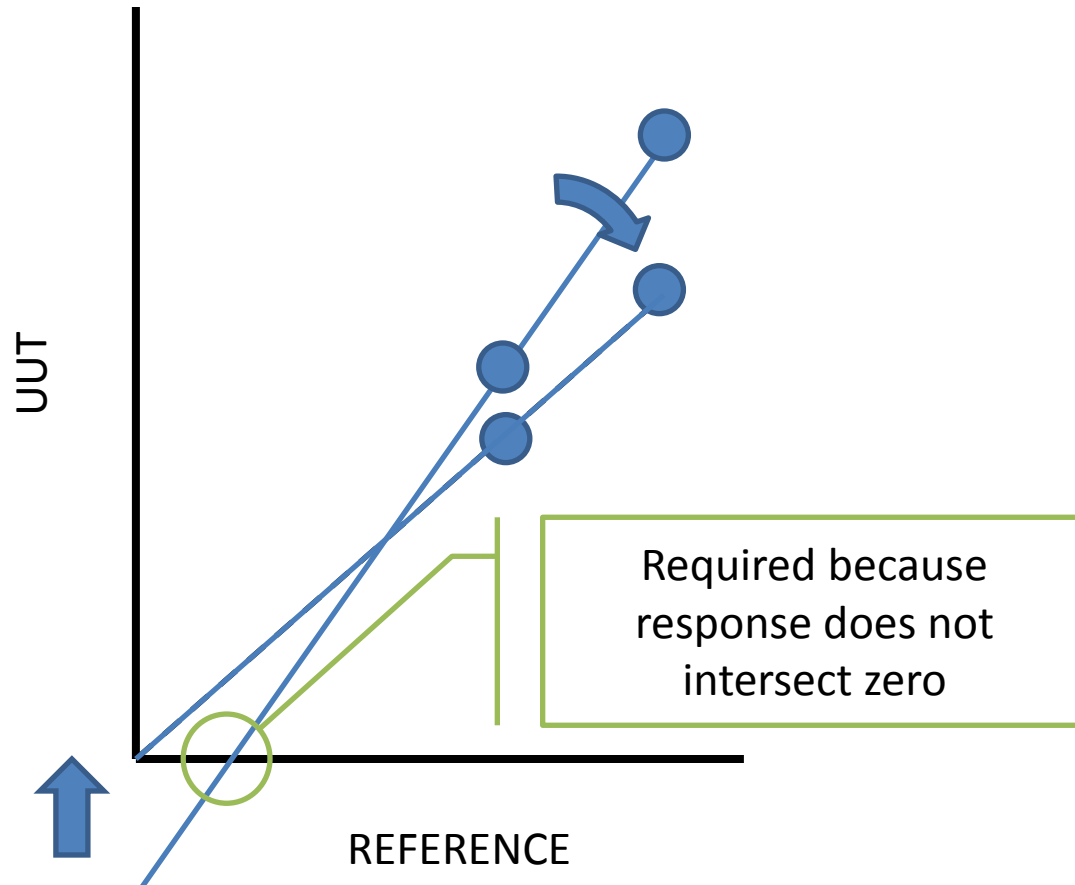
One-point Offset Adjustment



**EBTRON** a measurable difference!

# When you must adjust

Two-point Offset-Gain Adjustment



**EBTRON** a measurable difference!

# Making Adjustments

## Field-cal Wizard (Gold & Hybrid)

- Transmitter prompts user for one or two point adjustment. Reference airflow rates are directly entered in transmitter by user when measurements are taken. Transmitter samples and automatically makes offset/gain calculations.

## Enter Slope and Intercept (Gold & Hybrid)

- Slope and intercept calculated by user is entered in transmitter.

## Live Adjustment (Gold and Hybrid)

- Pushbutton offset/gain adjustments are made in real-time by comparing reference airflow rates to LCD output.

## At Host Control System (Gold, Hybrid or ELF)



Thermal Dispersion Airflow Measurement

# Why Choose Ebtron?



# Ebtron History

- Leader in commercial HVAC airflow measurement for 25+ years
- Introduced our first microprocessor-based thermal dispersion airflow meter in 1986
- Moved to Loris, SC (20 mi from Myrtle Beach) in 1994
- Advantage product line introduced in 2001
- ~75 employees and a 5 building campus
- 80+ representatives



# Ebtron = Support & Training

- Our Representatives – excellent pre-sale & post-sale support
- Factory Support
  - Tested, Proven Installation Guidelines
  - Application Assistance (Inside Sales)
    - Review building drawings & recommend products & placement upon request
    - Review all incoming orders over \$5K
  - Dedicated Technical Support Group
- Product Performance & Reliability
- Industry-Leading Educational Programs
  - ‘Bring-A-Guest’ Seminars
  - ‘Lunch & Learns’
  - Webinars



# **EBTRON** a measureable difference!

## Accuracy

- True *percent-of-reading* airflow accuracy from 0 to 5,000 FPM
- NIST traceable 16 point airflow & temperature calibration
- Highest sensor density of any airflow measurement device

## Stability

- Superior bead-in-glass thermistor probes (waterproof design)
- Microprocessor-based transmitters with high performance ADC
- Industrial rated integrated circuits and gold plated interconnects

## Reliability

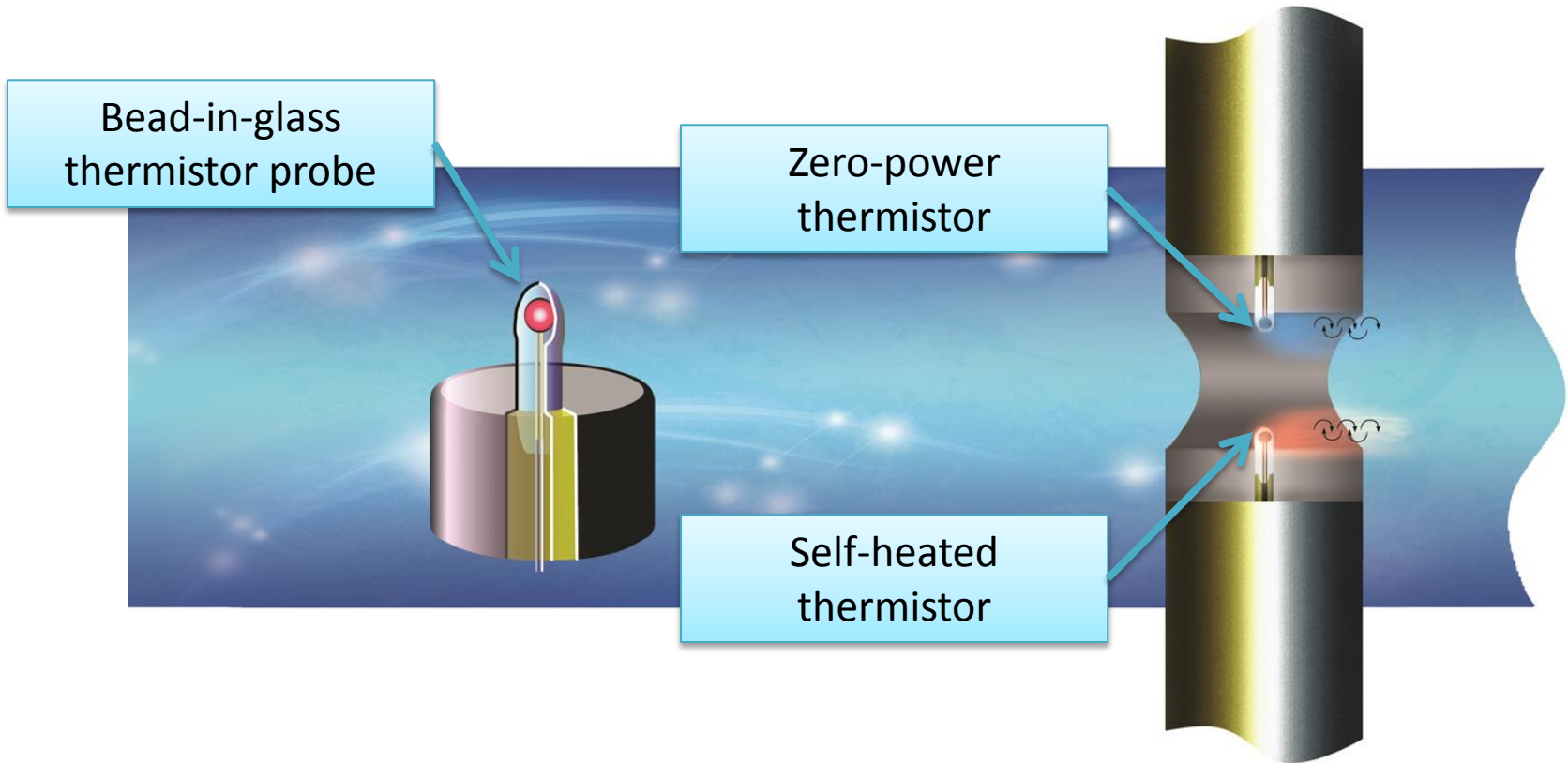
- Watchdog timer circuitry
- Fused and protected power and signal circuitry
- UL and BTL tested and listed – 3 year standard warranty

## Connectivity

- Isolated analog, RS-485, Ethernet and Lon output options
- Combination output cards on Gold Series transmitters
- Airflow, velocity weighted temperature and alarm outputs

# EBTRON Thermal Dispersion Technology

Power  $\rightarrow$   $Q = \frac{\kappa A}{d} \left[ B + C \left( \frac{\rho v d}{\mu} \right)^m (T_H - T_A) \right]$  Velocity  $\Delta T$





# performance matters!

## EBTRON Standard

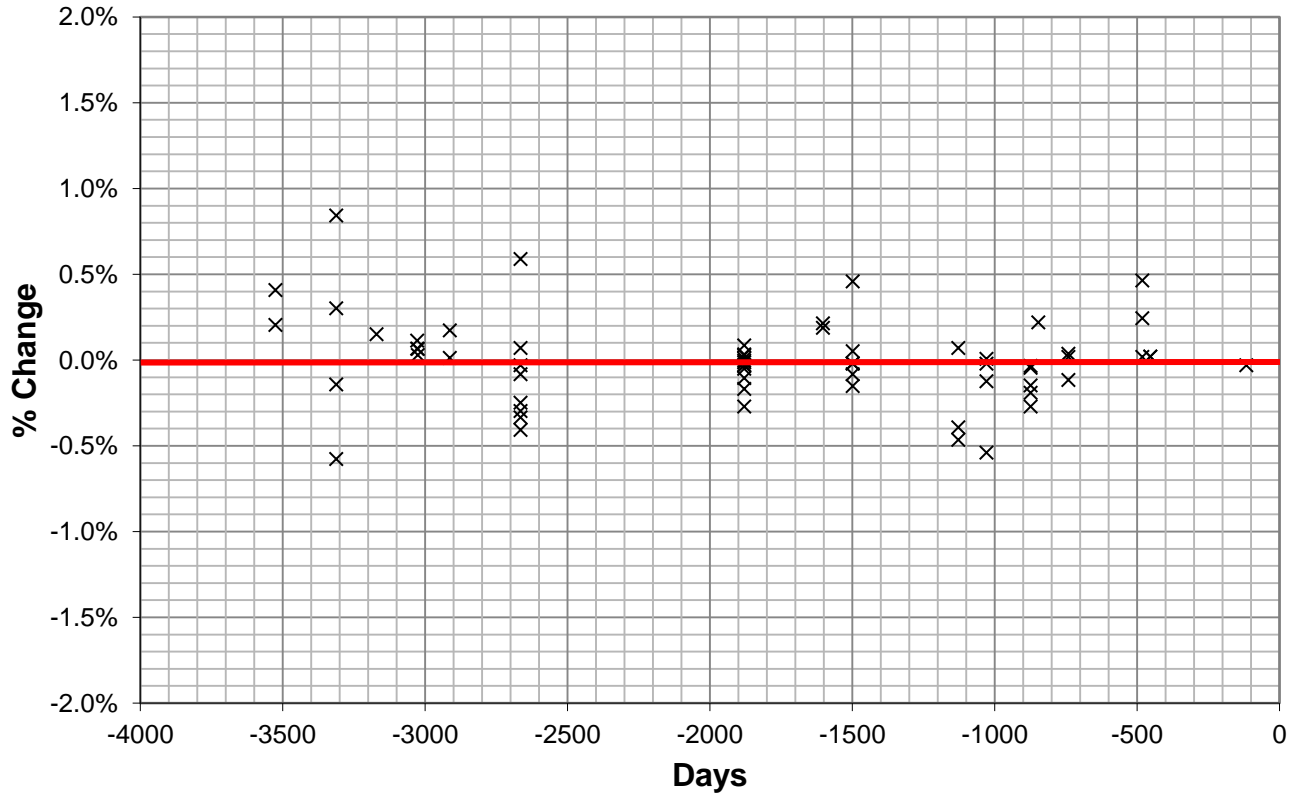
NIST Airspeed (VNIST), [fpm]	IUT Output (VIUT), [fpm]	Expanded Uncertaint y, [%]
115.92	116.03	1.43
175.58	175.83	1.09
219.59	219.83	0.81
268.35	266.31	1.18
316.32	314.61	1.03
366.59	365.41	0.82
419.39	417.92	0.76
462.72	462.39	0.67
506.95	506.91	0.71
744.49	743.96	0.68
1035.1	1033.5	0.73
1190.7	1187.8	0.67
1438.0	1434.1	0.67
1772.5	1765.7	0.65
2050.1	2040.6	0.64
2488.3	2476.0	0.64
2986.9	2975.0	0.67
3382.5	3367.2	0.68
3984.5	3963.2	0.70
4988.1	4959.6	0.67
5990.8	5965.3	0.88
6979.2	6941.6	0.87
7993.3	7937.7	0.65

## Typical Production Unit Calibration Report

Ref	UUT	Error	Error%	
0	0.00	-0.01		
1	116.89	117.18	0.3	0.3%
2	157.40	157.34	-0.1	0.0%
3	227.43	227.89	0.5	0.2%
4	333.64	331.39	-2.3	-0.7%
5	453.03	447.86	-5.2	-1.1%
6	577.73	574.96	-2.8	-0.5%
7	740.80	737.85	-3.0	-0.4%
8	943.69	940.25	-3.4	-0.4%
9	1153.84	1165.31	11.5	1.0%
10	1414.55	1402.48	-12.1	-0.9%
11	1678.59	1687.86	9.3	0.6%
12	2024.89	2008.12	-16.8	-0.8%
13	2409.37	2399.48	-9.9	-0.4%
14	3342.61	3340.49	-2.1	-0.1%
15	4941.23	4923.32	-17.9	-0.4%

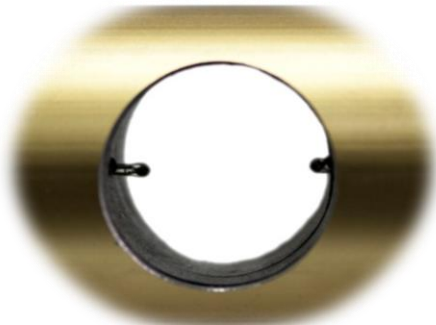
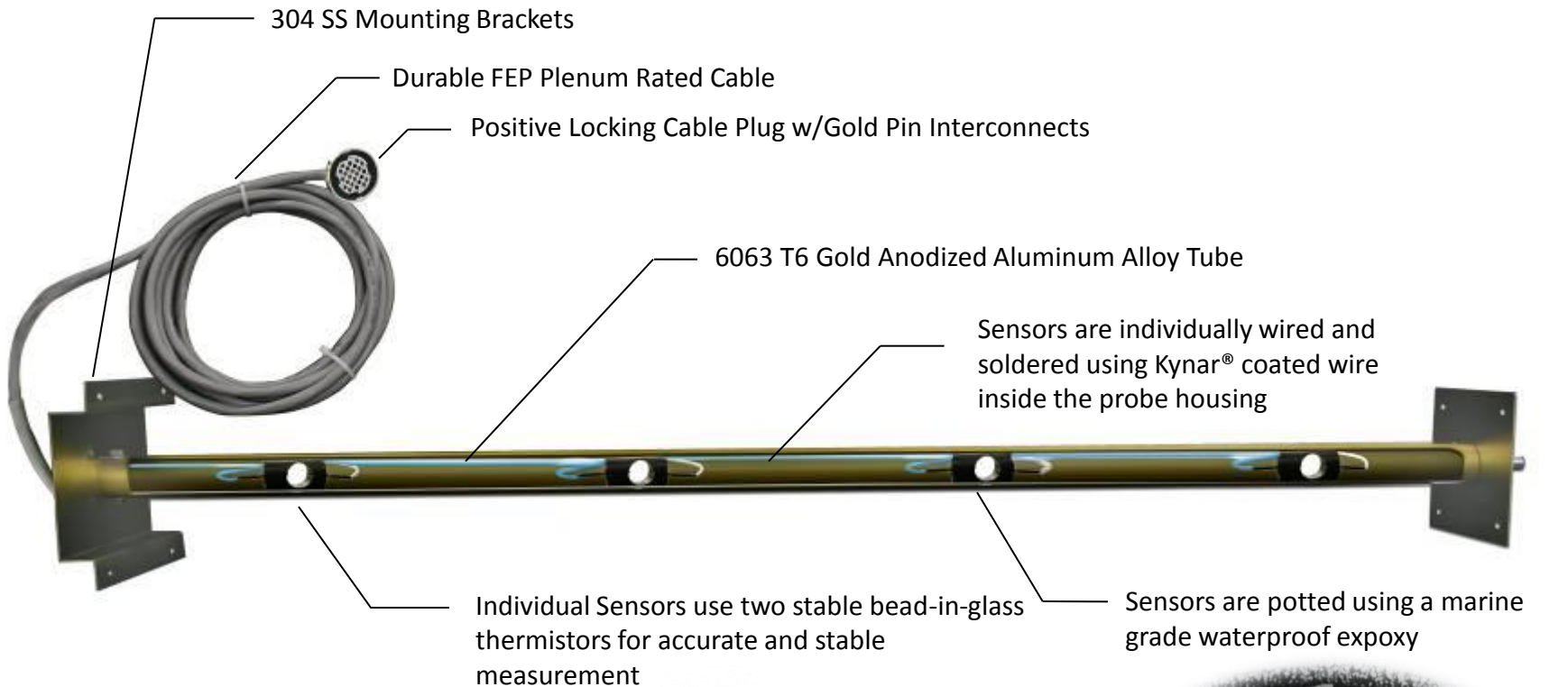
# EBTRON long term stability!

EBTRON Bead-in-glass Thermistor  
Long term stability



**EBTRON** the **GOLD** standard!

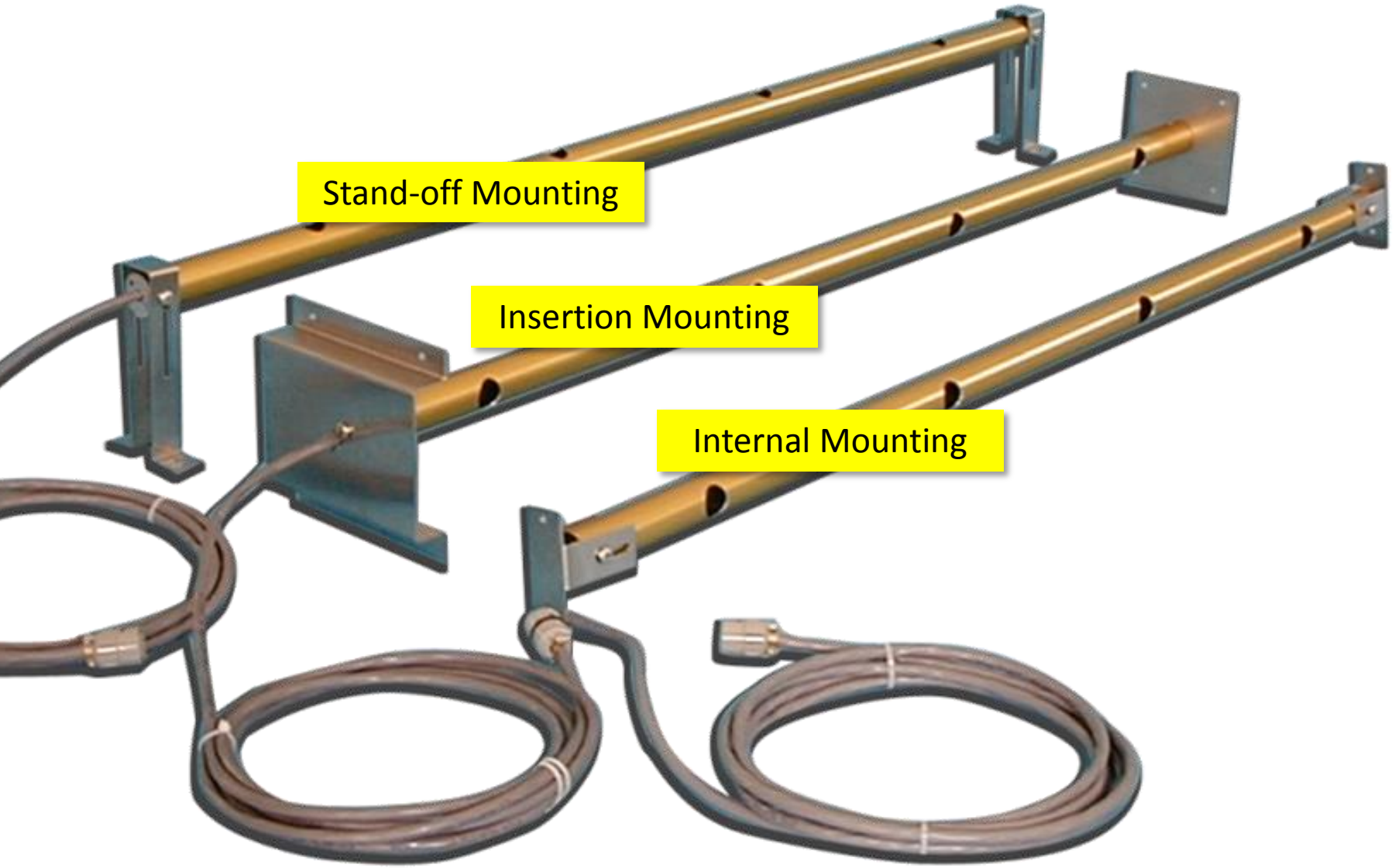
# GTx116-P Duct & Plenum Probes





**EBTRON** the **GOLD** standard!

## GTx116-P Flexible Mounting Options





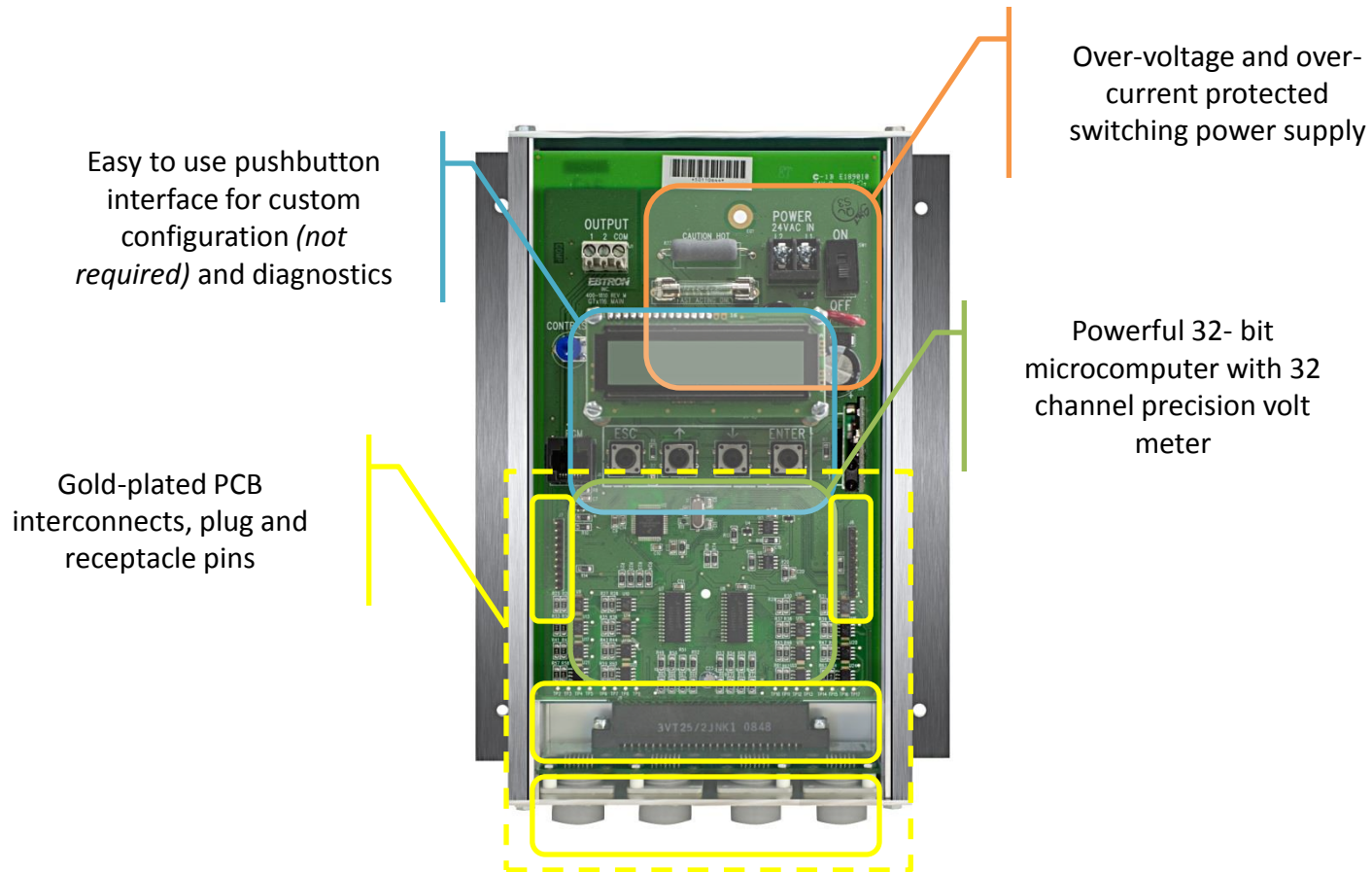
**EBTRON** the **GOLD** standard!



**TAMCO EBTRON**  
**AIR-IQ AIR FLOW MEASUREMENT SOLUTION**

**EBTRON** the **GOLD** standard!

# GTx116-P Superior Transmitter Design



**EBTRON** the **GOLD** standard!

# GTx116-P Unsurpassed Connectivity Choices

Snap-in Output Cards  
for the Ultimate  
Connectivity  
Flexibility!



## **GTC116-P (Standard)**

Two field selectable 0-5, 0-10 VDC or 4-20 mA isolated outputs  
One field selectable RS-485 BACnet MS/TP or Modbus-RTU output

## **GTM116-P**

Two field selectable 0-5, 0-10 VDC or 4-20 mA isolated outputs  
One field selectable Ethernet BACnet I/P or Modbus TCP output

## **GTL116-P**

Lonworks

## **GTD116-P**

USB thumb-drive datalogger, logs average airflow and temperature plus airflow and temperature readings of individual sensors with time stamp

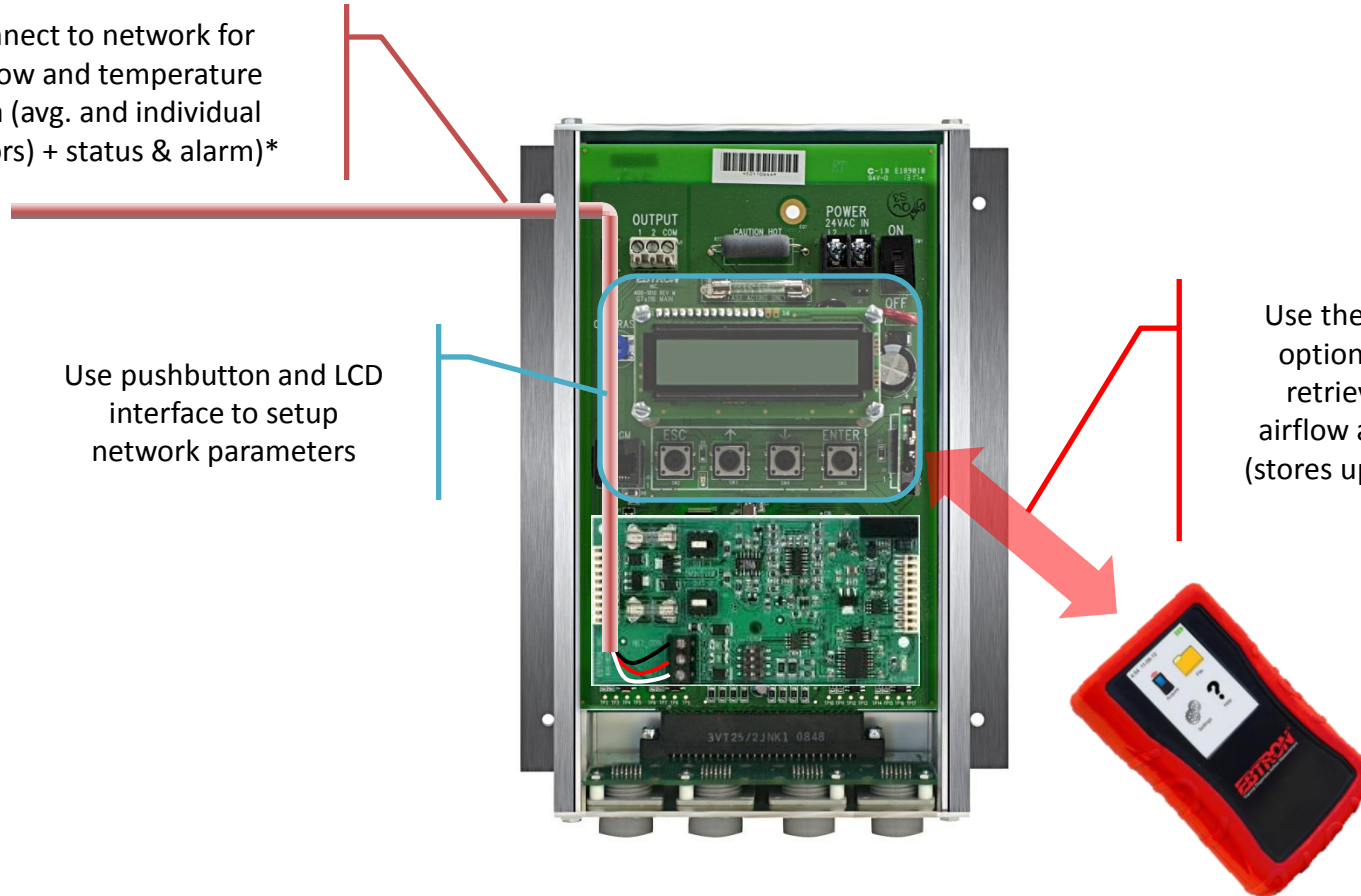
**EBTRON** the **GOLD** standard!

## GTx116-P Added Functionality

Connect to network for  
airflow and temperature  
data (avg. and individual  
sensors) + status & alarm)\*

Use pushbutton and LCD  
interface to setup  
network parameters

Use the **EB-Link Reader** with  
optional **EB-Link** IR card to  
retrieve individual sensor  
airflow and temperature data  
(stores up to 32 locations – USB  
interface)



\* GTX116 RS-485 Shown

# **EBTRON** Small Duct Option

## Hybrid Series HTx104-P

GTx116  
Transmitter



HTx104  
Transmitter



### GTx116-P/HTx104-P Comparison

- HTx104-P is designed for small ducts (approx. 4 ft<sup>2</sup> or less) or larger duct applications that do not require out-of-the-box installed accuracy
  - 4 sensors max.
- Uses same probe technology as Gold Series
- Same as Gold Series with the following exceptions:
  - Uses DIN receptacles and plugs without gold plating
  - Only available with dual analog output signals **OR** RS-485 (no plug-in cards)
  - No *EB-Link* option
- Slightly lower cost for same size duct



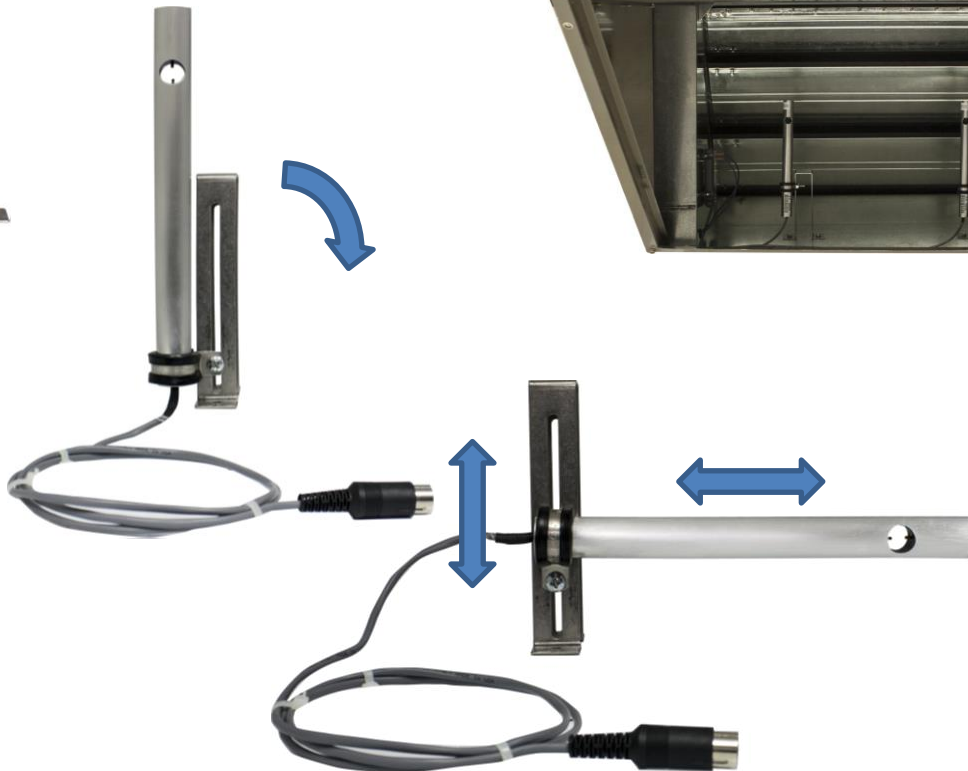
# **EBTRON** Specialty Measurement

## Hybrid Series HTx104-U

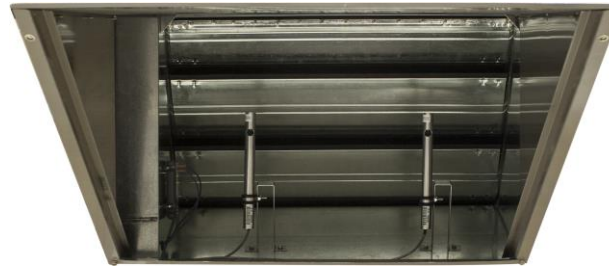
0-2,000 FPM, 3% of reading accuracy (typ.)

Airflow and Temperature Measurement

**Available in 8" or 16" probe lengths**



RTU OA Intakes (3 to 12.5 tons)



Desiccant Wheel ERVs <48"



# EBTRON Small Round Duct Options

## HTx104-T and ELF

0-3,000 FPM, calibrated in duct sized wind tunnels, 3% of reading installed accuracy (typ.)  
Specifically designed for small round ducts and terminal box applications



### HTx104-T/ELF Comparison

- Both use -T probes specifically designed and calibrated for round ducts  $\leq 16''$
- Both HTx104-T and ELF are available with an RS-485 BACnet option
- HTx104-T transmitter can be remotely mounted, ELF cannot be
- HTx104-T has more power and signal protection than ELF
- ELF base version only has airflow output only (no temperature)
- ELF does not have an LCD display or pushbutton user interface
- ELF has a significantly lower cost



Thermal Dispersion Airflow Measurement

Innovative Solutions

Real Applications

That Other Engineers Utilize Ebtron



# Ebtron Products Save Time & Money

- Reduces set-up costs
  - Simple product installation
    - Installed by Controls Contractor not the Mechanical Contractor
  - Start-Up Procedure
    - No 'K' factors or 'pressure-to-velocity' conversions
    - Turn Power Switch to ON ... done
  - TAB goes from calibration to verification (when installed per guidelines)



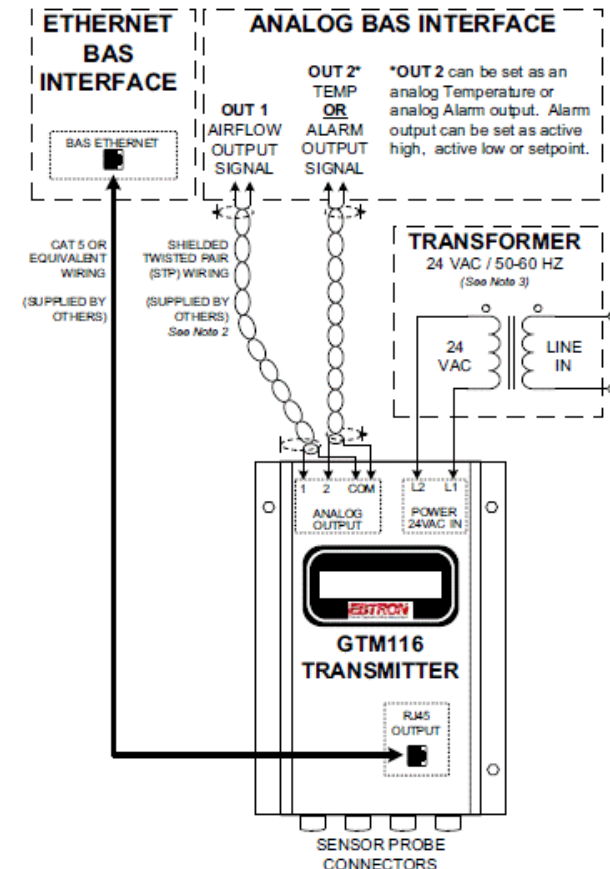
Start-Up Procedure  
Step 1: Turn Power ON  
Step 2: Replace Cover

# Ebtron Products Save Time & Money

- Free Temperature Output (Gold)
  - Saves material and installation costs of a temperature sensor (\$125+ Savings)
  - Excellent Accuracy (+/- 0.15°F)

Two Analog Outputs

1. Airflow
2. Temperature



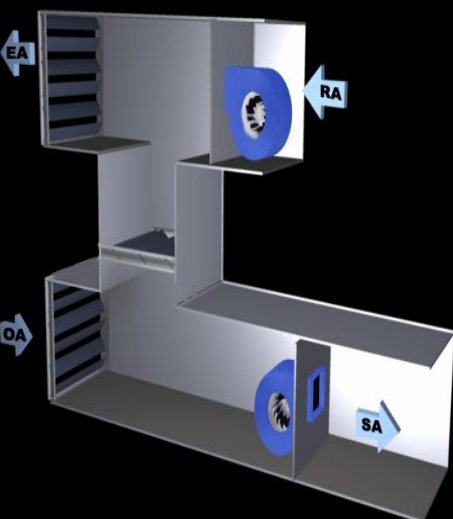
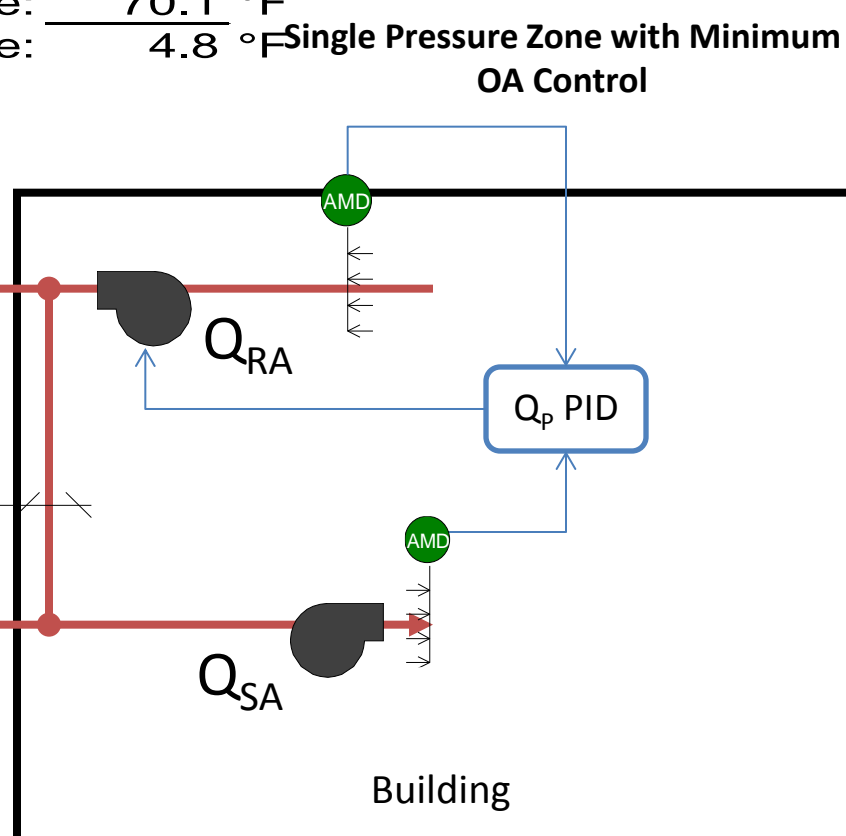
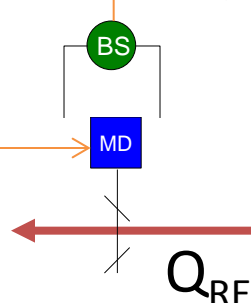
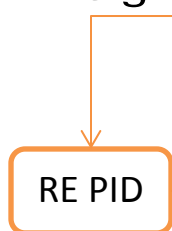
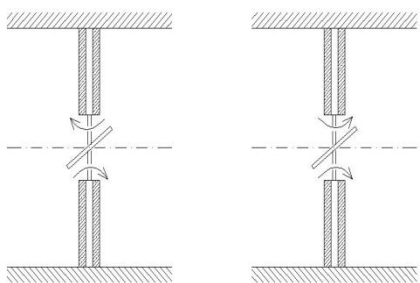
# Arithmetic vs. Weighted Temperature Example

Measurement Location: Mixed Air Stream

Velocity Profile (FPM)			
1646	1431	1418	1426
1184	1195	1217	1024
783	561	685	788
519	445	358	460

Temperature Profile (°F)			
82.4	81.1	80.3	80.4
70.6	69.9	69.8	68.0
60.3	59.9	60.1	61.9
49.8	49.9	51.0	49.7

Arithmetic Average: 65.3 °F  
 Weighted (true) Average: 70.1 °F  
 Difference: 4.8 °F



# CURRENT PRACTICE

## AHU SYSTEM CONTROL

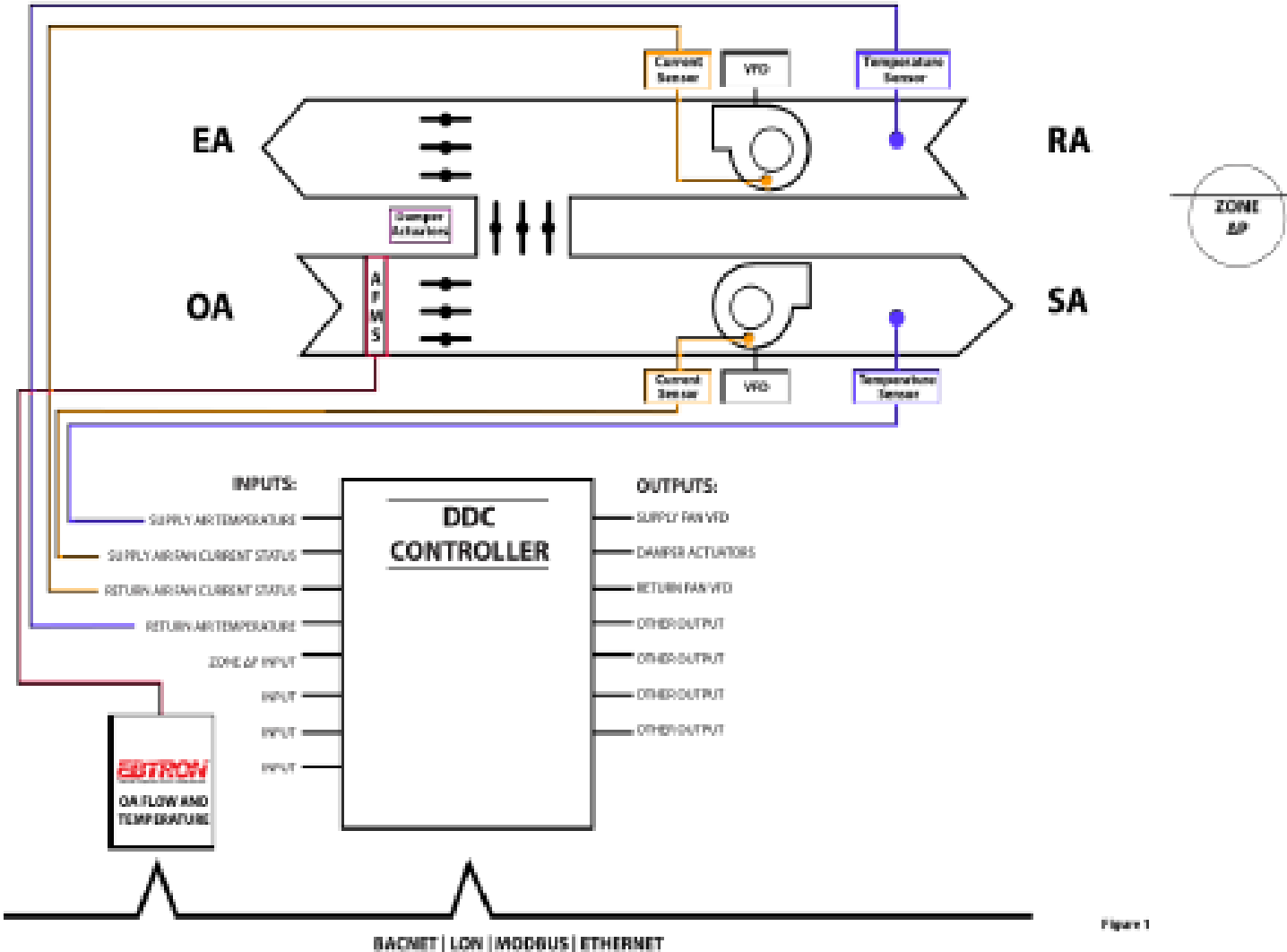


Figure 1

Figure 1. Current Practice – AHU System Control

# NEW OPPORTUNITY

## AHU SYSTEM CONTROL

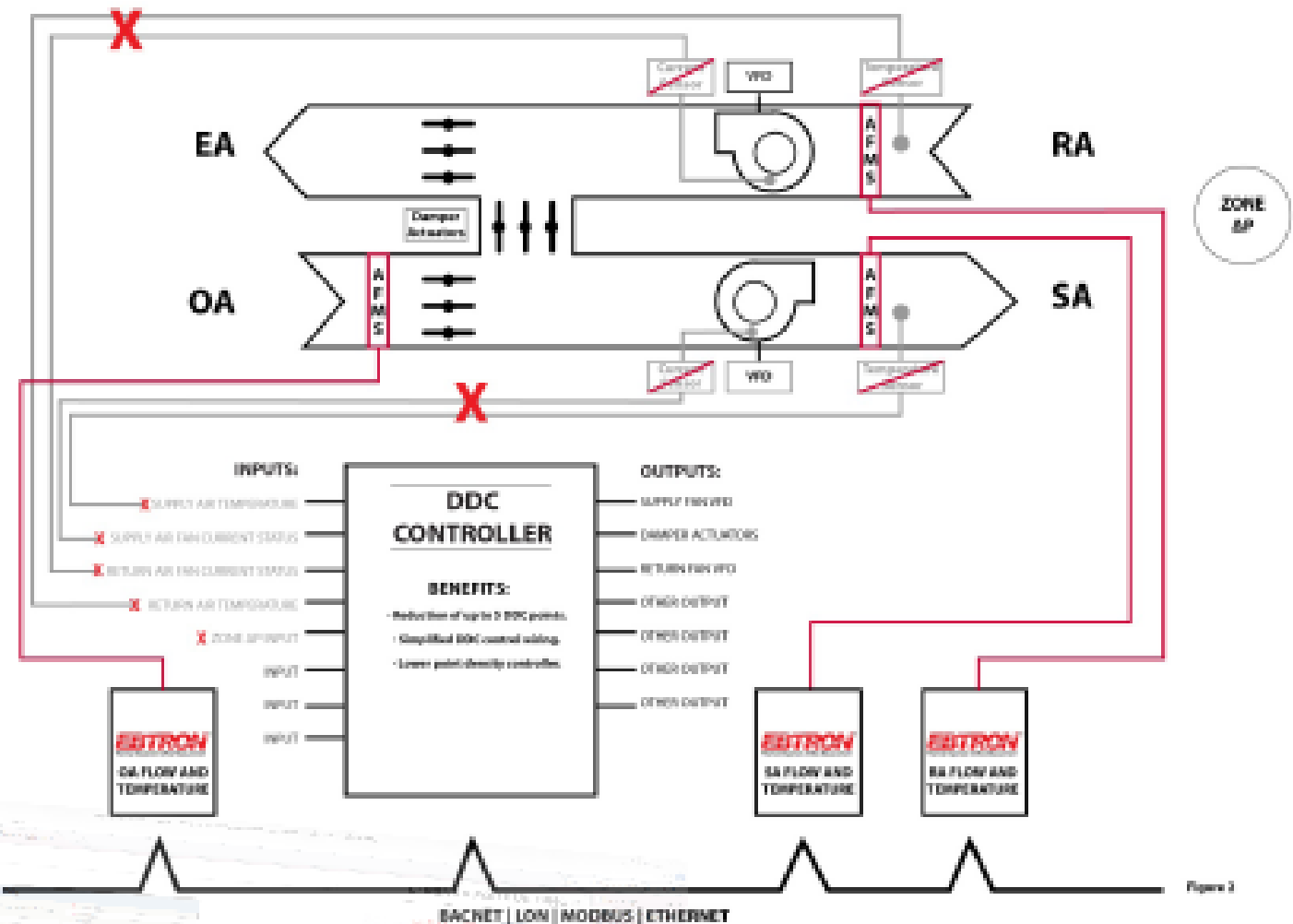


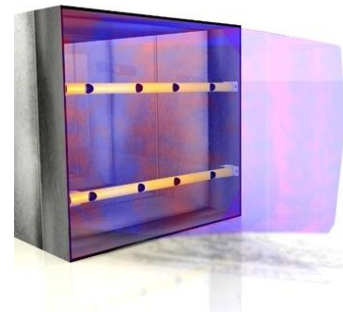
Figure 2

Figure 2. Cost-Effective Solution – AHU System Control

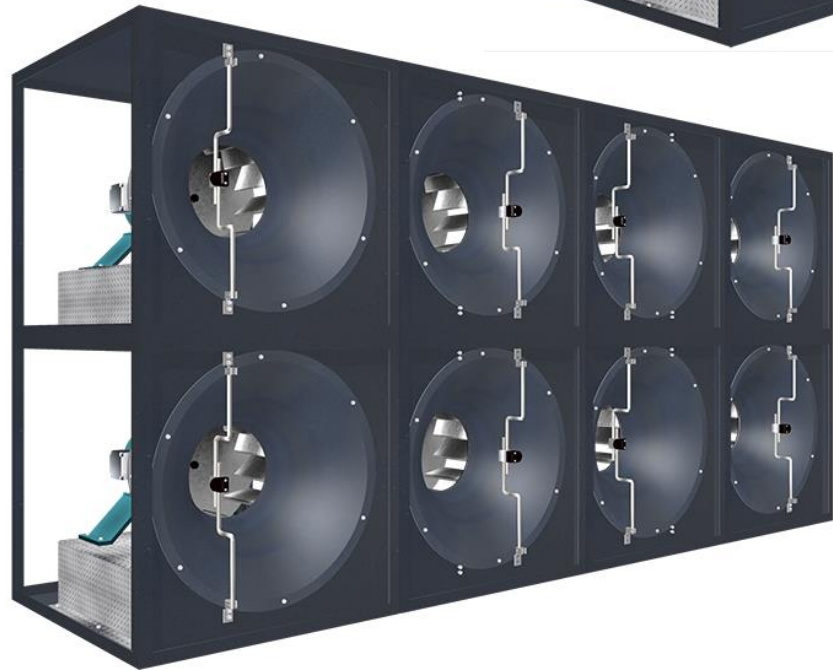
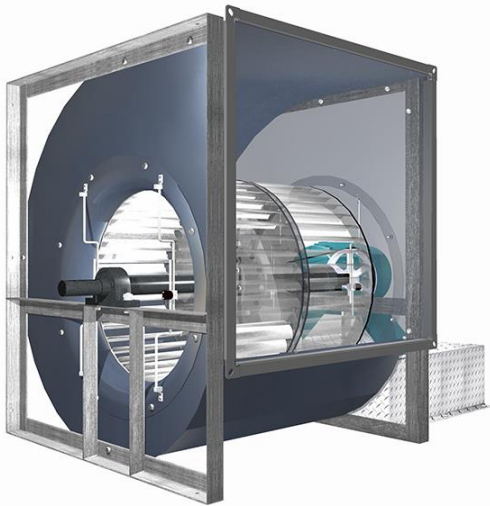
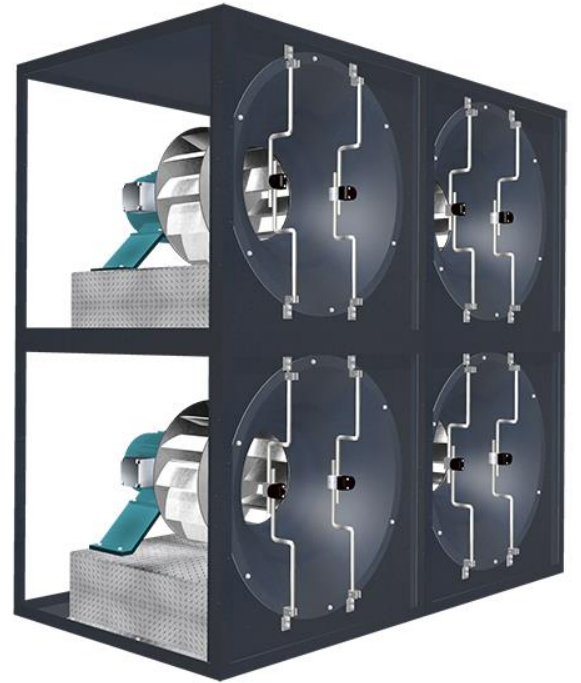
# What about Fan Arrays



One Drive Controls Multiple Fans?  
Micro Drive Back To A PLC?



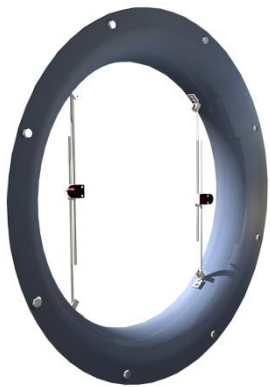




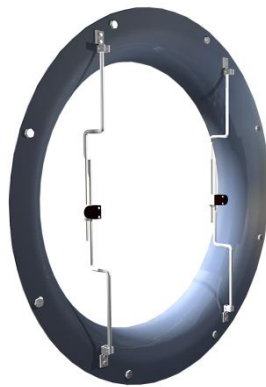
# Mounting Options:



✓ Throat



✓ Face



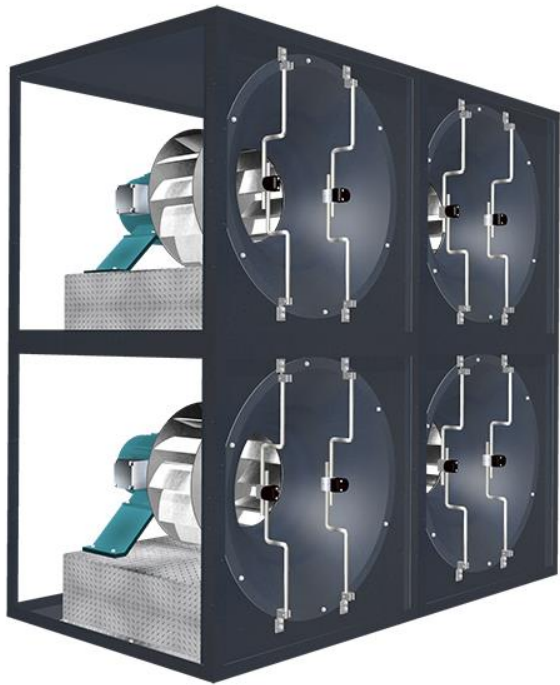
✓ Forward



✓ Flare







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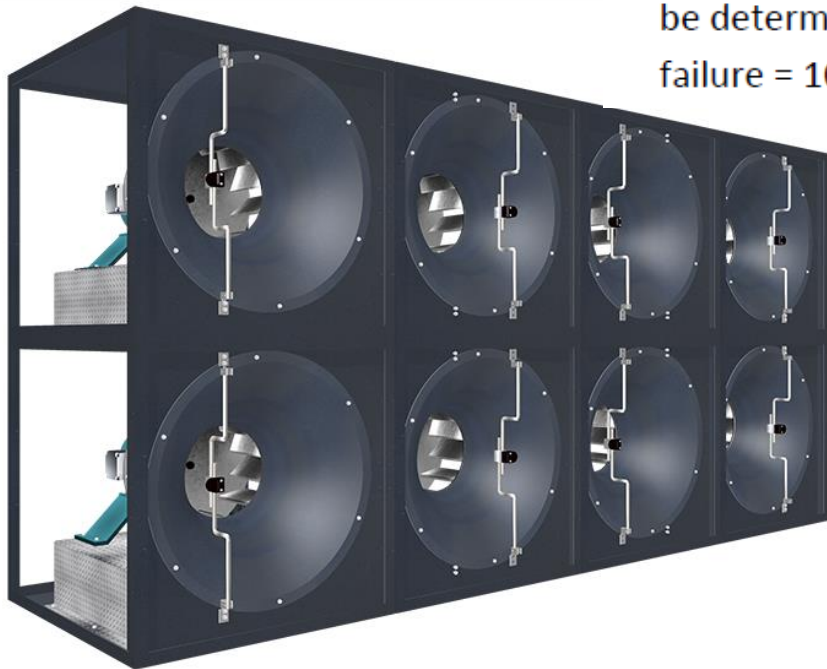
## INDIVIDUAL FAN ALARMING METHODS

---

MINIMUM	User defined minimum FPM or CFM
DEVIATION	User defined % deviation from median FPM or CFM of all fans
% MAXIMUM	% deviation from maximum velocity stored of each individual fan

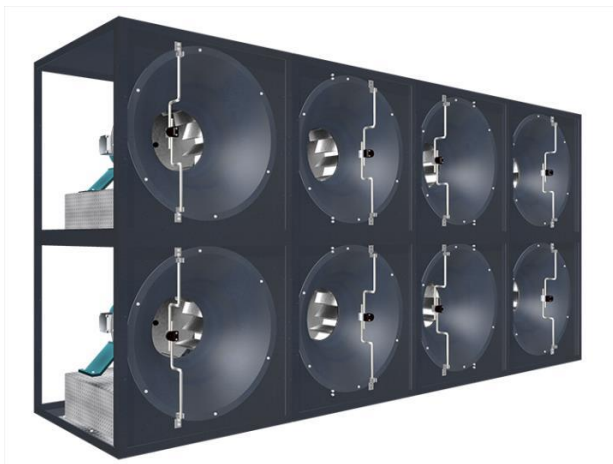
---

The *Fan Alarm* is available via the network or by assignment of the alarm to the second analog output, AO2, on GTC108 and GTM108 models. Fan failure on the analog output can be determined by the magnitude of the output signal (fan 1 failure = 10% of F.S., fan 2 failure = 20% of F.S., etc.)



# Example

Items	Cost Add	Piezo Ring	EBTRON Fan Array
Ring	\$50 per fan	\$400.00	
Transducer	\$200 per fan	\$1600.00	
Current Donut	\$50 per fan	\$400.00	
ATC Alarms Points	\$ 600 per fan	\$ 4800.00	\$1000.00
		\$7,200.00	\$3,512.00



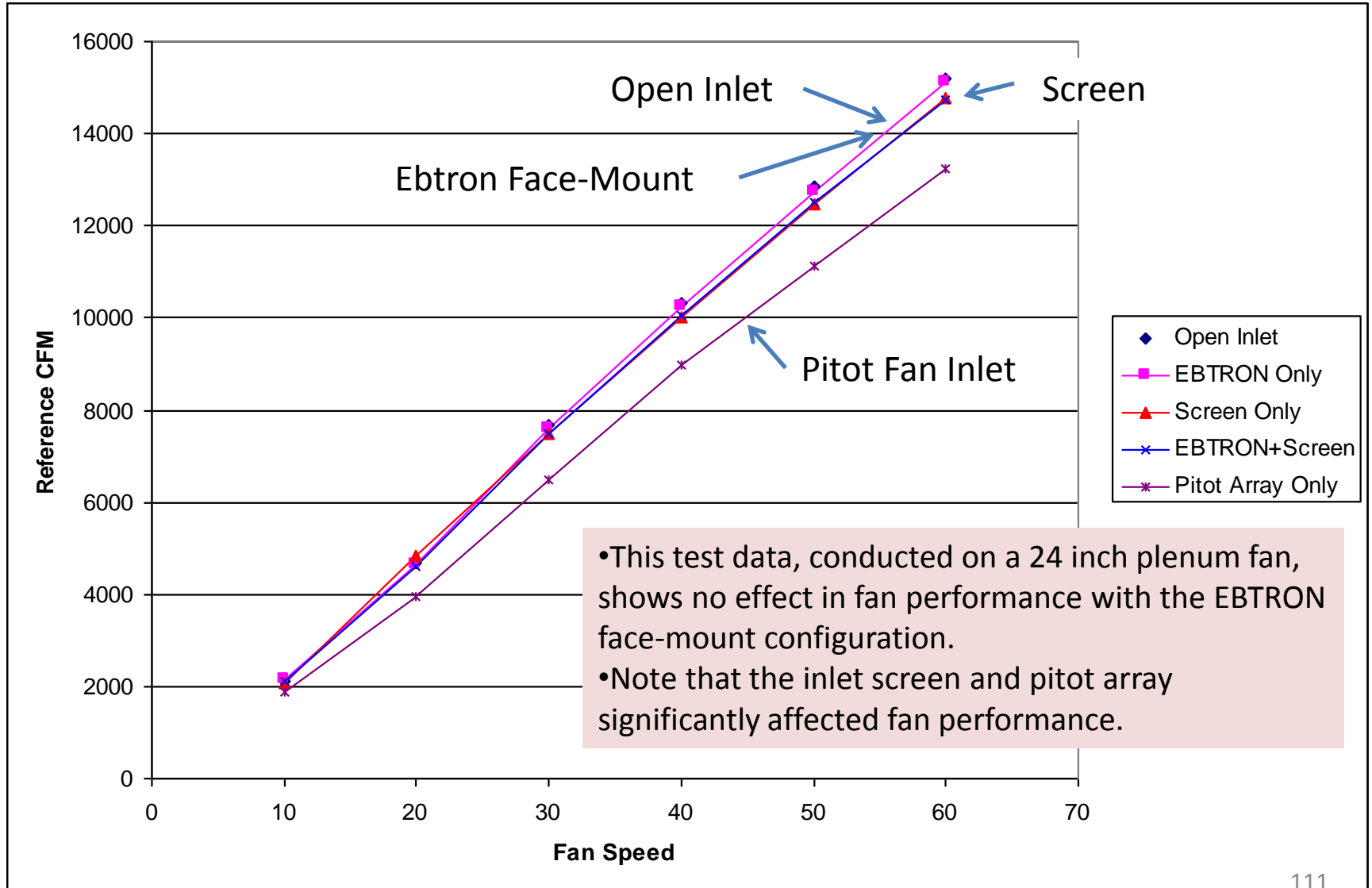
**Better Performance**  
**No Yearly Calibration**

# -F Fan Inlet Specifications

Range:	0-10,000 fpm
Airflow Sensor Acc'y:	+/- 2% of the reading +/- 0.25% repeatability
Temp Sensor Acc'y:	+/- 0.15 °F
Environmental:	-20 to 160 °F 0 to 99% RH, non-condensing
Size Ranges:	11 to 64 inches
Plug & Play:	No matching of probe to transmitter Calibration data stored in cable's memory chip
Cables:	Plenum rated, PVC jacket 10 ft. standard, 50 ft. maximum



# Face-Mount: No Fan Performance Effects



## A more cost effective Bleed Sensor!

- SB1 compatible
- Two analog output signals
- Contact closure alarm



# Bi-Directional, Low-Flow Sensor Specifications

Range: -3,000 to 3,000 fpm  
bi-directional

Airflow *Sensor Acc'y*: +/- 2% of the reading  
+/- 0.25% repeatability

Temp Sensor *Acc'y*: +/- 0.15 °F

Environmental: -20 to 160 °F  
0 to 99% RH, non-condensing

Outputs: Velocity (can convert to equivalent pressure)

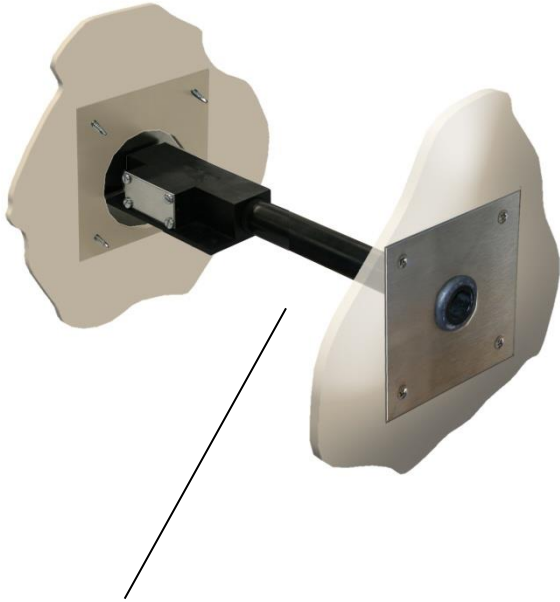
Plug & Play: No matching of probe to transmitter  
Calibration data stored in cable's memory chip

Cables: Plenum rated, PVC jacket  
10 ft. standard, 50 ft. maximum



Measures Flow  
instead of  
Pressure to  
Ensure/Calculate  
Zone or Bldg.  
Pressurization

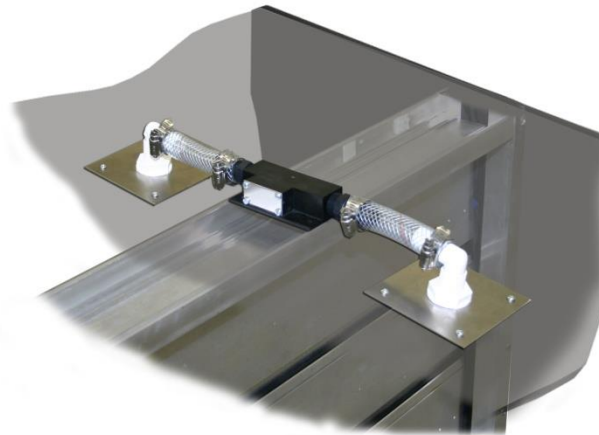
# -B Bi-Directional, Low-Flow Airflow Sensors For Measuring Differential Pressure Between 'Zones'



## MONITOR LOW PRESSURE

Use to verify pressure differentials by determining the pressurization flow between spaces or across the building envelope

*EBTRON* optional *Through-Wall* kit shown. Protect from rain or snow by providing a rain hood or louver (by others) on exposed outdoor walls.



## CONTROL DAMPERS

Assure proper airflow direction across relief dampers (supply/return fan system) or recirculation dampers (supply/exhaust fan systems)

Sensors can also be used to determine airflow across many intake louver configurations (consult *EBTRON* for flow rate requirements).

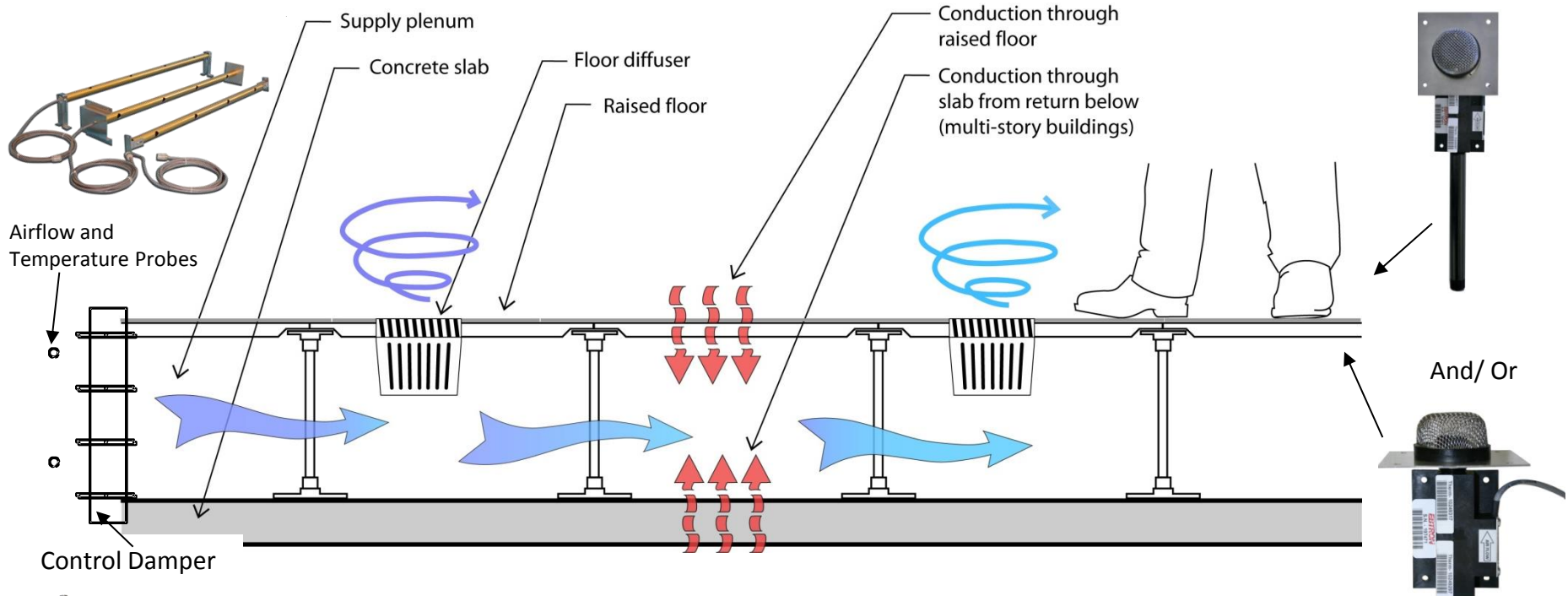


## MAINTAIN UNDER FLOOR PRESSURE

Use bleed airflow to maintain stable pressurization with under floor systems



# -B Bi-Directional, Low-Flow Sensor for Under Floor System Control



## MAINTAIN UNDER FLOOR PRESSURE:

Use the bleed sensor to monitor the UFAD pressurization flow. Using a GTX-116 airflow (through the BAS) and a simple reset PID control loop, reset the flow (800 to 1200 fpm nominal) to incrementally increased and decreased the UFAD supply damper flow to meet the bleed sensor(s) nominal velocity for stable under floor control.





# Original Data Center Designs

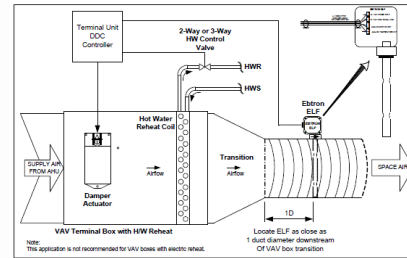
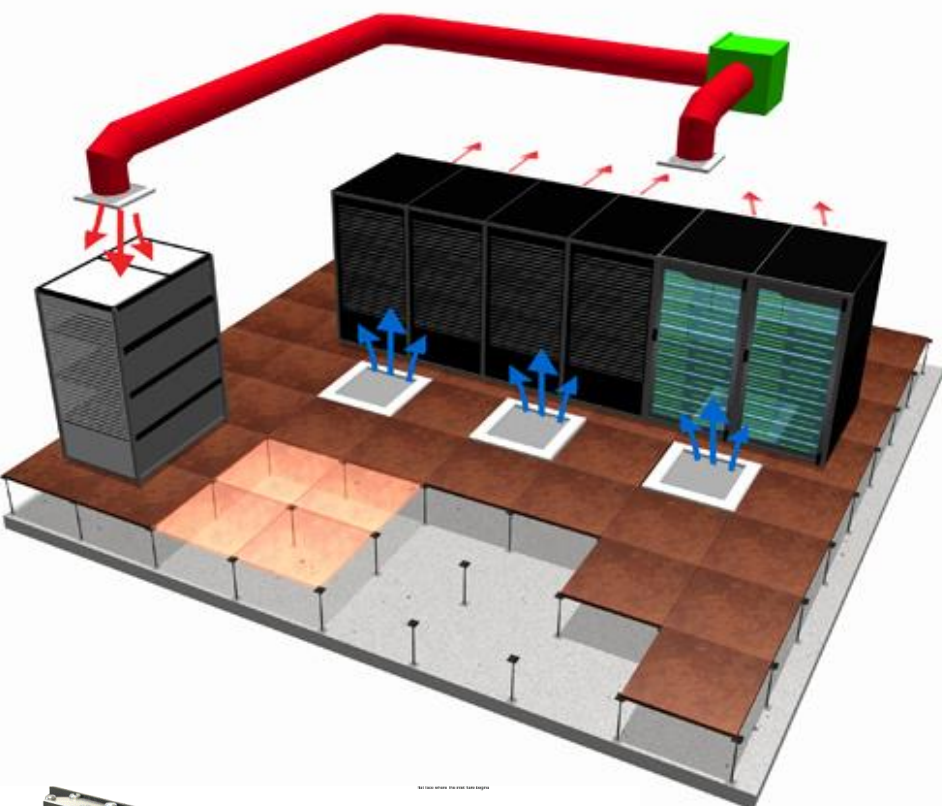
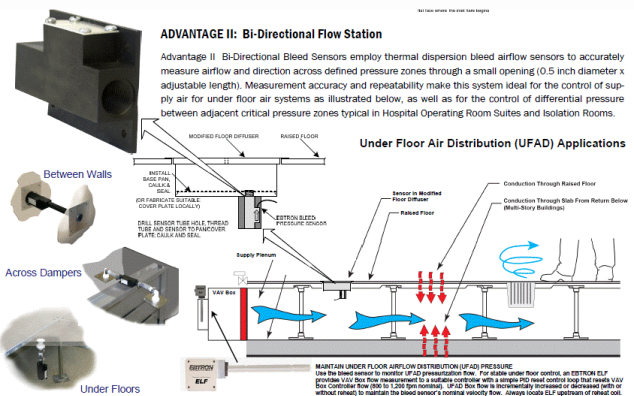
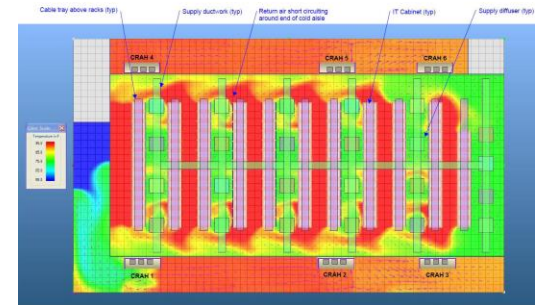


FIGURE 1.  
ELF-D APPLICATION - VAV TERMINAL UNIT WITH HOT WATER REHEAT

Phase 1 - No Aisle Containment - TS F Supply Air Temp

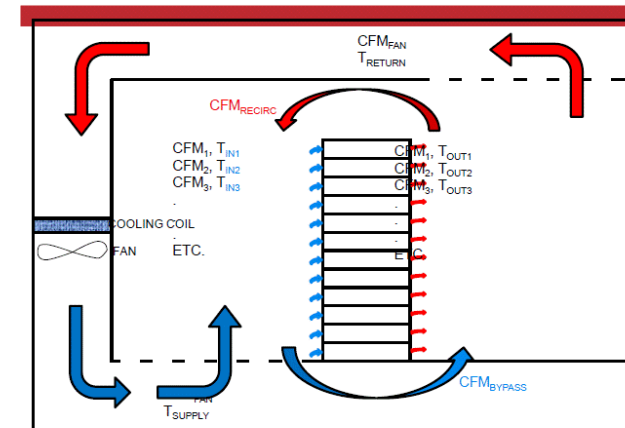


## ADVANTAGE II: Bi-Directional Flow Station

Advantage II Bi-Directional Bleed Sensors employ thermal dispersion bleed airflow sensors to accurately measure airflow and direction across defined pressure zones through a small opening (0.5 inch diameter x adjustable length). Measurement accuracy and repeatability make this system ideal for the control of supply air for under floor air systems as illustrated below, as well as for the control of differential pressure between adjacent critical pressure zones typical in Hospital Operating Room Suites and Isolation Rooms.

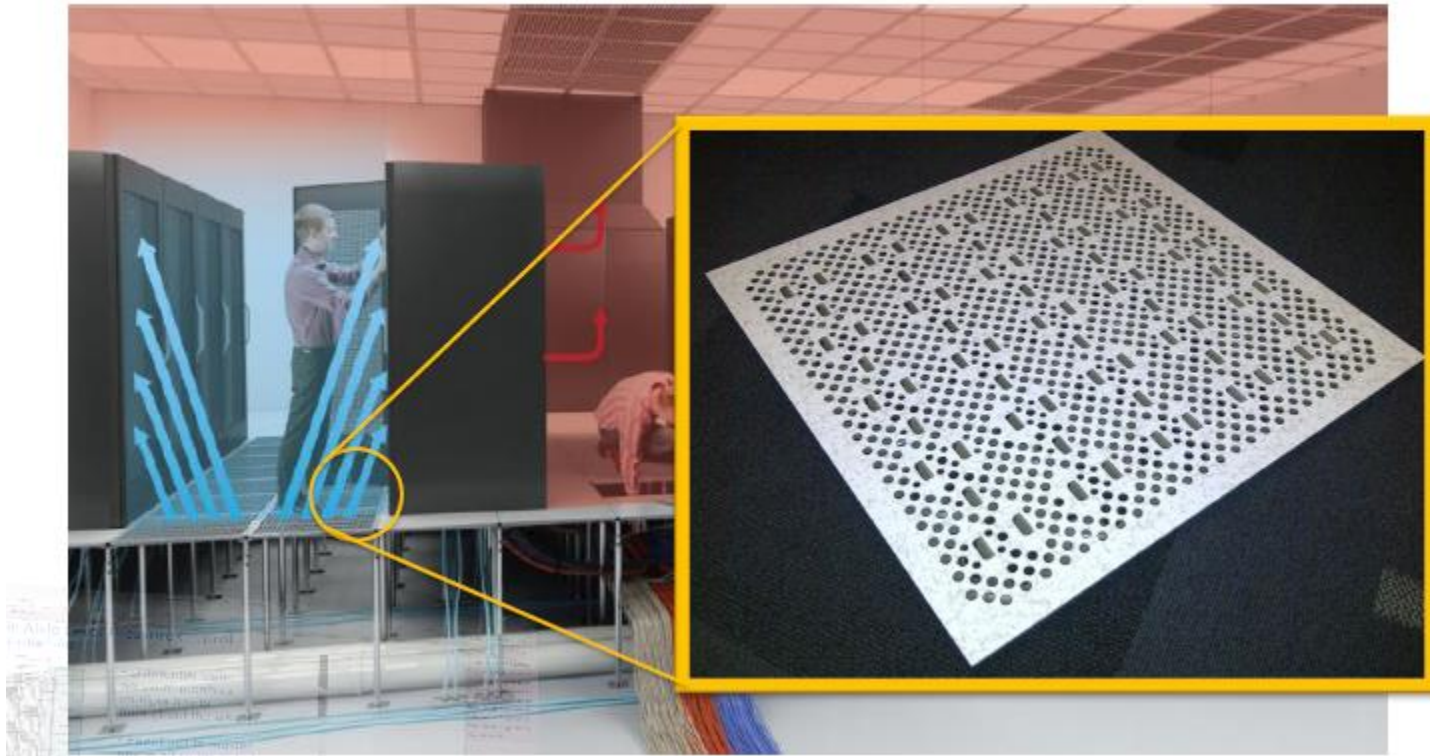
## Under Floor Air Distribution (UFAD) Applications

MAINTAIN UNDER FLOOR AIRFLOW DISTRIBUTION (UFAD) PRESSURE. One to three bleed sensors per pressure zone. For stable under floor control, an ETRON ELF provides VAV flow measurement in a multi-control loop with a simple PID bleed control loop that reads VAV flow control from 0PS to 250 gpm (nominal). UFAD flow is normally increased or decreased with or without reheat) to maintain the bleed sensor's nominal viscosity flow. Always locate ELF upstream of reheat coil.

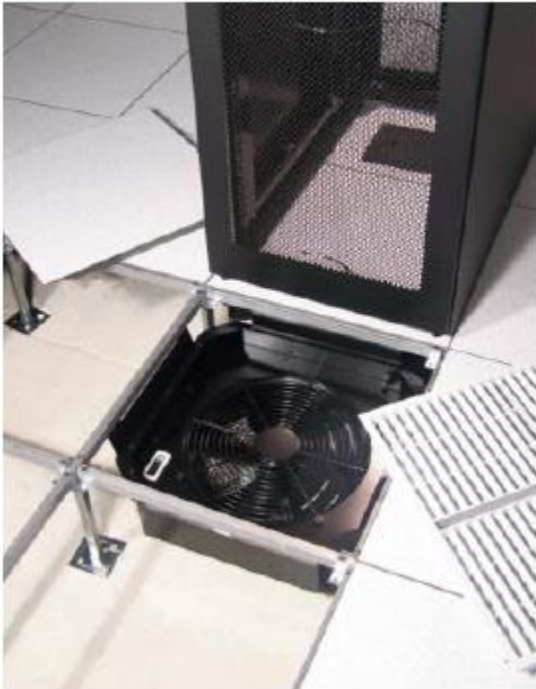


Representative Data Center Without Containment

## Directional Perf (Directional Airflow Perforated Panel)



## Fan Assisted Cooling

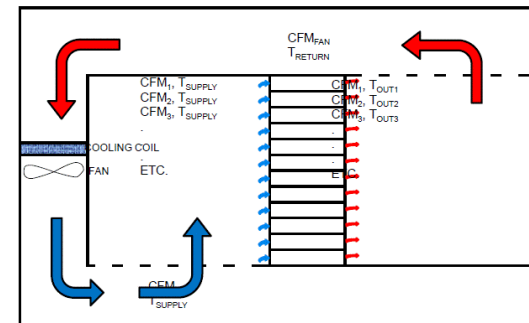
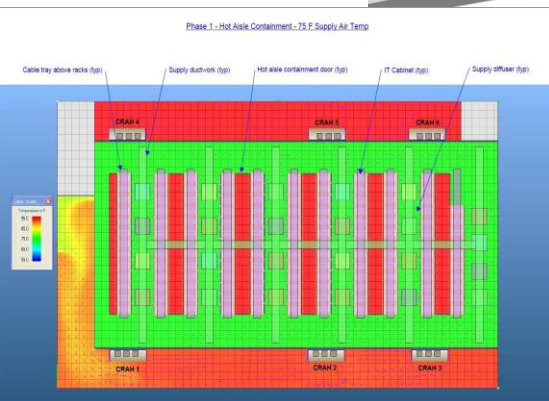




# Future Data Center Designs

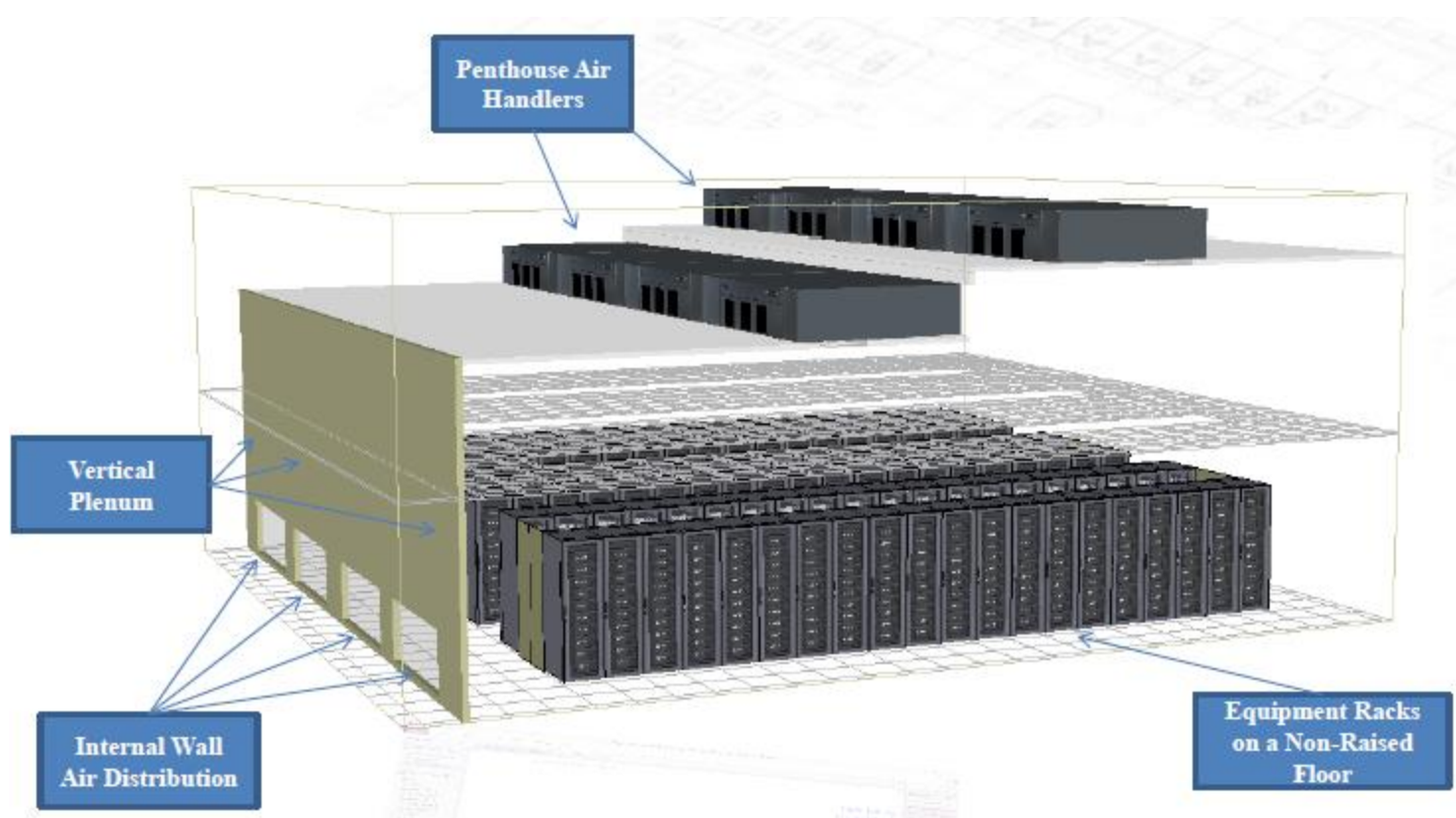


## Hot / Cold Containment



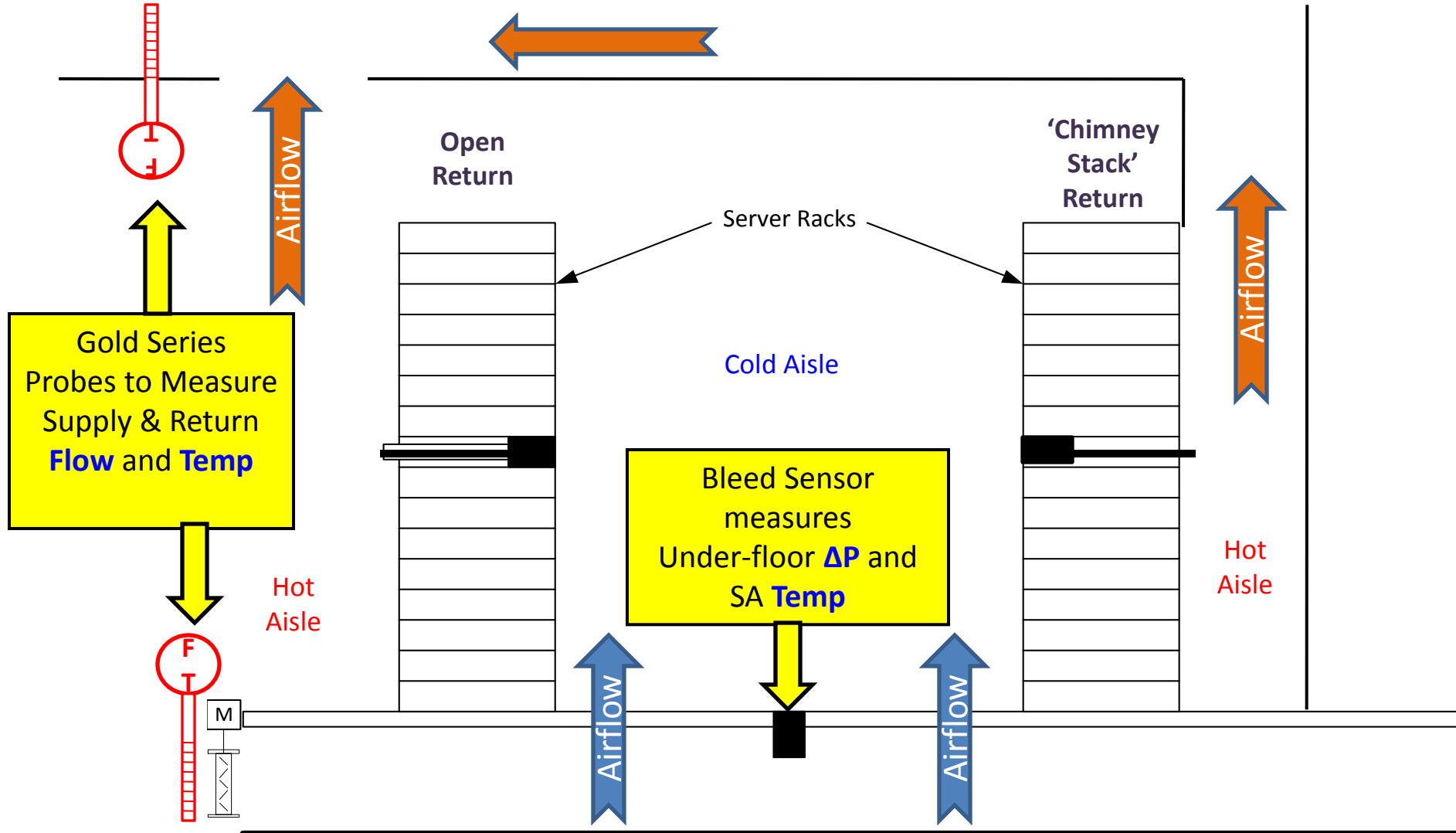
Representative Data Center With Containment

# Central Air Handler System

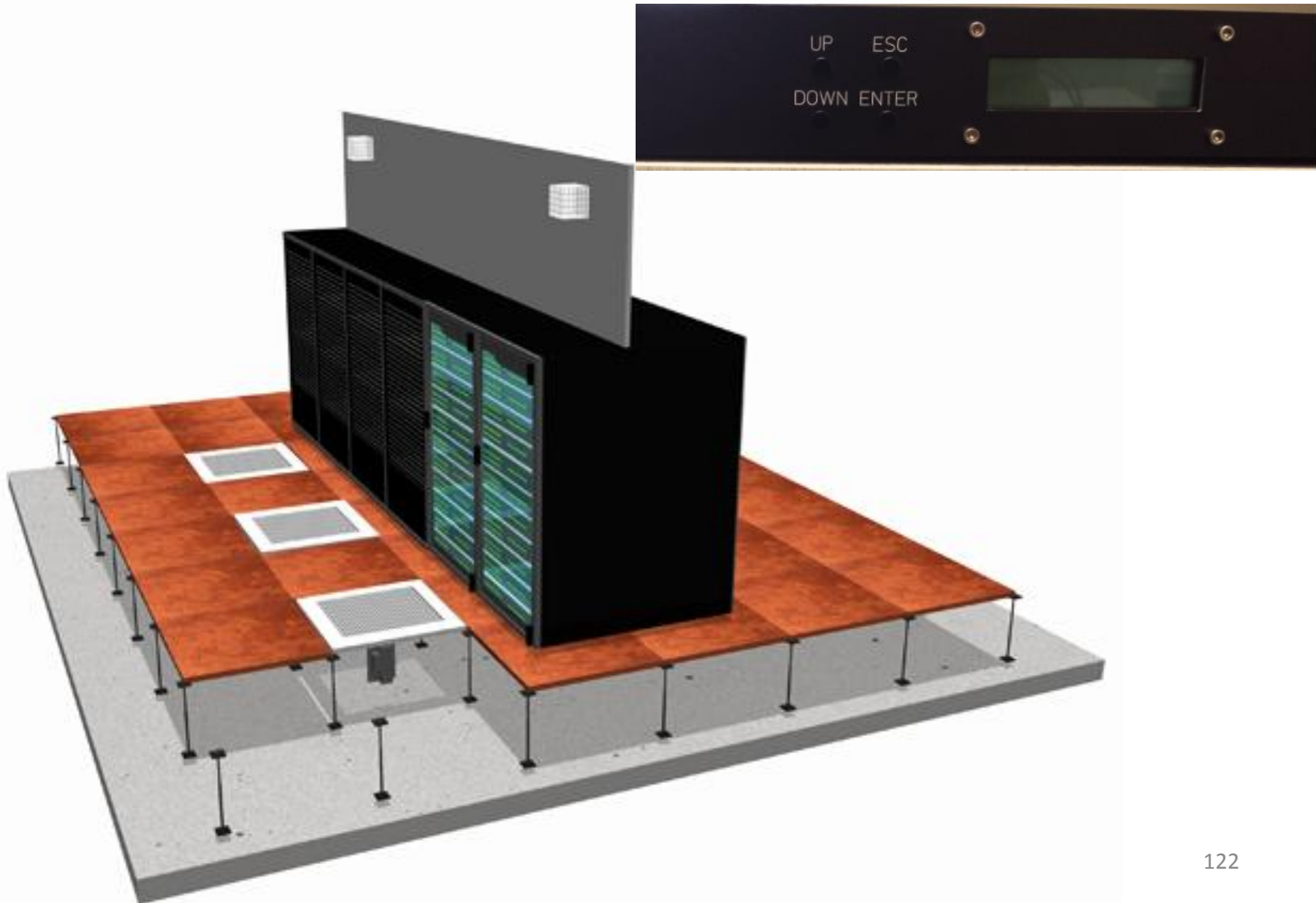


# EBTRON Airflow Stations & 'Bleed'

Ensure Proper SA & RA Flow and Temperature



# Future Data Center Designs



# Data Center Action Plan

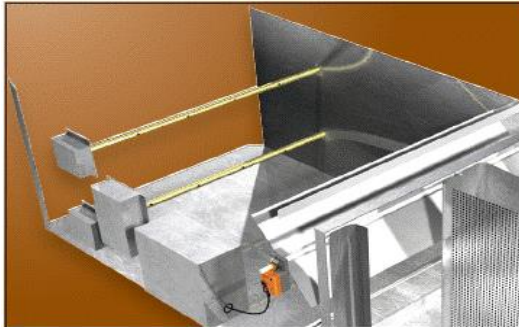
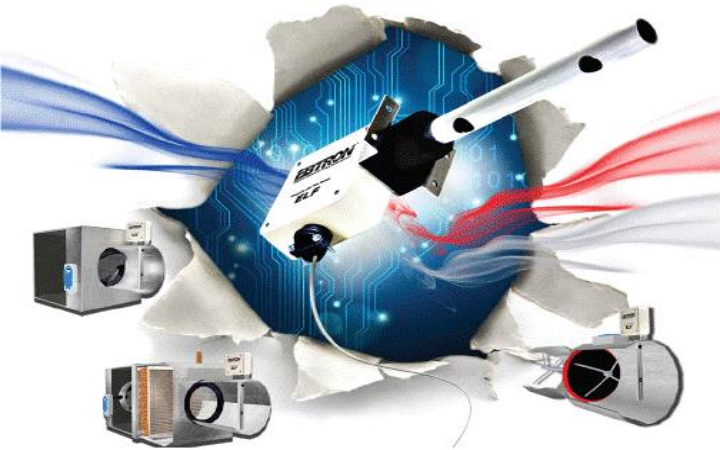
$$\text{PUE} = \frac{\text{Total data center power}}{\text{IT equipment power}} = \frac{1}{\text{Site infrastructure efficiency}}$$

- Understand their Language for Data Centers (Owner & Consulting Engineers)
- Ebtron sensors can be utilized as alarms for existing & smaller data center designs
- Ebtron sensors can be utilized as an alarm and control points for Hot/Cold Aisle Containment
- Ebtron's Velocity Weighted Temperature Control point is unmatched and saves the client money
- Ebtron's Bi Directional Flow Meters provide the client with the most reliable and stable system for underfloor applications.

**Protect Your Equipment!**  
**Compare the Ebtron Cost to Cost of the Servers**



# **EBTRON ELF** (Electronic Low Flow)



## **Factory-Mounted Controls**

- Ebtron Electronic Air Flow Stations
- Customer Provided Controls
- Factory Controls

Airflow Ranges: 0-500 fpm  
0-1,000 fpm  
0-2,000 fpm  
0-3,000 fpm

Accuracy: +/-3% of the READING

Input: 24 VAC  
Voltage Output: 0-10/2-10 VDC  
0-5 /1-5 VDC

Outputs (units): Airflow (fpm)  
Equivalent Velocity Pressure  
(for controllers designed to take a  $\Delta P$  input)

Duct Sizes: 4 to 16 inches

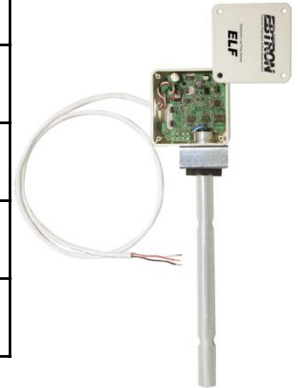
**Ideal for lab/operating/isolation room airflow tracking and accurate VAV box measurements**

# +/-% of Reading Error Comparison Pressure Transducer *Drift* Effect vs. **Ebtron ELF**

	<b>ΔP Devices</b>			<b>EBTRON ELF</b>
	@1,250 fpm	@750 fpm	@400 fpm	
<b>Start-Up</b>	<b>0%</b>	<b>0%</b>	<b>0%</b>	<b>3%</b>
<b>Year 1</b>	2.0%	5.7%	21.9%	<b>3%</b>
<b>Year 2</b>	4.1%	11.8%	53.2%	<b>3%</b>
<b>Year 4</b>	8.4%	25.5%	Error%*	<b>3%</b>
<b>Year 6</b>	12.8%	42.2%	Error%*	<b>3%</b>

$$p_{vel} = p_{total} - p_{static}$$

$$V = 2500 \times \sqrt{p_{vel}}$$



ΔP Assumptions:

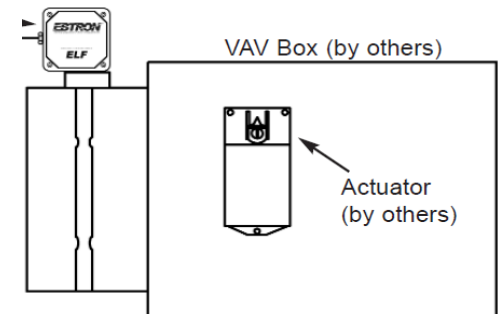
**0 error at start-up**

**0.5% F.S./yr pressure transducer drift**

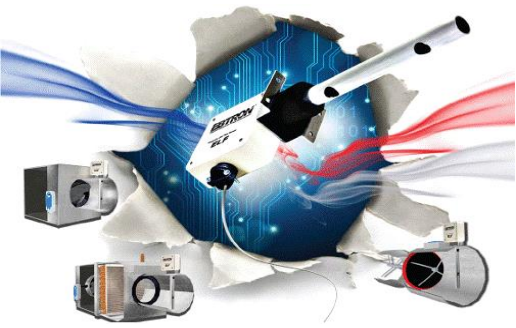
**2" w.c. pressure range**

**k = 2,500 fpm ('amplifying' flow cross)**

**\* >100% Error - Airflow cannot go negative**



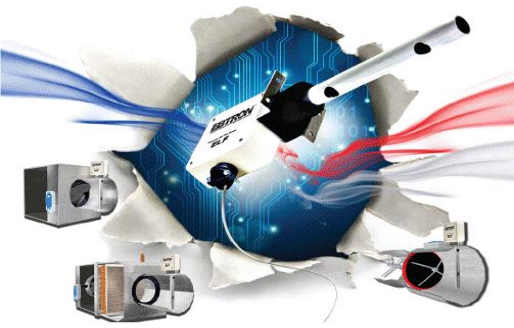
**Ebtron ELF Outperforms Today's VAV Box  
Airflow Measurement**



## ***Ebtron ELF: Labs***

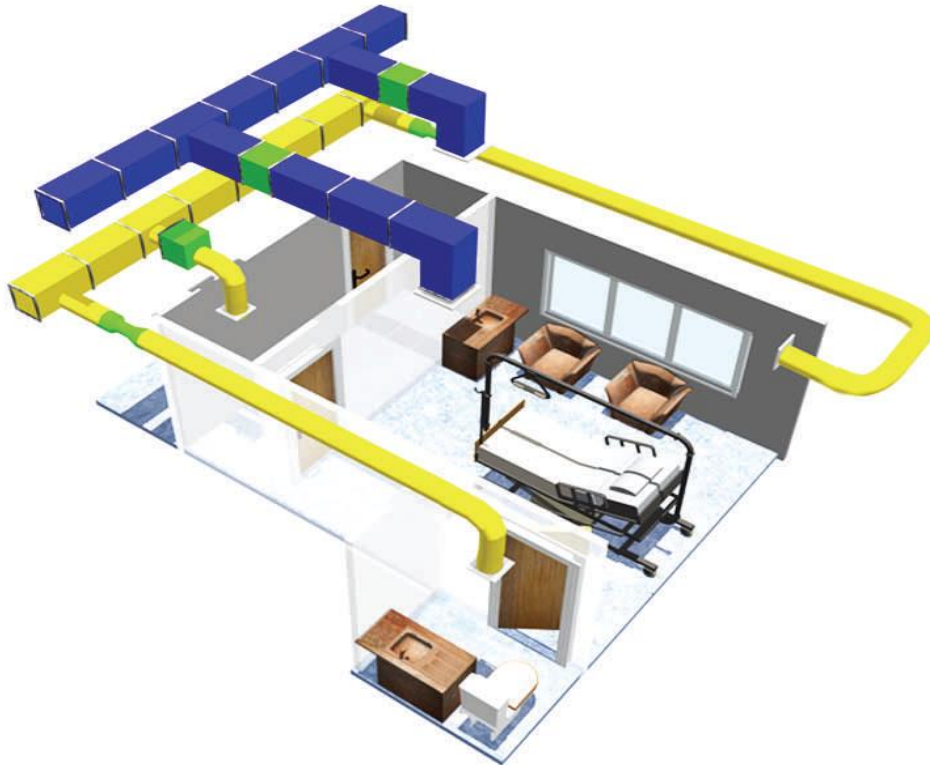
Engineers take into effect all the factors that can contribute to leakage and specify a differential airflow based on an estimated leakage rate or target for which the airflow rates are adjusted





# ***Ebtron ELF:*** Hospitals

Pressurization is a key factor in controlling room airflow patterns in a health care facility. Engineers take into effect all the factors that can contribute to leakage and specify a differential airflow based on an estimated leakage rate or target for which the airflow rates are adjusted



# Exciting New Alliance!



**TWO PREMIERE MANUFACTURERS  
ONE EXCEPTIONAL PRODUCT**

**ADVANCED THERMAL DISPERSION  
AIRFLOW MEASUREMENT SYSTEM  
AND DAMPER**

**TAMCO EBTRON**  
**AIR-IQ AIR FLOW MEASUREMENT SOLUTION**



# TAMCO EBTRON

## AIR-IQ AIR FLOW MEASUREMENT SOLUTION

### AIR-IQ SMART-SOLUTION

You provide us with the:

- Opening size
- Damper series
- Mounting application
- Access requirements for probes

We build your unit with the:

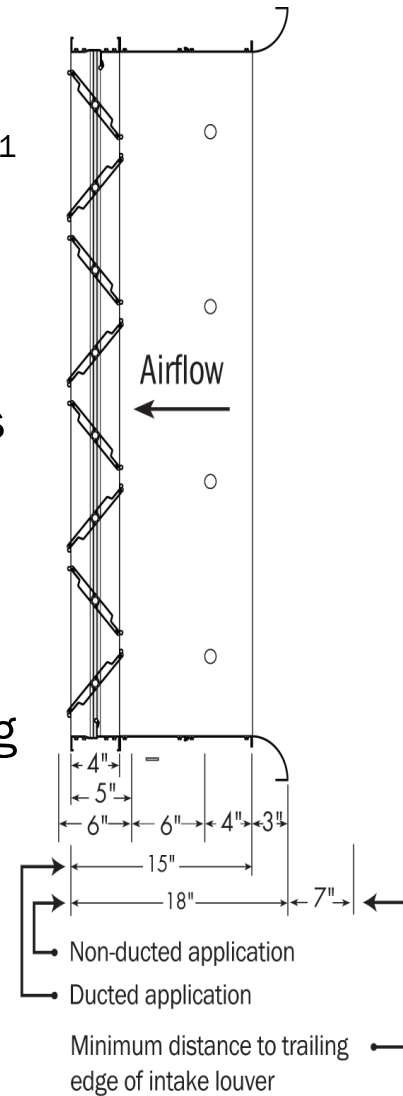
- ✓ Optimal probe sensor density
- ✓ Ideal probe placement
- ✓ Appropriate sleeve style

### BENEFITS

- Satisfy ASHRAE 62.1, 189.1 & 90.1
- Obtain LEED points
- Improve indoor air quality
- Save energy
- Reduce maintenance costs

### APPLICATION

- Outside air intakes
- Floor return airflow tracking
- AHU return & bypass flow measurement



# TAMCO **EBTRON**<sup>®</sup>

## 2000 SERIES DAMPERS



**SERIES 2100**



**SERIES 2900**

**PERFECTLY ADJUSTED AND CALIBRATED**

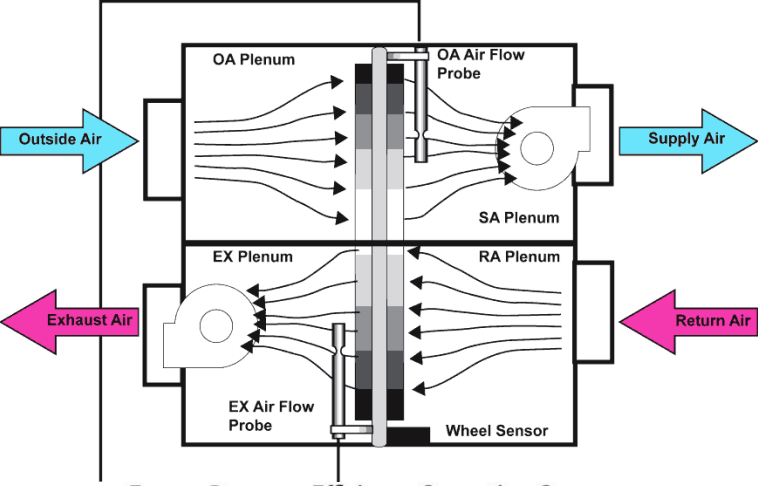
for use in conjunction with  
EBTRON Airflow Measuring devices

**LONG-LASTING AND ACCURATE PERFORMANCE**

for fresh air intake and exhaust applications

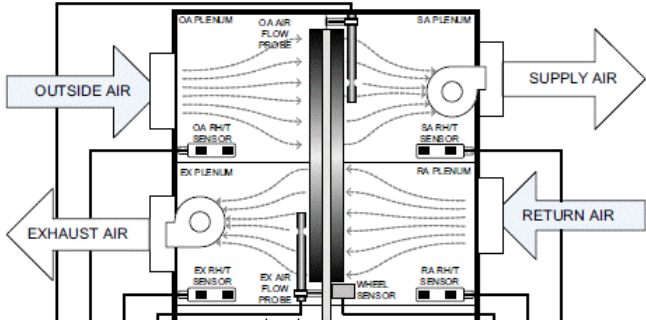
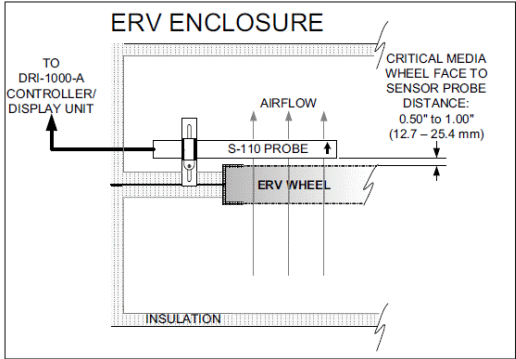
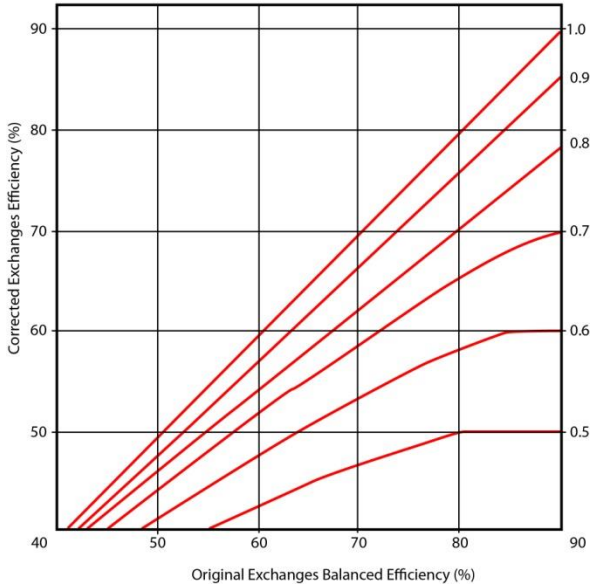
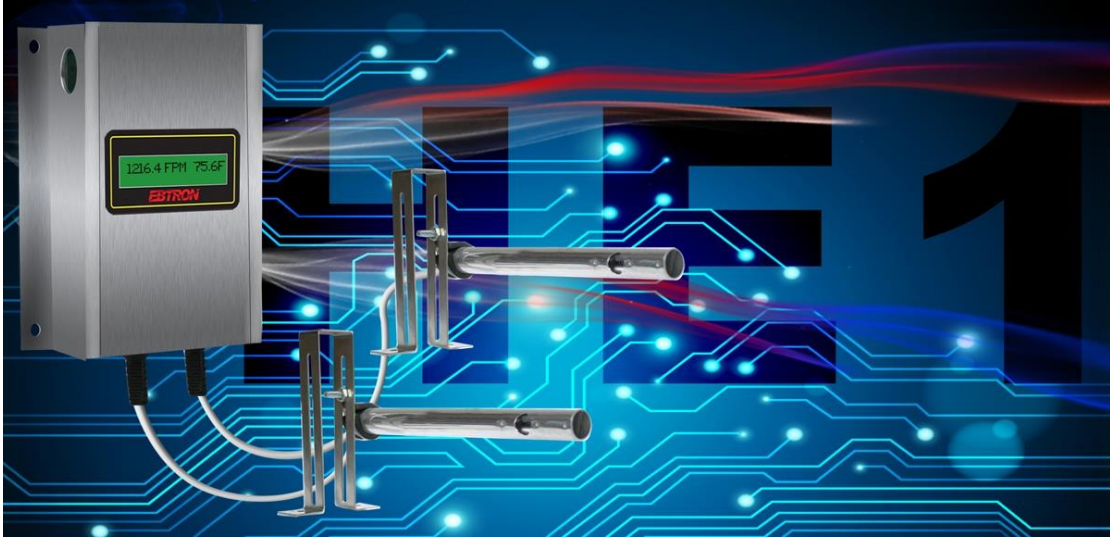
**MAINTENANCE-FREE**

# Energy Recovery Ventilation Air Flow Solutions



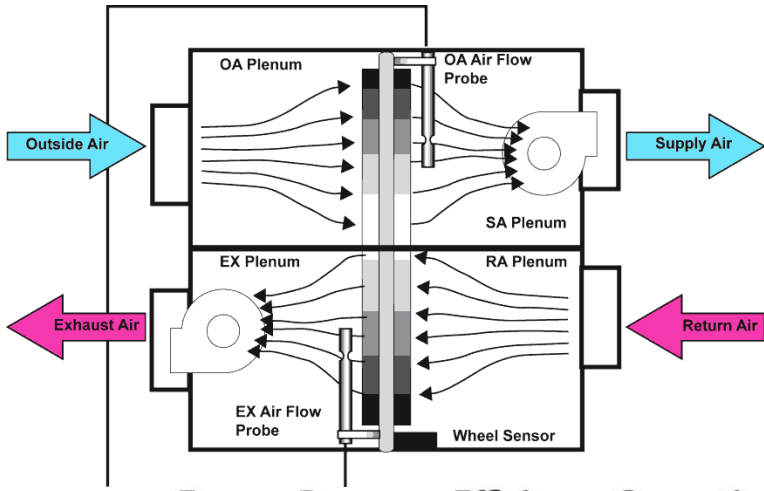
**Energy Recovery Efficiency Correction Curve**

$$\frac{\text{Energy Recovery Efficiency (\%)}}{\text{Corrected Exchanges}} = \frac{\text{Air Volume Ratio (K Factor)}}{\text{Original Exchanges}} = \frac{\text{Exhaust Air Volume}}{\text{Supply Air Volume}}$$



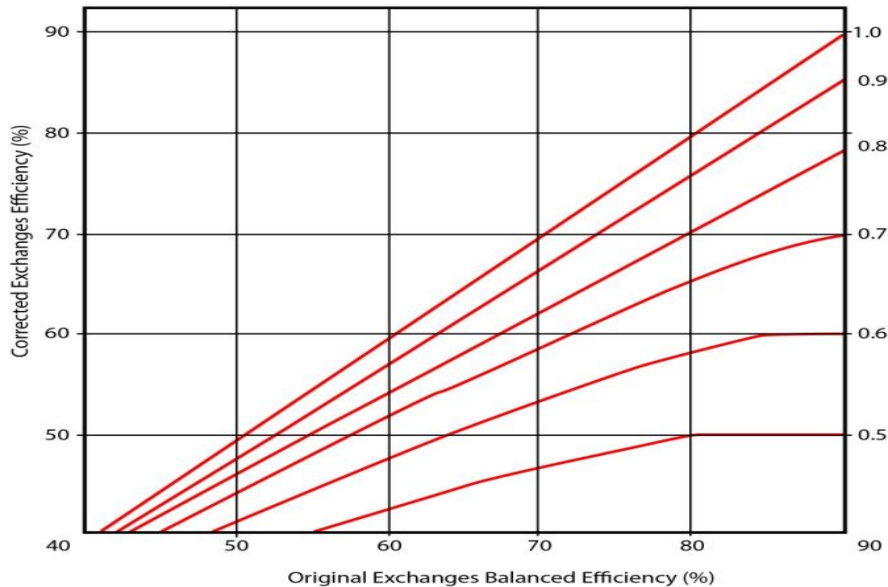


# Energy Recovery Ventilation Air Flow Solutions



**Energy Recovery Efficiency Correction Cure**

$$\text{Energy Recovery Efficiency (\%)} \times \text{Air Volume Ratio (K Factor)} = \text{Exhaust Air Volume} / \text{Supply Air Volume}$$

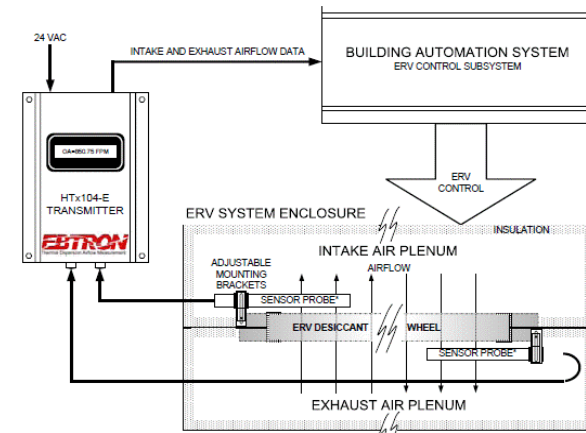


## 2 Analog Outputs

In ERV mode, place a flow probe on each side of the wheel (supply air and exhaust air streams)

## Helps solve 2 main issues with HRV's/ERV's

- Setup the airflow balance on each side of the wheel airflow balance is key to wheel efficiency
- Helps to maintain the desired balance (or offset) during the HRV/ERV's life
  - Detects dirty filters
  - Detects clogged wheels



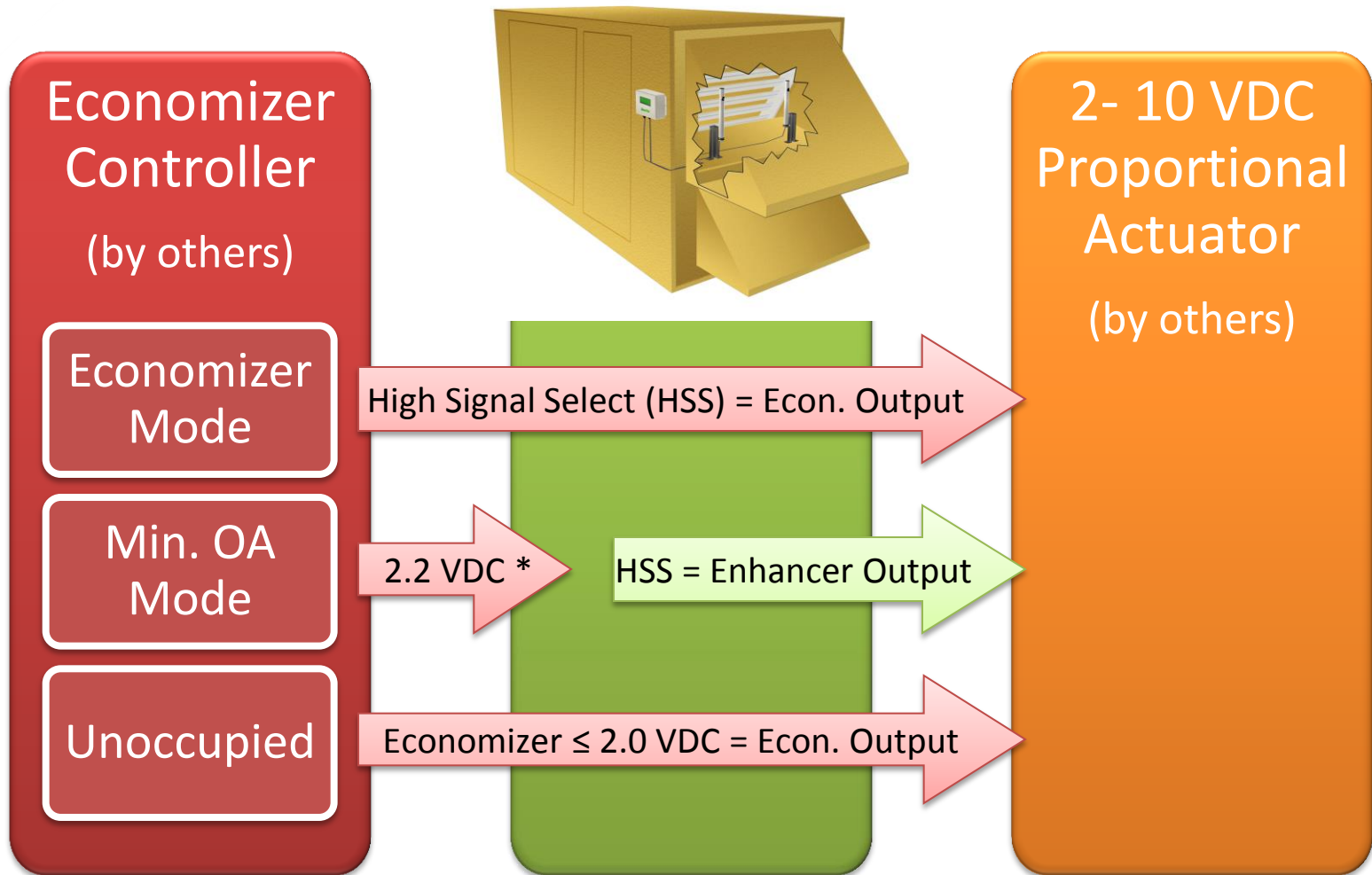
\*INSTALL SENSOR PROBES 0.25 - 0.75 IN (6.35 - 19MM) FROM ERV MEDIA FACE



## Economical Airflow Measurement

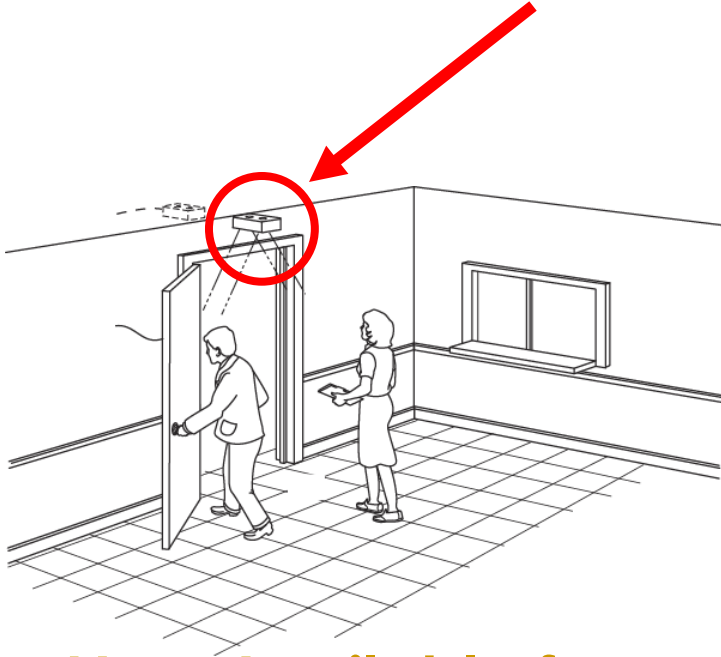
- Universal insertion and stand-off mount
- Ideal for small rooftop unit OA measurement (in hood or ducts)
- Perfect for ERVs
- Can be applied in most classroom unit ventilators
- T probe compatible (ELF with display)
- Two analog output signals
- Contact closure alarm





# CENSus<sup>®</sup>

## BACnet/Analog Room Occupancy (ie People) Counter



- IR-based device to count people as they enter & exit a room
- First release is for interior single zones (ie classroom or movie theater) with one or two doors
- Combine with the outdoor airflow measurement for real-time DCV
- Result: Energy Savings with DCV that meets the 'Spirit & Letter' of the building codes and standards

**Now Available for  
Single Rooms**

**Looking for BETA Test  
Sites!**



# CENSus<sup>®</sup>

## Application Criteria

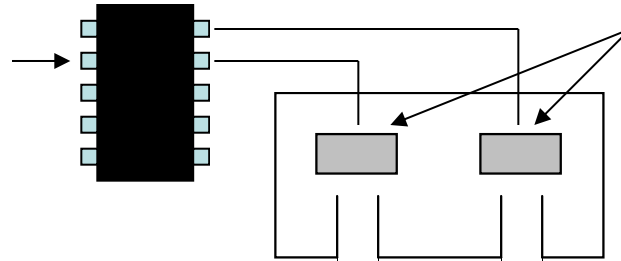
- Designed for spaces with a design of 15 or more occupants.
- Doors/Opening must meet specific criteria (first version).
  - 36” width maximum
  - 7 ft. height maximum (other heights are being evaluated)
  - Door must open away from counter (limits applications if counter is in high traffic hallway).
  - Door closers must not cross the plane of the sensors.
- Requires door mounted sensor.
  - First release will be for single doors.
  - Not recommended to replace occupancy sensors for lighting control.



# CENSus<sup>®</sup>

## How it works

A high speed microprocessor with ADC processes signals in real-time



Two thermopiles measure thermal signature and event time

Entry event thermal signature

energy

Focus slots

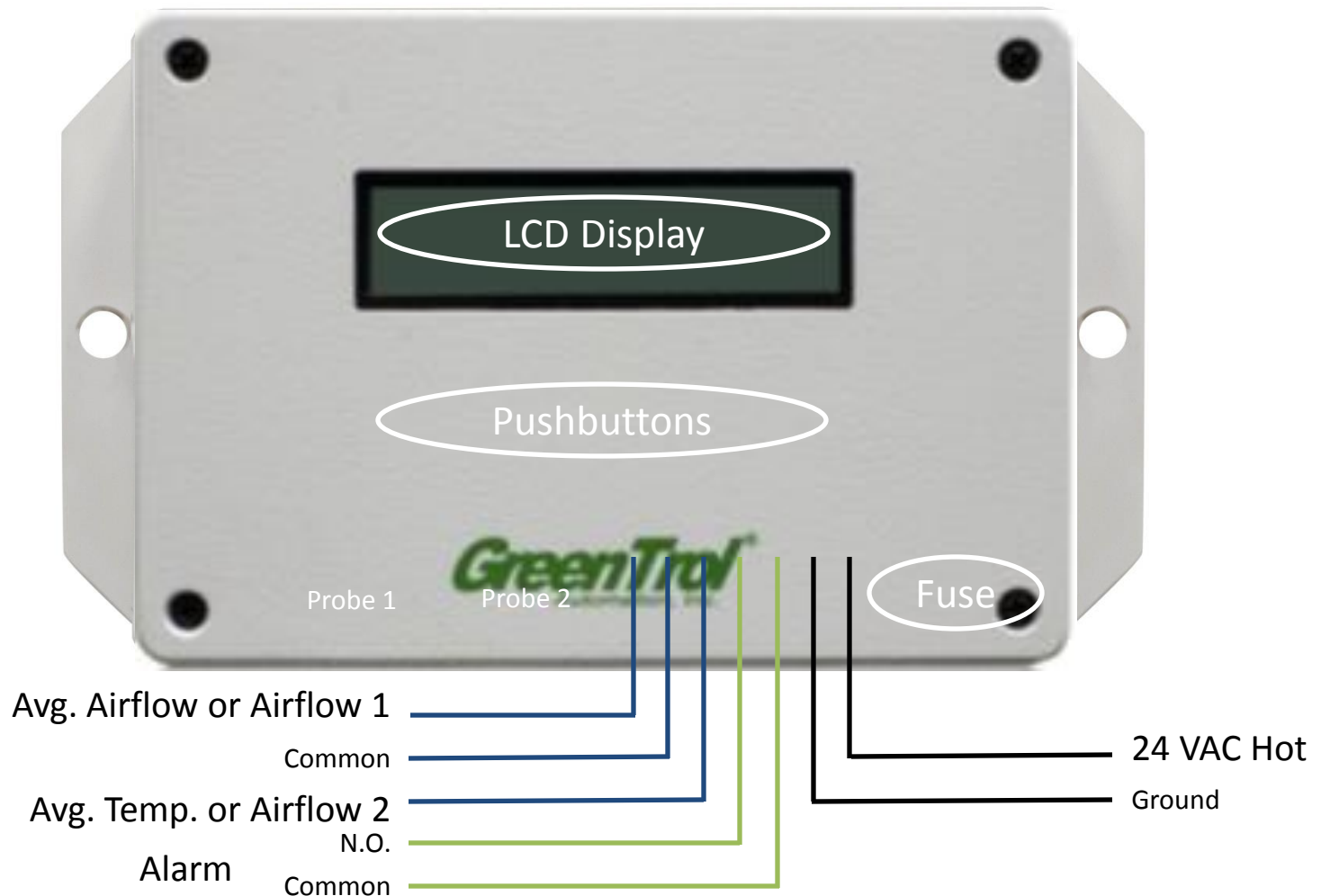
Exit event thermal signature

time



# Airflow Transmitters

**GF-A2000** (accepts up to 2 probes & 2 total sensors)







ALRT-200

ALRT-100

## Alarms and Bridges

### ALRT-200

- Programmable remote display
- Visible and contact closure alarm
- Analog to RS-485 bridge (BACnet and Modbus)

### ALRT-100

- Visible (LED) and contact closure alarm accepts 0-10 or 4-20 mA signal



**EBTRON** Presents...  
**BRING - A - GUEST**   
The Myrtle Beach Seminar for IEQ



**2015 Seminar Dates:**

- May 14<sup>th</sup> to 16<sup>th</sup>
- September 10<sup>th</sup> to 12<sup>th</sup>
- October 22<sup>nd</sup> to 24<sup>th</sup>

Arrive: Thursday afternoon  
Depart: Saturday evening or Sunday

# Agenda

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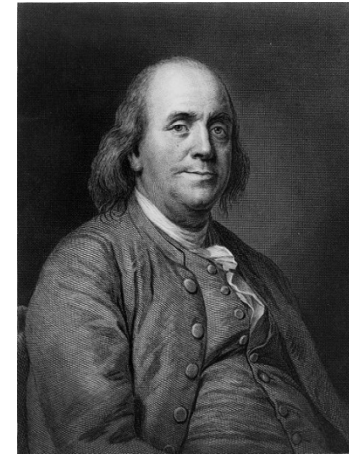
- I. Why Measure & Control Outdoor Air Delivery?
- II. Analyze Alternatives:
  - A. Fixed Outdoor Air Damper Position  $\neq$  Control
  - B. Supply Air – Return Air  $\neq$  Outdoor Air
- III. Outdoor Airflow Control Improves CO<sub>2</sub>-based Ventilation Control Systems
- IV. Outdoor Air Delivery Design Guidelines
- V. Selecting Outdoor Airflow Monitors
- VI. Applying for LEED 2009 IEQ Credit 1, Outdoor Air Delivery Monitoring

# Benefits of Measuring and Controlling Outdoor Air Intakes

# Proper Ventilation Helps Ensure a Comfortable, Healthy, & Productive Indoor Environment

---

Benjamin Franklin  
On Fresh Air, 1785



*“ I considered (fresh air) as an enemy and closed with extreme care every crevice in the rooms I inhabited.*

*Experience has convinced me of my error. I now look upon fresh air as a friend. I even sleep with an open window.*

*I am persuaded that no common air from without, is so unwholesome as the air within a close(d) room that has been often breathed and not changed.”*

Letter from Benjamin Franklin to Dr. Ingenhaus physician to the emperor in Vienna

Quote found in Real Estate Law (Thomson/Southwestern) Jennings, 2008 & 2005: pg 229, Chapter 10: Commercial Leases: Condition of the Premises – The Sick Building Syndrome



# Ventilation Standards and Codes

---

- ASHRAE 62.1, Ventilation for Acceptable IAQ
  - Designers must choose compliance under one procedure from Section 6.
    - Ventilation Rate Procedure
      - A prescriptive, **ventilation rate based** procedure that specifies breathing zone outside airflow rates based on space type/application, population and floor area.
      - Typically selected by engineers and owners
    - Indoor Air Quality Procedure
      - A subjective procedure, often requiring expensive and sophisticated monitoring equipment.
      - Not all contaminants of concern may be recognized or monitored, thus exposing occupants to risk.
      - Not recognized by LEED 2009 for Mechanically Ventilated Systems!

# Ventilation Standards and Codes

---

- International Mechanical Code (IMC)
  - Strict compliance with the ventilation rate procedure (VRP) of ASHRAE 62.1
    - Current version has adopted 62.1
    - IMC does not recognize the 62.1's IAQ Procedure
    - Most, if not all, jurisdictions reference older versions of IMC
      - Prior to 2004, IMC's ventilation standard only included the per person ventilation portion and did not include the per ft<sup>2</sup> ventilation rate
      - Presents a conflict for designers since older versions reference the standard prior to 2004. Ventilation rates were calculated differently at that time.

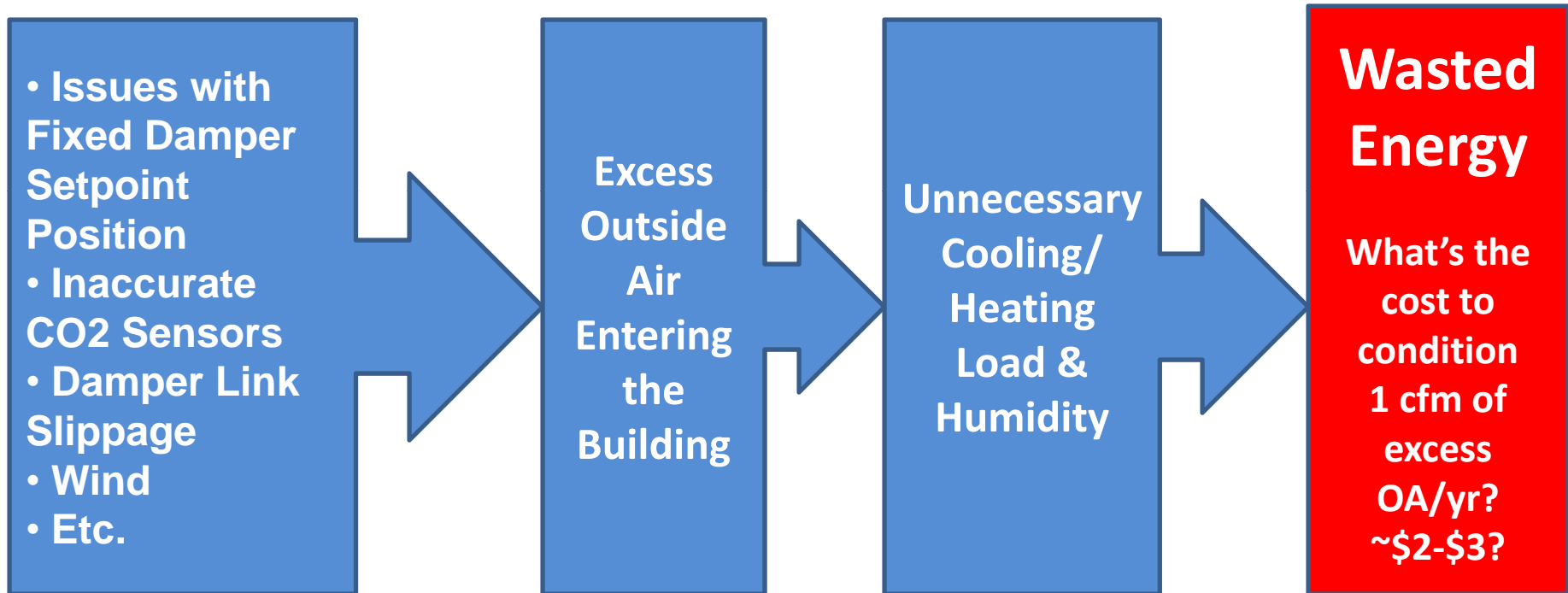


# *Controlling* Outdoor Air Intakes Ensures Compliance to Ventilation Codes and Standards

- Measurement & Verification provides documented proof of compliance
- Cannot control what is not measured
- Outdoor Air Delivery Monitoring is required or recommended by:
  - ASHRAE 62.1 in VAV Systems
  - LEED 2009
  - Local Statutes like Minnesota 123B.71 – Schools
  - ASHRAE 189.1

# Controlling Outdoor Air Intakes Prevents Wasted Energy Caused by Over-Ventilation

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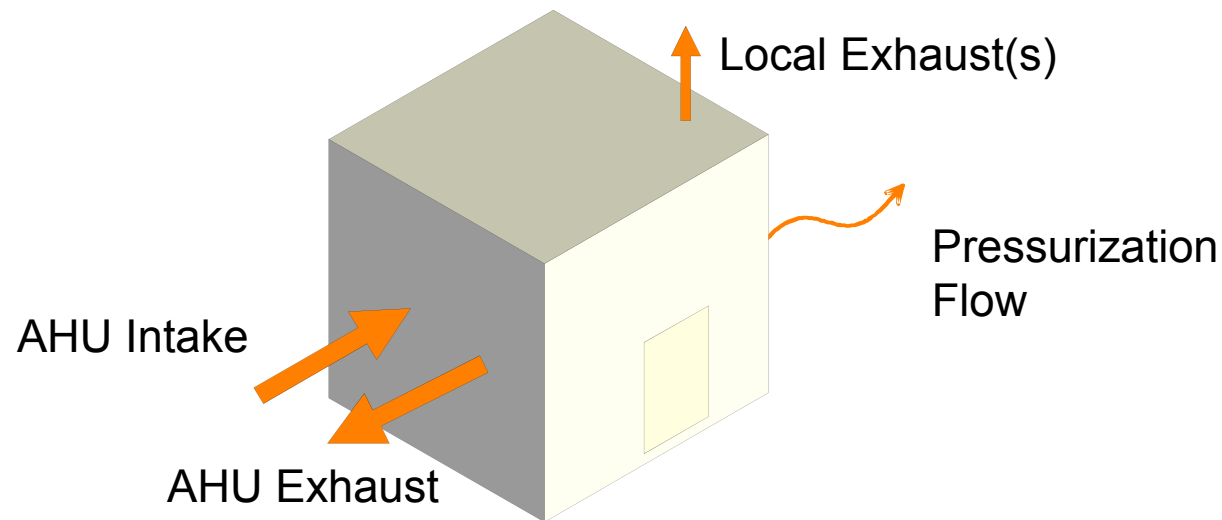


Bringing in more outside air than predicted costs \$'s  
300 cfm of extra outdoor air can cost \$600-\$900 or more per year!

# Outdoor Air Delivery is the Key to Maintaining Building Pressurization

---

- Pressurization Flow – Delivering more outside air into the building than is being exhausted
- Only the mechanical ventilation system can pressurize your building



**Net Building Pressure = Pressurization Flow = In - Out**

# Control Building Pressure to Reduce Contaminants

Negatively pressurized buildings use the building envelope as the first stage of filtration!



## Contaminant Sources:

- school bus loading areas
- sewer vents
- exhaust air from the school
- loading docks
- garbage receptacles
- boiler or generator exhausts
- mist from cooling towers



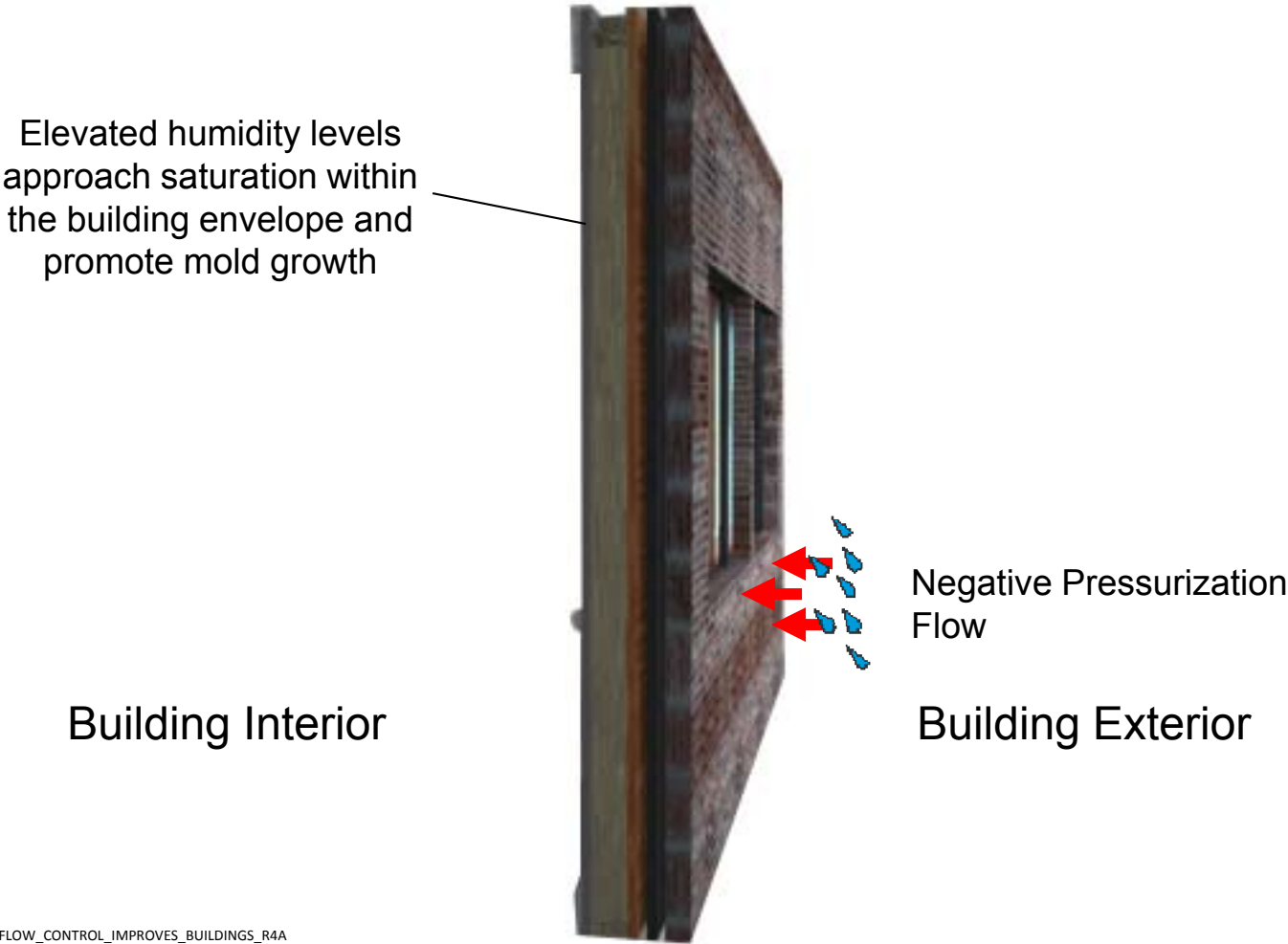
Negative Pressurization  
Flow

Building Interior

Building Exterior

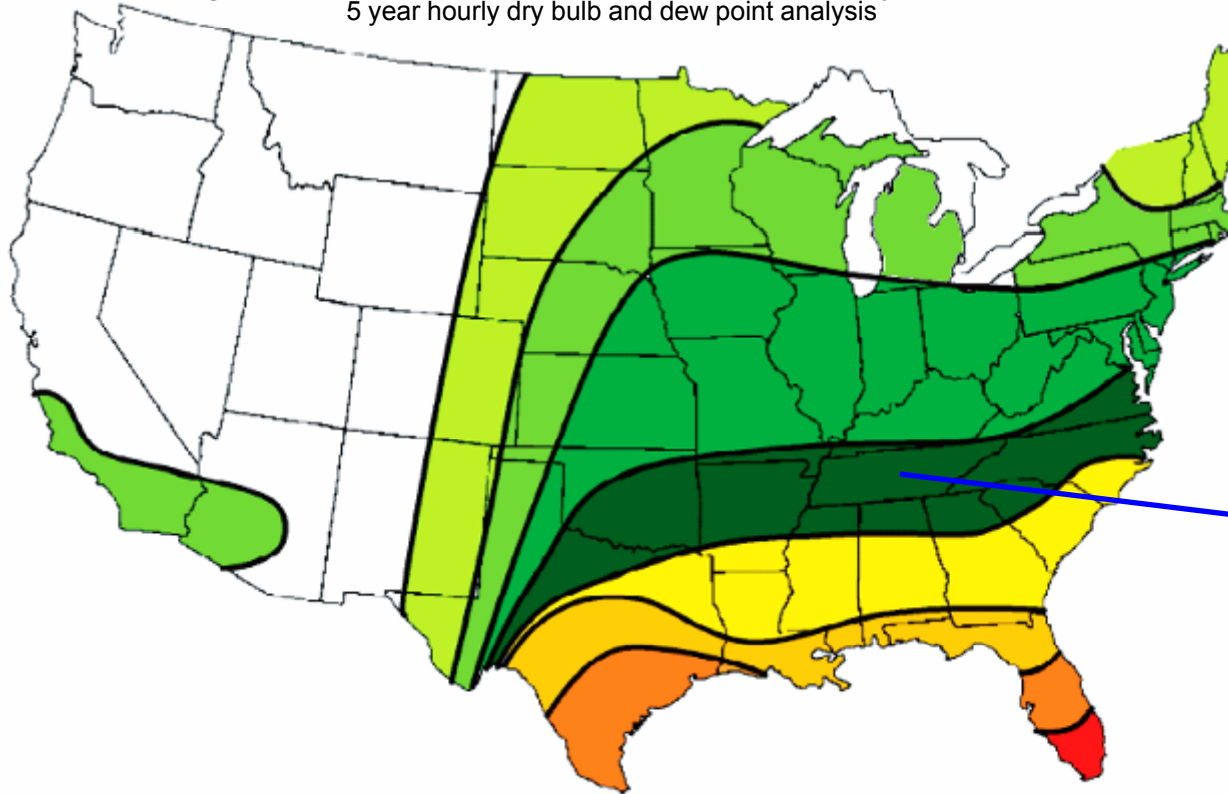
# Control Building Pressure to Reduce Mold

Mold growth may occur in negatively pressurized buildings when the outside air dew point is greater than 65 °F



# Control Building Pressure to Reduce Mold

**Mold Growth Potential**  
Percentage of time that the envelope humidity can exceed 70%\*  
5 year hourly dry bulb and dew point analysis

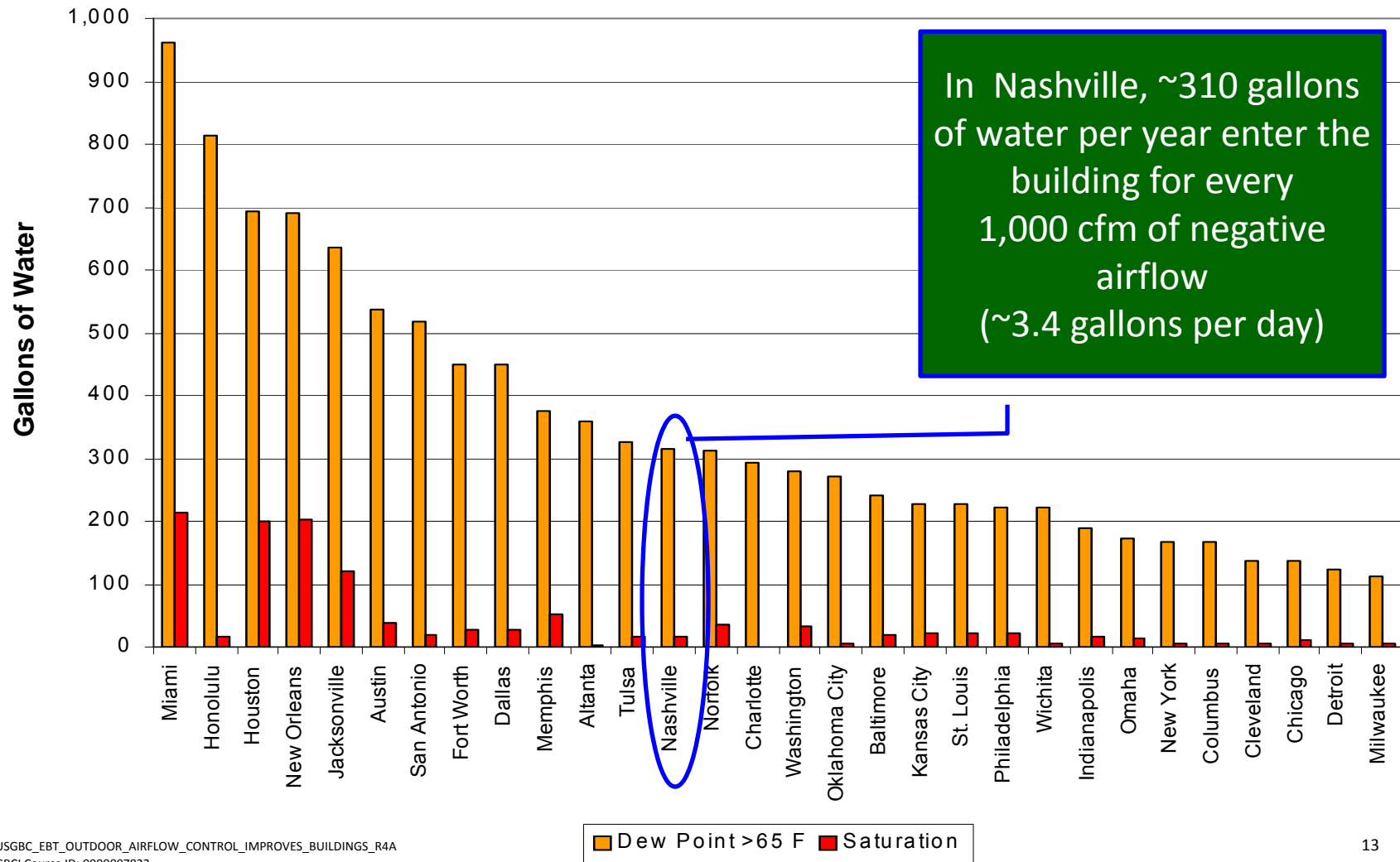


In TN, Conditions are Favorable for Mold Growth 20-30% of the Time (~91 days per year)



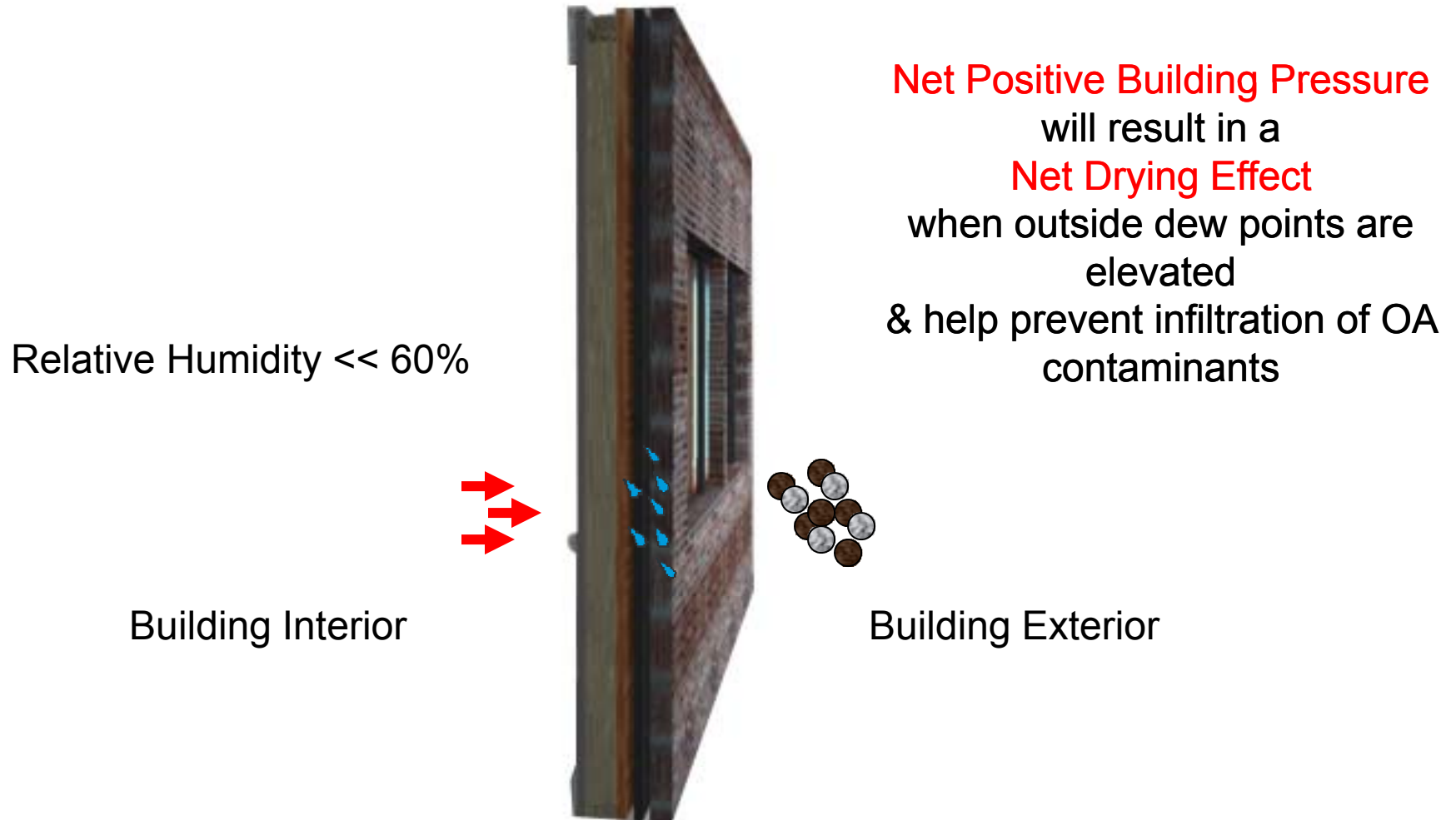
\* Based on an indoor temperature of 74 F and an outdoor dew point  $\geq$  65 F  
Data provided to EBTRON courtesy of the Forecast Institute, Inc.

## Annual Gallons of Water Transported Across the Building Envelope for every 1,000 CFM of Negative Airflow First 30 of top 50 US Cities by Population (2000 Census)



# Building Pressure Is Key to Indoor Environment Quality

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**Recommendation: Keep Building NET POSITIVE**



# Outdoor Air Control Helps Meet the Intent of LEED 2009: Better Performing Buildings

Prerequisite or Credit	Description	NC	SCHOOLS	CS
EA Prerequisite 1	Fundamental Commissioning	Required	Required	Required
EA Prerequisite 2	Minimum Energy Performance	Required	Required	Required
EA Credit 1	Optimize Energy Performance	1-19 points	1-19 points	3-21 points
EA Credit 3	Enhanced Commissioning	2 points	2 points	2 points
EA Credit 5	Measurement and Verification	3 points	2 points	NA
IEQ Prerequisite 1	Minimum IAQ Performance	Required	Required	Required
IEQ Prerequisite 2	ETS (tobacco smoke) Control	Required	Required	Required
IEQ Prerequisite 3	Minimum Acoustical Performance	NA	Required	NA
<b>IEQ Credit 1</b>	<b>Outdoor Air Delivery Monitoring</b>	<b>1 Point</b>	<b>1 Point</b>	<b>1 Point</b>
IEQ Credit 2	Increased Ventilation	1 Point	1 Point	1 Point
IEQ Credit 3/3.1	Construction Management Plan (constr.)	1 Point	1 Point	1 Point
IEQ Credit 3.2	Construction Management Plan (occup.)	1 Point	1 Point	NA
IEQ Credit 6.2	Controllability of Systems - Thermal	1 Point	1 Point	1 Point
IEQ Credit 7/7.1	Thermal Comfort - Design	1 Point	1 Point	1 Point
IEQ Credit 7.2	Thermal Comfort - Verification	1 Point	1 Point	NA
IEQ Credit 9	Enhanced Acoustical Performance	NA	1 Point	NA
IEQ Credit 10	Mold Prevention	NA	1 Point	NA
ID Credit 1	Innovation in Design	1-5 points	1-4 points	1-5 points



# LEED 2009, IEQ Credit 1

## Outdoor Air Delivery Monitoring

	NC	SCHOOLS	CS
Credit	IEQ Credit 1	IEQ Credit 1	IEQ Credit 1
Points	1 Point	1 Point	1 Point

**Intent:** To provide capability for ventilation system monitoring to help promote occupant health and well-being.

**Requirement:** Generate an alarm via either the BAS to the building operator or a visible or audible alert to the building occupants when values are more than +/-10% of design.

### MECHANICALLY VENTILATED SYSTEMS

#### Low Occupant Density Spaces (under 25 people per 1,000 sq.ft.)

- When 20% or more of the design supply airflow serves non-densely occupied spaces, provide a *direct* outdoor airflow measurement device capable of measuring the minimum outdoor air intake flow rate with an accuracy of +/-15% of reading.

#### High Occupant Density Spaces (> 25 people per 1,000 sq.ft.)

- Provide a CO<sub>2</sub> device within all high occupant density spaces.



# Standard 189.1-2009

---

## 8.3.1.2 Outdoor Air Delivery Monitoring

### 8.3.1.2.1 Spaces Ventilated by Mechanical Systems.

A permanently mounted, *direct total outdoor airflow measurement device* shall be provided that is capable of measuring the system *minimum outdoor airflow rate*.

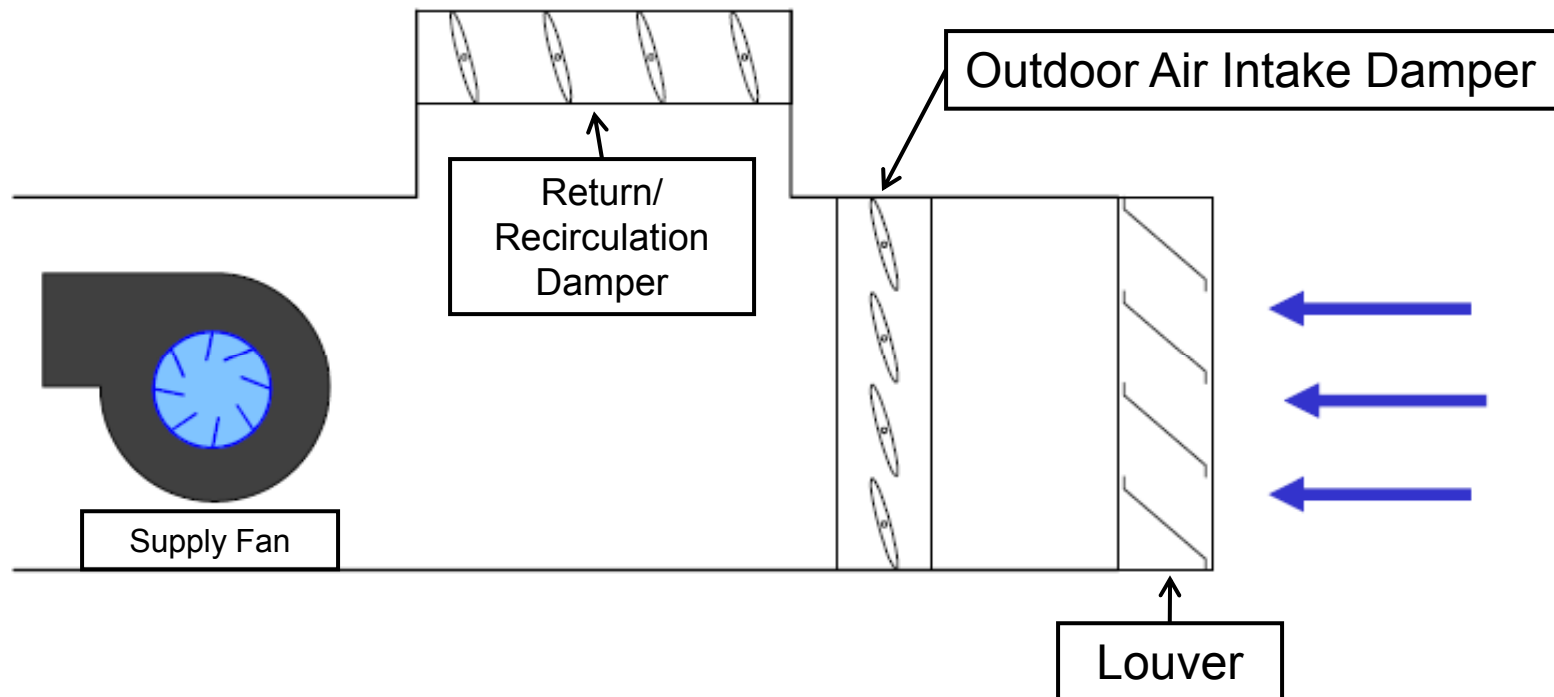
The device shall be capable of measuring flow within an accuracy of  $\pm 15\%$  of the *minimum outdoor airflow rate*. The device shall also be capable of being used to alarm the building operator or for sending a signal to a building central monitoring system when flow rates are not in compliance.

**Exception:** *Constant volume air supply systems that use a damper position feedback system* are not required to have a direct total outdoor airflow measurement device.

Fixed  
Outdoor Air  
Damper Position  
≠  
Control

# What is 'Fixed Outdoor Air Damper Position'?

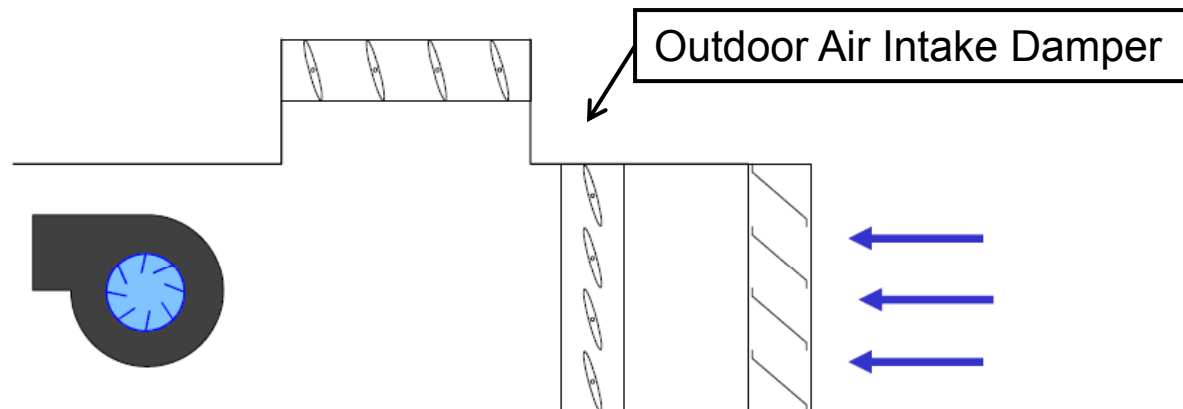
- During 'Occupied Mode', the Outdoor Air Intake Damper goes to a pre-determined '% Open'
- This method of 'control' is unfortunately used by an overwhelming majority of new and existing buildings



# Fixed Damper Position $\neq$ Control

Fixed Damper Setpoint Position is:

- Determined by 'Test And Balance' during initial commissioning
- Based on the minimum design airflow (i.e. building codes or ASHRAE 62.1)
- '% Open' kept throughout the building's life
- Rarely ever re-checked (i.e. retro-commissioned)



# Fixed Damper Position $\neq$ Control

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## Sources of Outdoor Air Intake Uncertainty with Fixed Damper Position

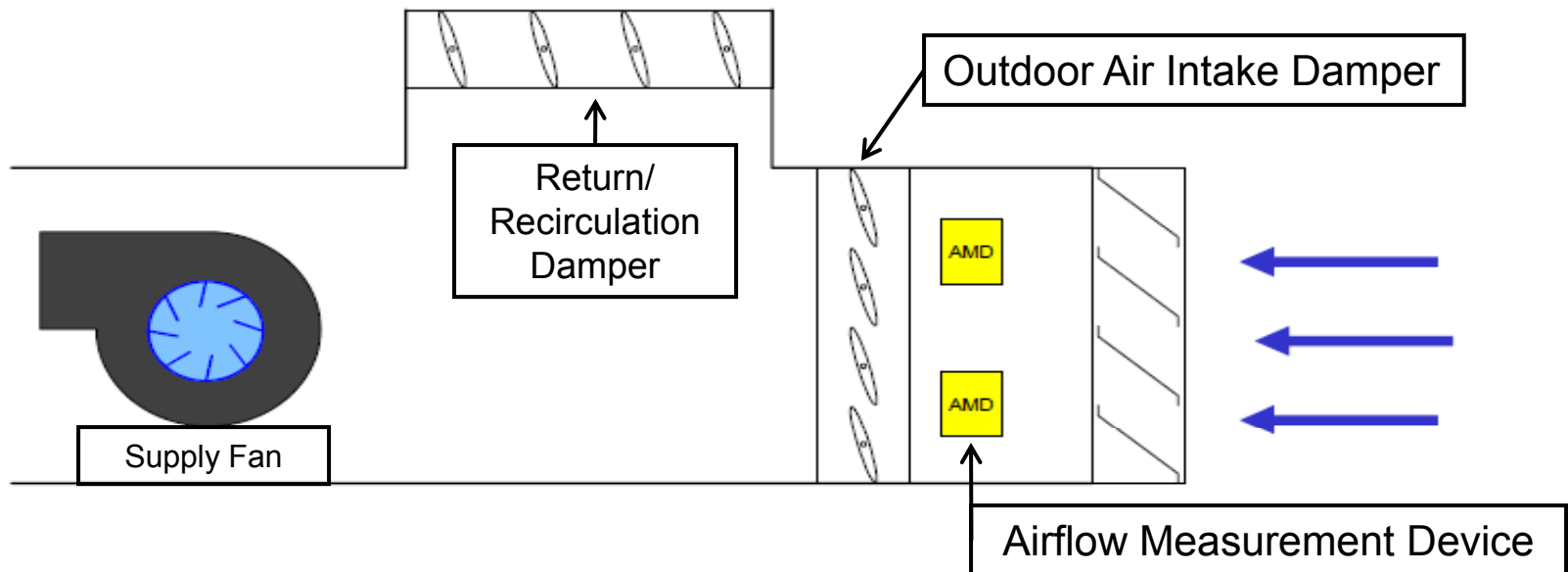
- Damper Hysteresis
  - Damper/Actuators don't always go back to the exact same position
- Wind Effect
- Stack Pressure
- Conditions at Time of Commissioning

# Damper Hysteresis Test: Damper 'Position' $\neq$ Desired Airflow

Step 1: A 'Fixed Damper Position' (15% open) was selected and the resulting airflow was recorded. This airflow will be the target (shown as 100% on the chart)

Step 2: Damper was moved fully open, then back to the damper setpoint position (15%) and the airflow measurement was taken (shown in red on the next slide)

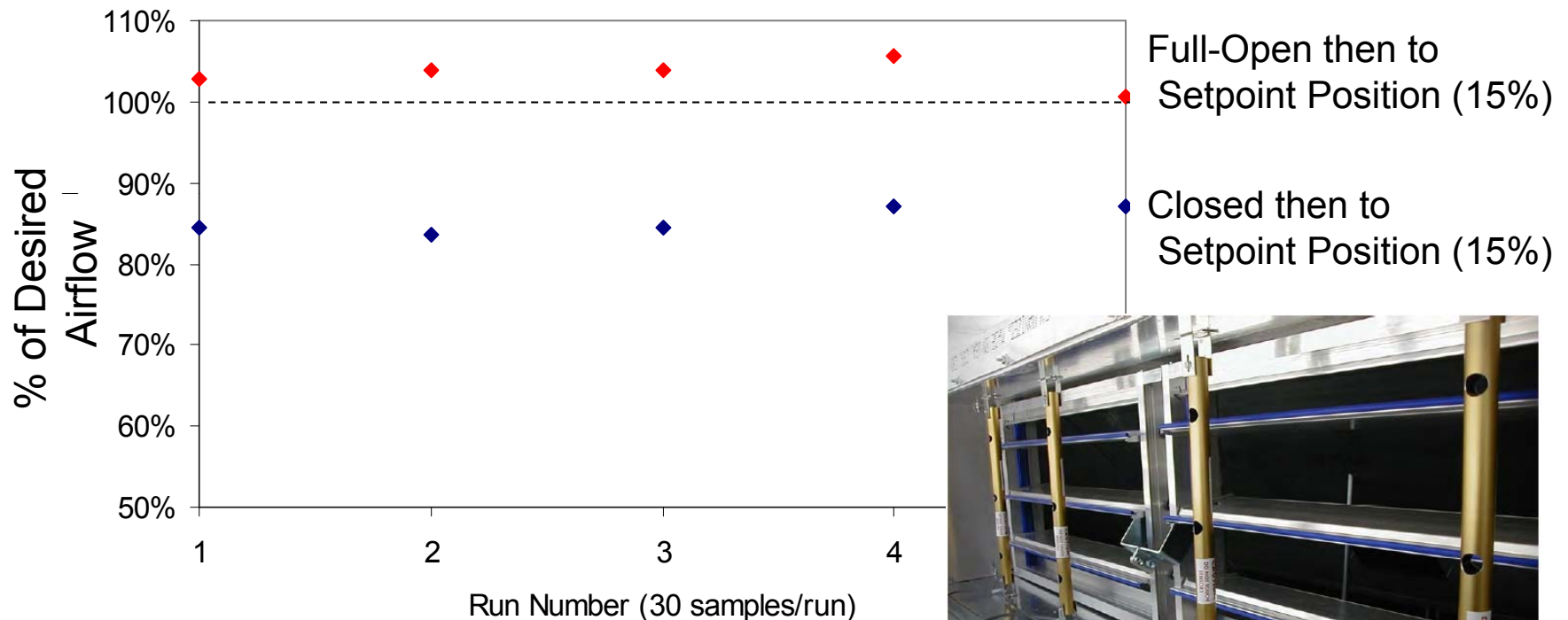
Step 3: Damper was closed. Then, moved back to the damper setpoint position (15%) and the airflow measurement was taken (shown in blue on the next slide)





# Damper Hysteresis Test Results: Position $\neq$ Desired Airflow

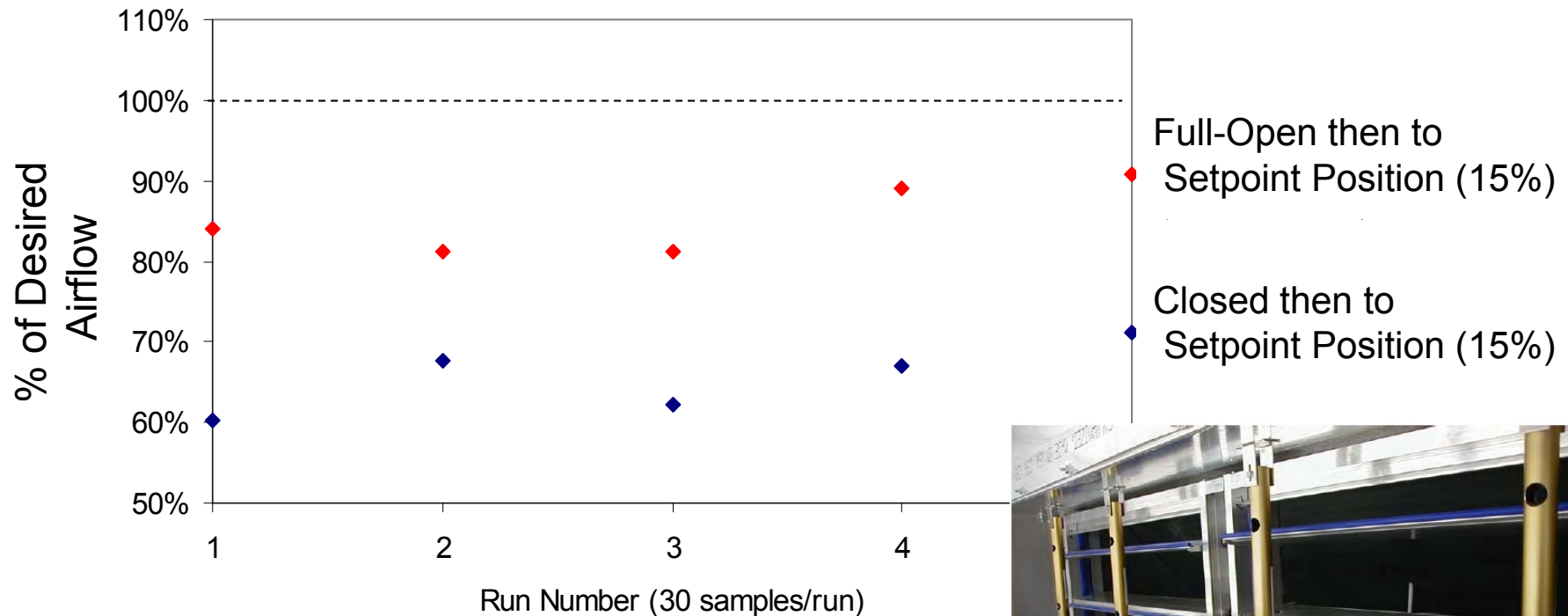
## Damper Hysteresis Test Results – Still Air



- Damper/Actuators don't always return to the exact desired position
- What is the airflow on Day 2 of operation (ie after the damper is closed at night)?

# Wind Effects Outdoor Air Intakes

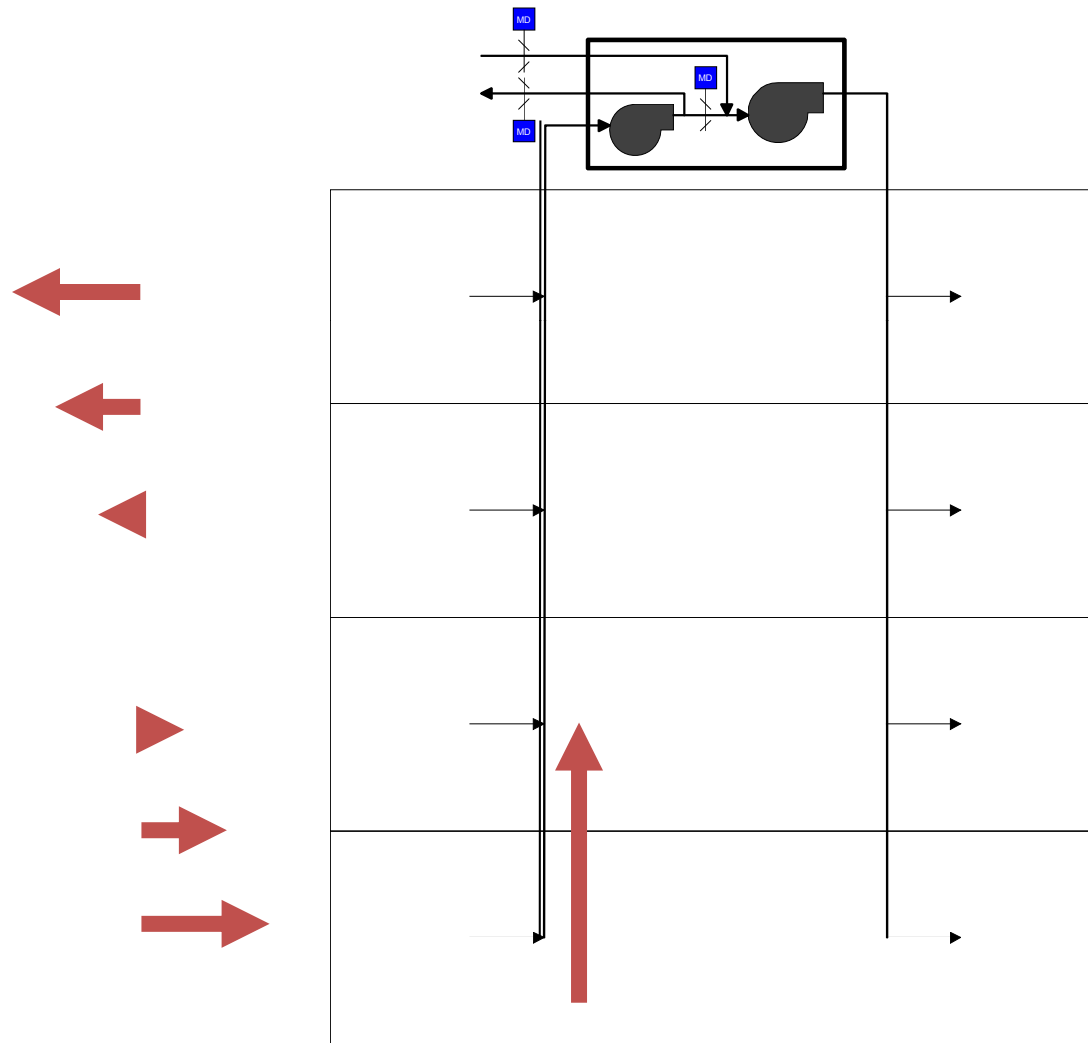
Damper Hysteresis Test Results – 15 mph Cross Wind



**What if the wind blows directly at the damper?**



# Stack Pressure Effects Outdoor Air Intakes



## Stack Effect in Winter

Warm air in the building rises pushing out on the outdoor air damper

### Question:

Will a damper setpoint position selected in the winter be valid in the summer?

# Fixed Damper Position ≠ Control

---

## Damper Setpoint Position Depends on Conditions at Time of Commissioning

What is wind speed?

What is the wind direction?

What is the indoor temperature?

What is the outdoor temperature?

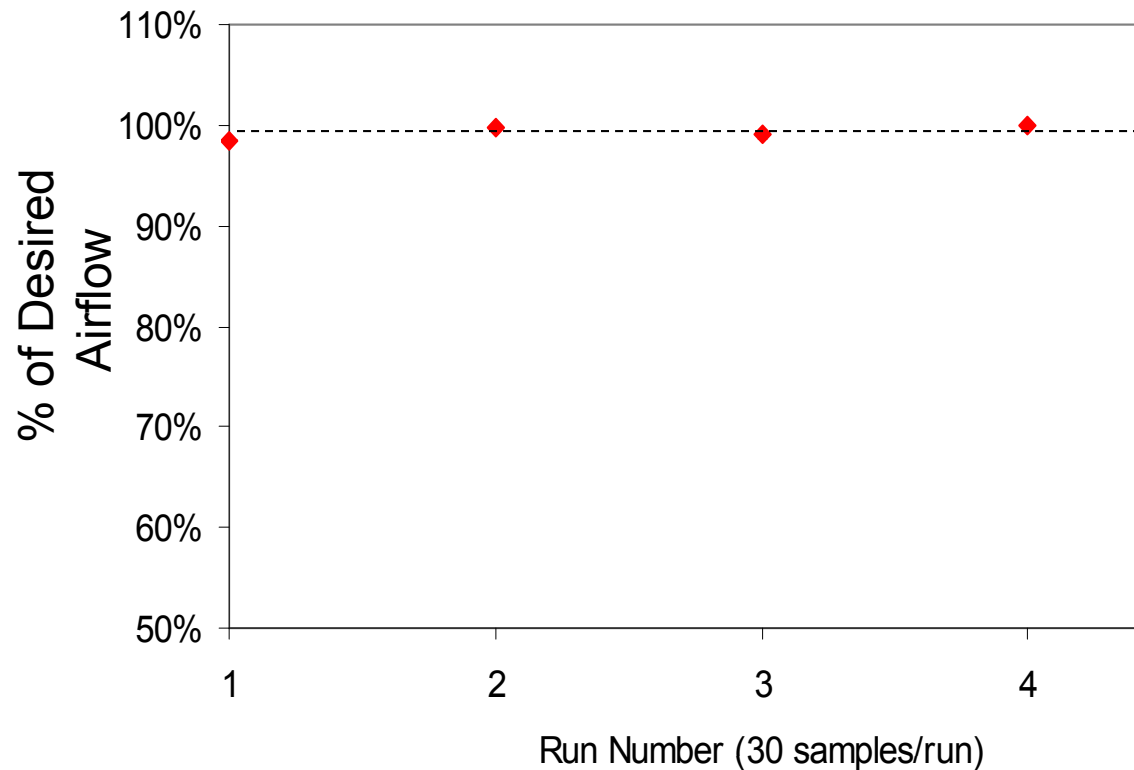
What is the damper hysteresis effect?

# Solution:

## Control Outdoor Intakes With Airflow Monitors

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Damper Under Active Control - Light & Variable Wind



**Requires Accurate & Stable Airflow Measurement**

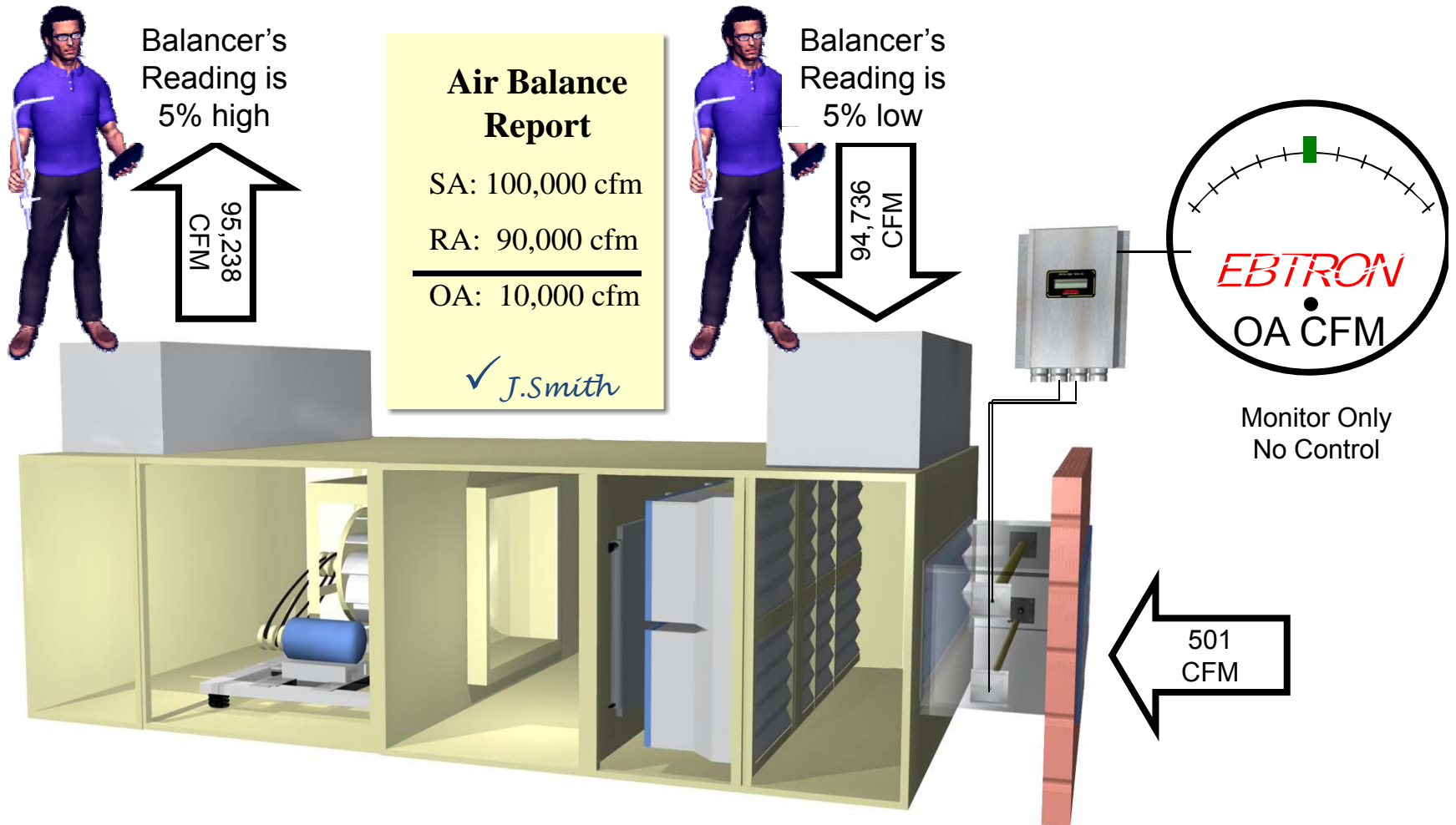
# Why Measure OA when Measuring SA & RA?

## Supply Air – Return Air $\neq$ Outdoor Air

---

- LEED 2009 IEQ-1 and ASHRAE 189.1 say to:  
*‘Provide a **Direct** Outdoor Airflow Measurement Device’*
- Numerous systems assume that SA-RA = OA, so OA is calculated, not measured
- Small errors in the SA or RA measurements result in large OA calculation error (see the following example)

# Directly Measure Outdoor Air Even When Measuring Supply & Return Airflows



- $SA - RA = OA$  uses the difference between two large airflows to calculate OA
- Small errors in measure SA & RA lead to large errors when calculating OA



# Overcome Issues with CO<sub>2</sub>-based Ventilation Control Using Outdoor Air Delivery Monitoring & Control

## 2 Issues with CO2-based Ventilation Control

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- Always want enough outdoor air entering the building during occupied mode to maintain building pressurization

- CO2 readings only indicate per person ventilation rates

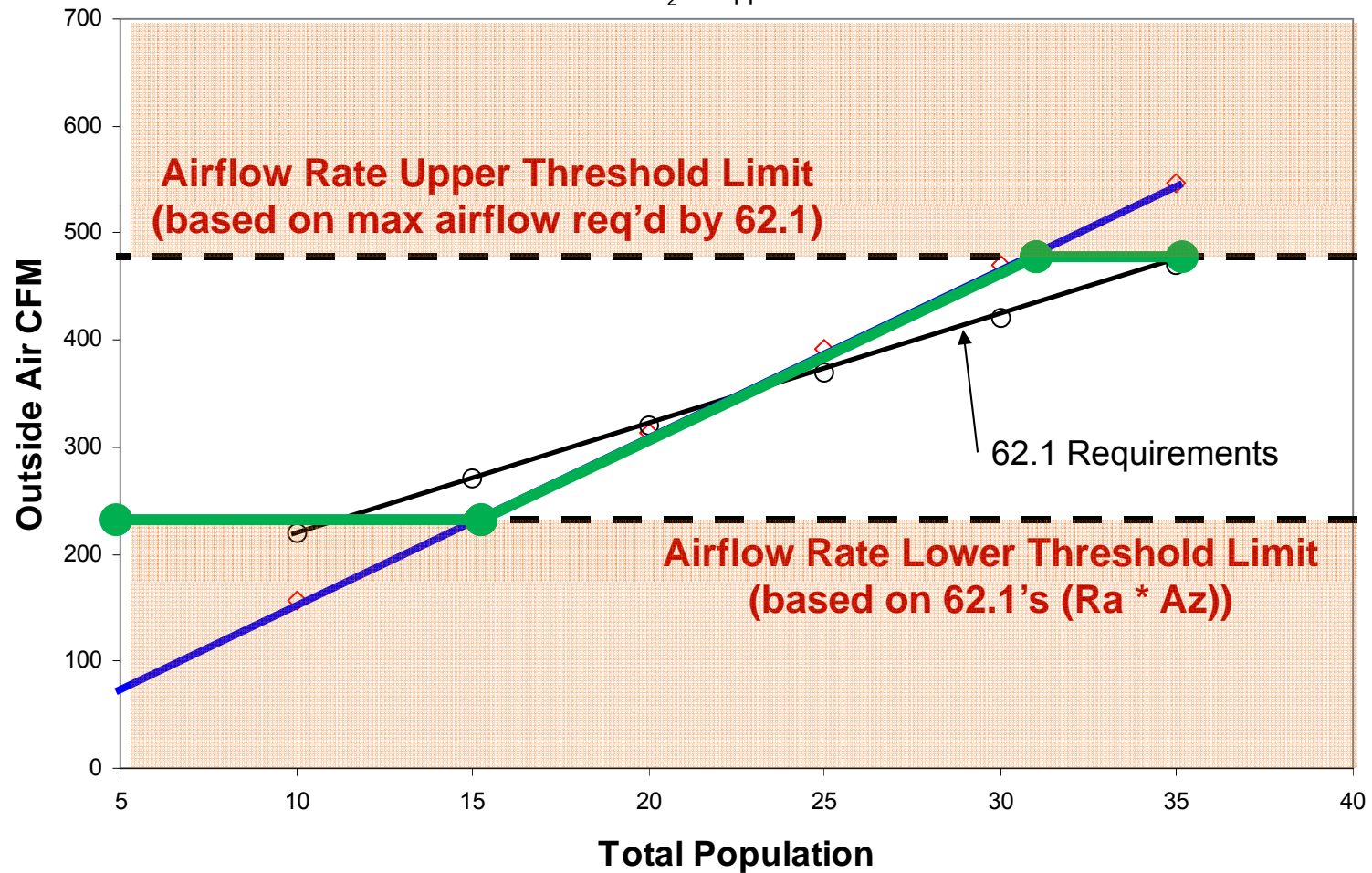
$$V_{bz} = R_p \cdot P_z + R_a \cdot A_z$$

- Never want to bring in more outdoor air than desired
  - Inaccurate or 'drifting' CO2 sensors may ask for more than necessary outdoor air

# Use Airflow Monitors to put 'Bounds' on CO2-based DCV's Airflow Adjustments

## Single Classroom

Assumptions: Steady-state,  $N=0.31$ , Sensor Uncertainty= $\pm 0$  ppm,  
OA  $CO_2=400$ ppm



# Outdoor Air Control Design Guidelines



# Outside Air Intake Guidelines

---

Follow these basic rules for success:

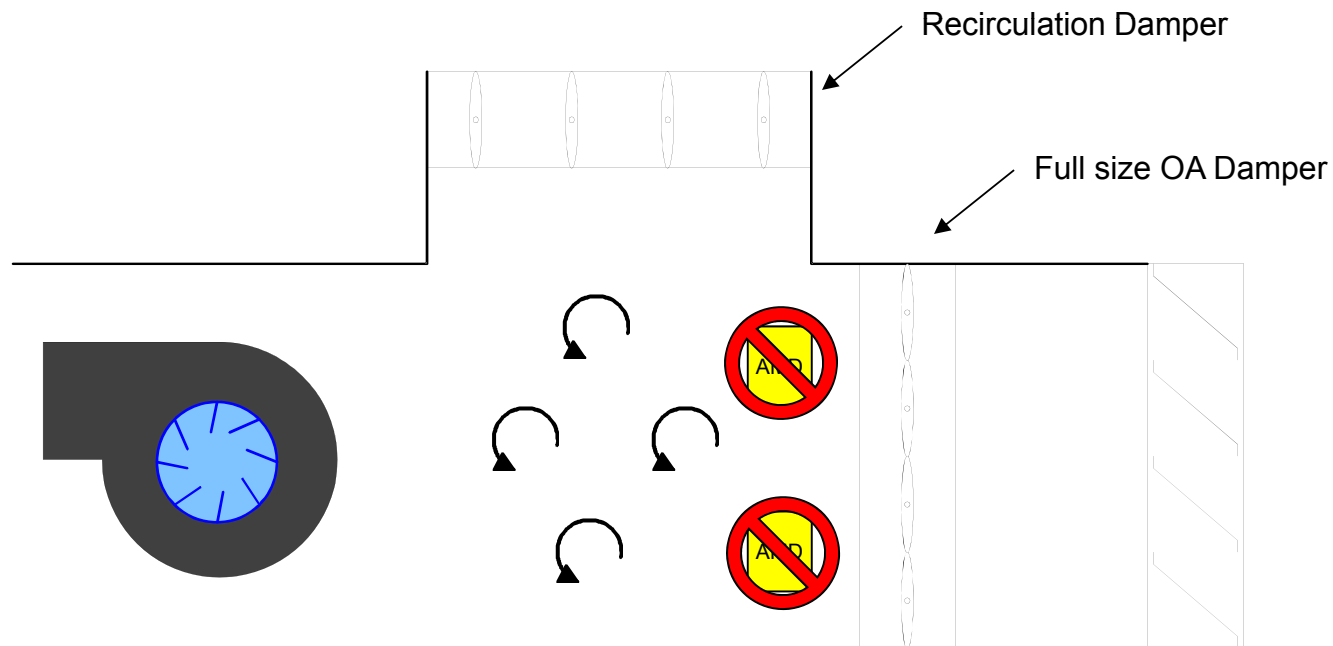
- Select and **apply** airflow measuring devices suited for the measurement of intake flow rates.
  - Make certain the flow meter can measure the outdoor air intake flow rates
  - **Make certain that the flow rates are high enough to control and are not affected by transient wind gusts (> 150 FPM at minimum [ 200 FPM preferred] )**
- Select and size quality control dampers.
  - Use high quality, extruded aluminum blades, with long-lasting and non-binding linkage
- Implement a control strategy that optimizes the performance of the system
  - **Use the right sequences and slow it down!**

# Outside Air Intake Guidelines

Turbulence in the mixed air plenum from fans and dampers can result in false airflow readings.



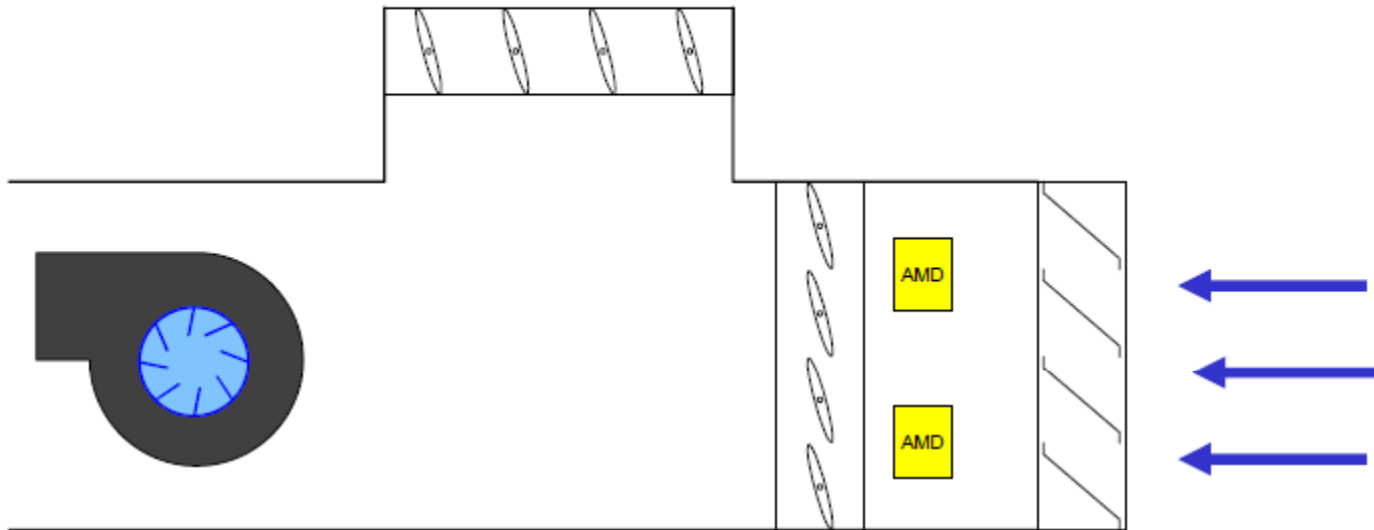
**Do NOT** measure airflow rates downstream of the intake damper or near the mixed air plenum!



# Outside Air Intake Guidelines

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Always place the airflow measuring station UPSTREAM of the intake damper.

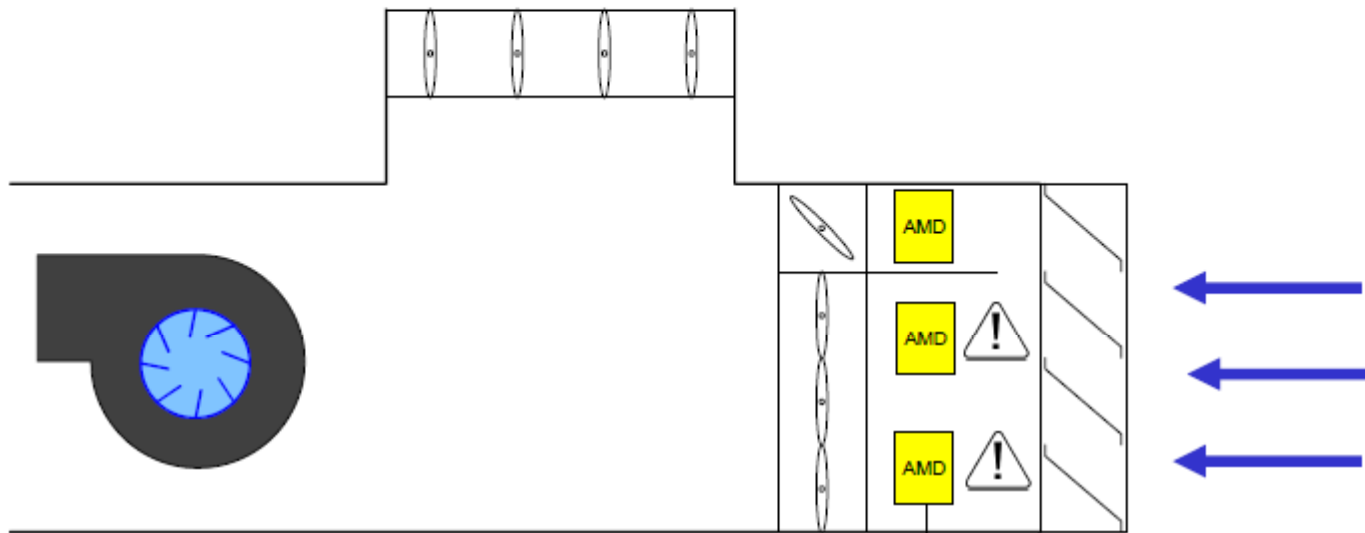


# Outside Air Intake Guidelines

Consider using Min/Max dampers to improve measurement and control of OA intake

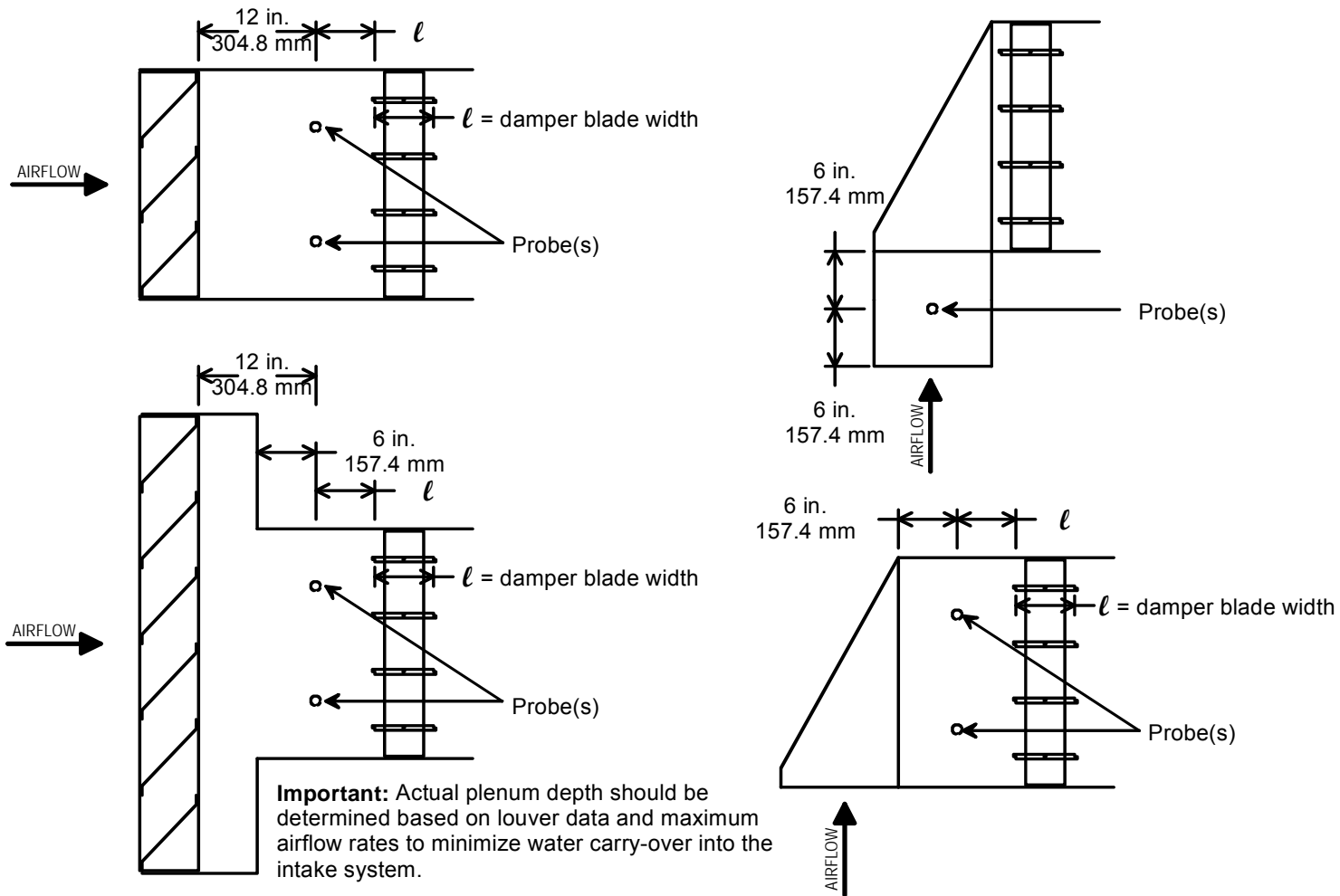


OA intake flow rates may not be accurately determined on max. damper as max. damper flow rate approaches 0 FPM as a result of wind effect on AMD!





# Outside Air Intake Placement Guidelines



Guidelines shown are for one manufacturer  
Not typical for all airflow monitors

# Selecting & Specifying Outdoor Airflow Monitors

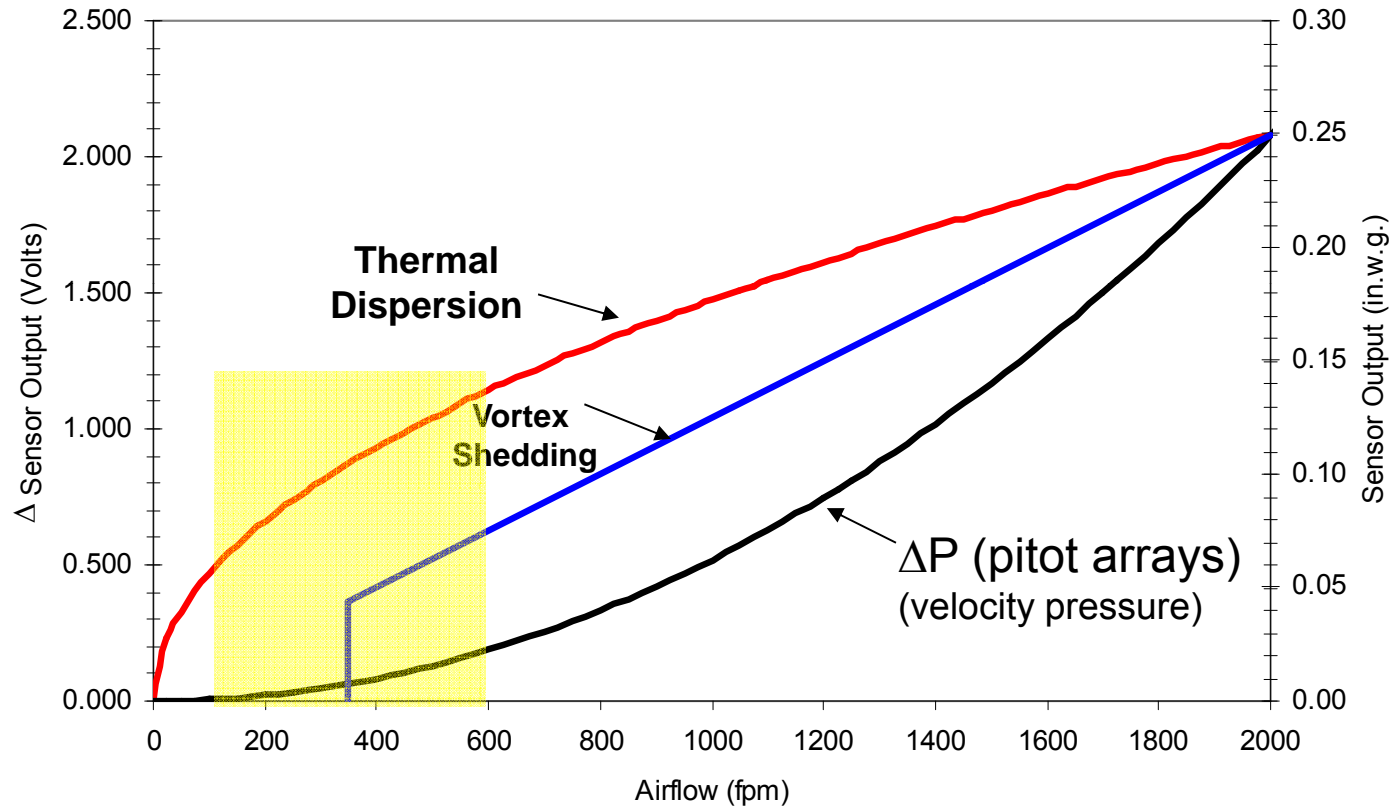
# What's important?

---

1. Suitability for Application
  - a) Desired Airflow
  - b) Minimum Placement Guidelines
2. Total Installed Accuracy
3. Repeatability (i.e. Long-Term Stability)
  - a) Long-Term Drift
  - b) Recommended Calibration Interval
4. Application Support
5. Cost
6. Reliability
7. Ease of Installation
8. Service and Support

# Technology Comparison

## Thermal Dispersion vs. $\Delta P$ vs. Vortex Shedding

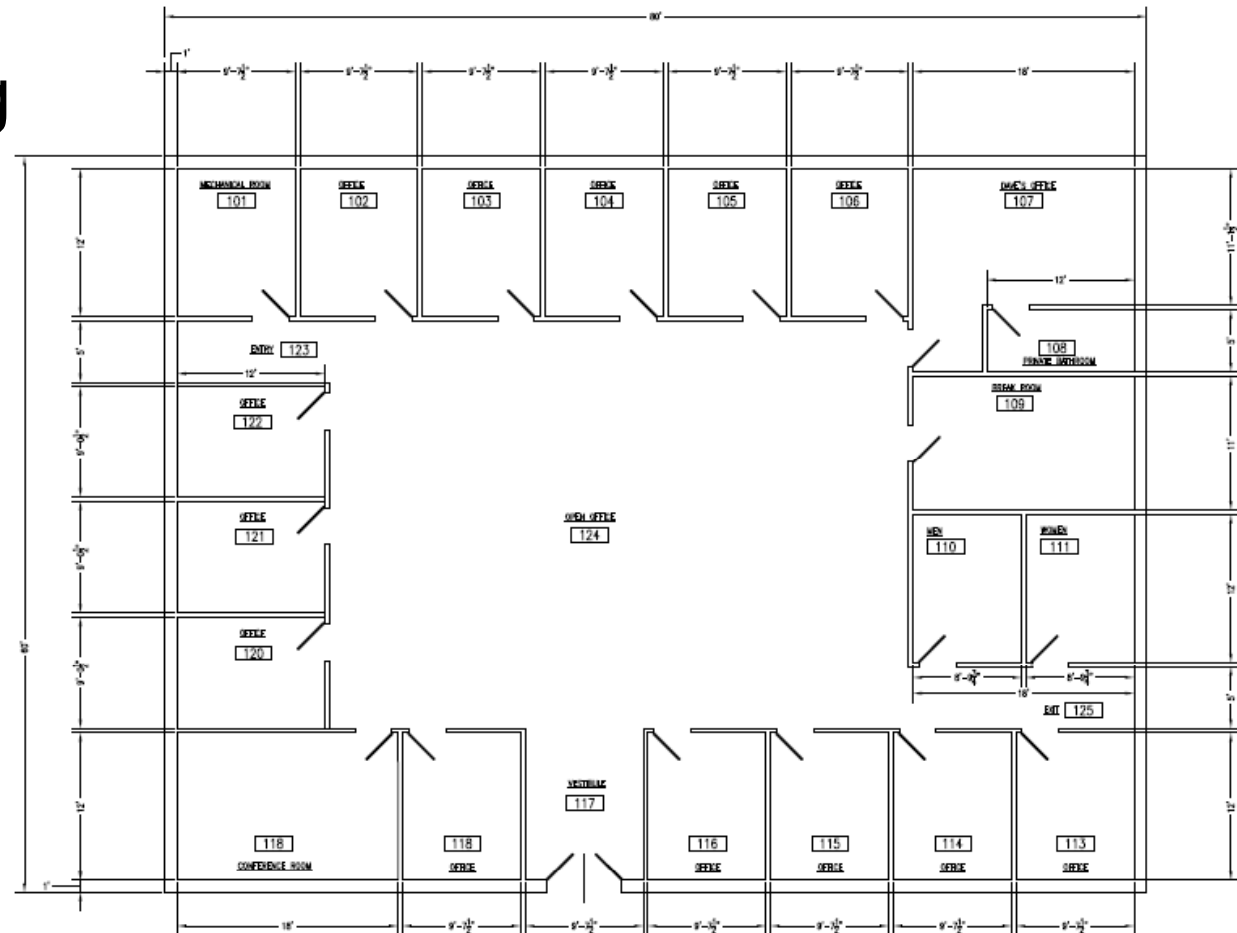


**Thermal Dispersion has the Best Sensitivity at Low Airflows**  
**Outdoor Air Intakes typically 150 to 600 fpm velocity**

# Applying for LEED 2009 IEQ Credit 1: Outdoor Air Delivery Monitoring Example: Office Building

# Example: Applying for LEED 2009 IEQ 1

Office Building  
Single-Zone  
4,800 SF  
22 People



# LEED 2009 IEQ Credit 1 Template



## LEED for New Construction: Design IEQ CREDIT 1: OUTDOOR AIR DELIVERY MONITORING

*All fields and uploads are required unless otherwise noted.*

A Licensed Professional Exemption (LPE) is available for Professional Engineers in lieu of providing plans, drawings, information on AHUs, and confirmations that monitors are installed and programmed appropriately.

Select one of the following:

Streamlined Path: LPE (PE).

Full Documentation.



Select all that apply to the project building:

The project building is mechanically ventilated, in part or in whole.

The project building is naturally ventilated, in part or in whole.

# LEED 2009 IEQ Credit 1 Template

---

## MECHANICAL VENTILATION

Upload a completed ASHRAE 62.1-2007 calculator OR a local version of the calculator that is at least as stringent as the ASHRAE version.

Upload

Files: 0

Select all that apply to the project building:

- Project building contains non-densely occupied spaces
- Project building contains densely occupied spaces

## NON DENSELY OCCUPIED SPACES

Upload a controls drawing sample showing the outdoor air flow measurement devices that serve non-densely occupied spaces.

Upload

Files: 0

Complete the table below for all mechanical ventilation systems where 20% or more of the design supply airflow serves non-densely-occupied spaces.



# LEED 2009 IEQ Prerequisite 1 Template



## LEED 2009 for New Construction and Major Renovations IEQ PREREQUISITE 1: MINIMUM INDOOR AIR QUALITY PERFORMANCE

Project # 1000009390 Building F

*All fields and uploads are required unless otherwise noted.*

### ALL OPTIONS

Select all that apply to the project building:

- The project building is mechanically ventilated, in part or in whole.
- The project building is naturally ventilated, in part or in whole.
- The project building is mechanically conditioned, in part or in whole.
- The project building is naturally conditioned, in part or in whole.

The project meets Sections 4 through 7 of ASHRAE 62.1-2007, Ventilation for Acceptable Indoor Air Quality.

#### REQUIRED SIGNATORY

Initial here:

VENTILATION  
SYSTEMS  
DESIGNER

# ASHRAE 62.1-2007 Outdoor Air Calculation

---

Step 1: Determine Calculation Variables

System =	Single-Zone Constant Volume
Function =	Office Space
Per Person Vent Rate ( $R_p$ ) =	5 cfm/person
Per SF Vent. Rate ( $R_a$ ) =	0.06 cfm/ft <sup>2</sup>
Floor Area ( $A_z$ ) =	4,800 ft <sup>2</sup>
Zone Population ( $P_z$ ) =	22 people

Step 2: Determine Breathing Zone Outdoor Air Requirement ( $V_{bz}$ )

$$V_{bz} = R_p * P_z + R_z * A_z$$
$$V_{bz} = (5 * 22) + (0.06 * 4,800)$$
$$V_{bz} = 398 \text{ cfm}$$

Step 3: Determine Zone Ventilation Effectiveness ( $E_z$ )

$$E_z = 1.0 \text{ per Table 6-2 in Standard 62.1-2007}$$

# ASHRAE 62.1-2007 Outdoor Air Calculation

---

Step 4: Calculate the Zone Outdoor Airflow ( $V_{oz}$ )

$$\begin{aligned}V_{oz} &= V_{bz} / E_z \\V_{oz} &= 398 / 1.0 \\V_{oz} &= 398 \text{ cfm}\end{aligned}$$

Step 5: For single zone systems, Calculate the Outdoor Air Intake Flow ( $V_{ot}$ )

$$\begin{aligned}V_{ot} &= V_{oz} \\V_{ot} &= 398 \text{ cfm}\end{aligned}$$

# LEED 2009 IEQ Prerequisite 1 Template

## MECHANICAL VENTILATION

Mechanical ventilation systems are designed using local code, which is more stringent than the ASHRAE Standard 62.1-2007 Ventilation Rate Procedure. (Optional)

Complete the following table for each mechanically ventilated space in the project building.

**Table IEQp1-1.** Ventilation Rate Procedure

AHU	Zone	Occupancy Category	Rp (cfm / person)	Ra (cfm/sf)	Occupant Density		Az (sf)	Vbz (cfm)	Ez	Voz (cfm)	Ev	Vot (cfm)
					Default	#/1000sf						
RTU-1	1	Office Space	5	0.06	<input type="checkbox"/> Yes	4.58	4,800	397.92	1	397.92	1	397.92

Add Row

Delete Row

*Note: Refer to ASHRAE Standard 62.1-2007 Ventilation Rate Procedure and ASHRAE 62MZCalc spreadsheet for detailed definitions and calculation procedures.*

**Table IEQp1-2.** Outdoor Air Flow

# LEED 2009 IEQ Credit 1 Template

---

Select all that apply to the project building:

- Project building contains non-densely occupied spaces
- Project building contains densely occupied spaces

## NON DENSELY OCCUPIED SPACES

Upload a controls drawing sample showing the outdoor air flow measurement devices that serve non-densely occupied spaces.



Files: 0

Complete the table below for all mechanical ventilation systems where 20% or more of the design supply airflow serves non-densely-occupied spaces.



# Template – Sample Control Sequence - OA

---

## RTU-1 Sample Sequence of Operation

2. Occupied Mode:
  - a. The supply fan shall operate continuously.
  - b. Minimum outside air: When the supply fan is started, the minimum outside air cycle shall be in control. The outside air damper shall modulate to maintain the minimum outside airflow setting as measured at the airflow measuring station.
  - c. Supply air temperature: ...
3. Unoccupied mode: ...
4. Alarms and reports: The following events shall send an alarm signal to the BAS:
  - a. When the minimum OA measurement at the airflow measuring station falls below 10% of the minimum OA design value.
  - b. ...

# LEED 2009 IEQ Credit 1 Template

Table. Outdoor Air Ventilation Rate

AHU Name or ID (20% or more of the design supply airflow serves non-densely occupied spaces)	Outdoor Airflow Measurement Device Present?	Minimum required outdoor air flow rate (CFM)	Accuracy of Outdoor Airflow Measurement Device (CFM)	Alarm Setpoint
RTU-1	Yes	398	5%	358.2

NOTE : Minimum required outdoor air flow rates are derived from the ASHRAE 62.1-2007 calculator.

All the outdoor air monitoring device is capable of measuring the minimum outdoor airflow intake flow with an accuracy of plus or minus 15% of the design minimum outdoor air rate, as defined by ASHRAE 62.1-2007 and the monitoring equipment is programmed to generate an alarm when the conditions vary by 10% or more from the setpoint. I have reviewed the information above and it is accurate to the best of my knowledge.

**REQUIRED SIGNATORY**  
 Initial Here :   
**CONTROLS DESIGNER**



# LEED 2009 IEQ Credit 1

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*LEED 2009 IEQ Credit 1:  
Outdoor Air Delivery Monitoring  
is one of the easiest points to get !*

# Summary

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- Airflow Measurement & Control = Comfortable, Healthy, Efficient, Compliant Indoor Environment
- Directly Measuring & Controlling Airflow is the Best Method for Outdoor Air Delivery & Building Pressurization Control
- Airflow Monitors Must Be Suitable, Accurate, Stable, & Reliable

---

# *Questions?*

Jim Riendeau

843 877 4049